CONSTRUCTION FOUNDATION REPORT MISSOURI RIVER FORT PECK MONTANA VOLUME 2 DRAWINGS(U) ARMY ENGINEER DISTRICT OMAHA NE JAN 83 AD A134 914 UNCLASSIFIED F/G 13/13 Νl



MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS - 1963 - A

CONSTRUCTION FOUNDATION REPORT

MISSOURI RIVER
FORT PECK LAKE, MONTANA

VOLUME II
DRAWINGS



TIC FILE COPY

JANUARY 1983



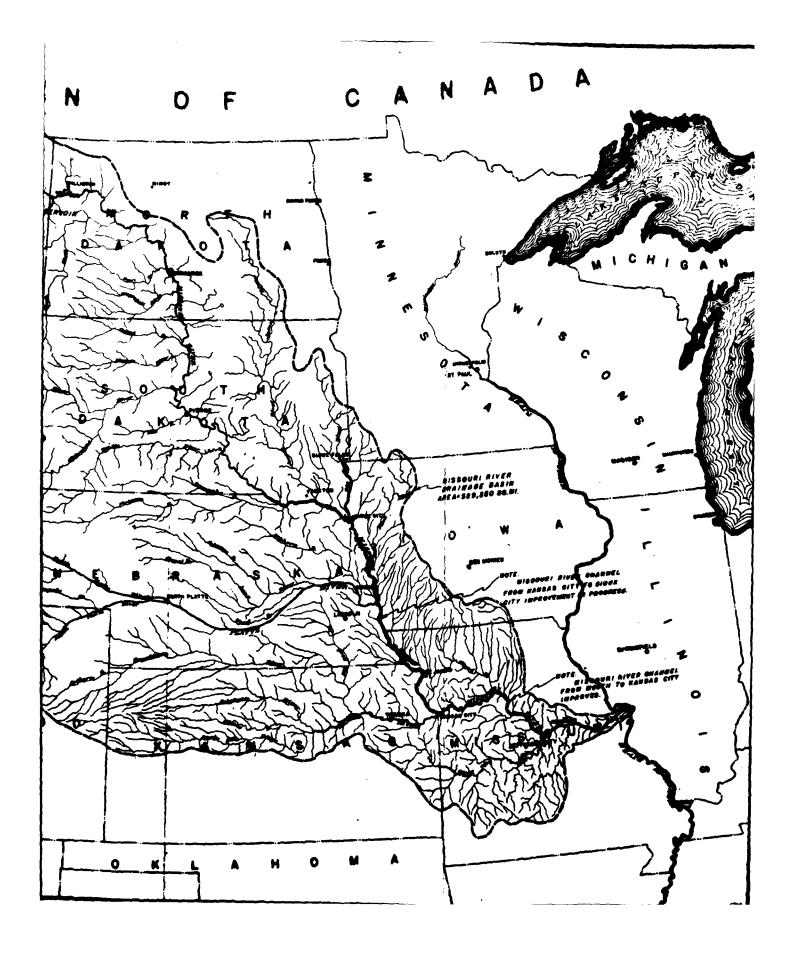
US Army Corps of Engineers

Omaha District

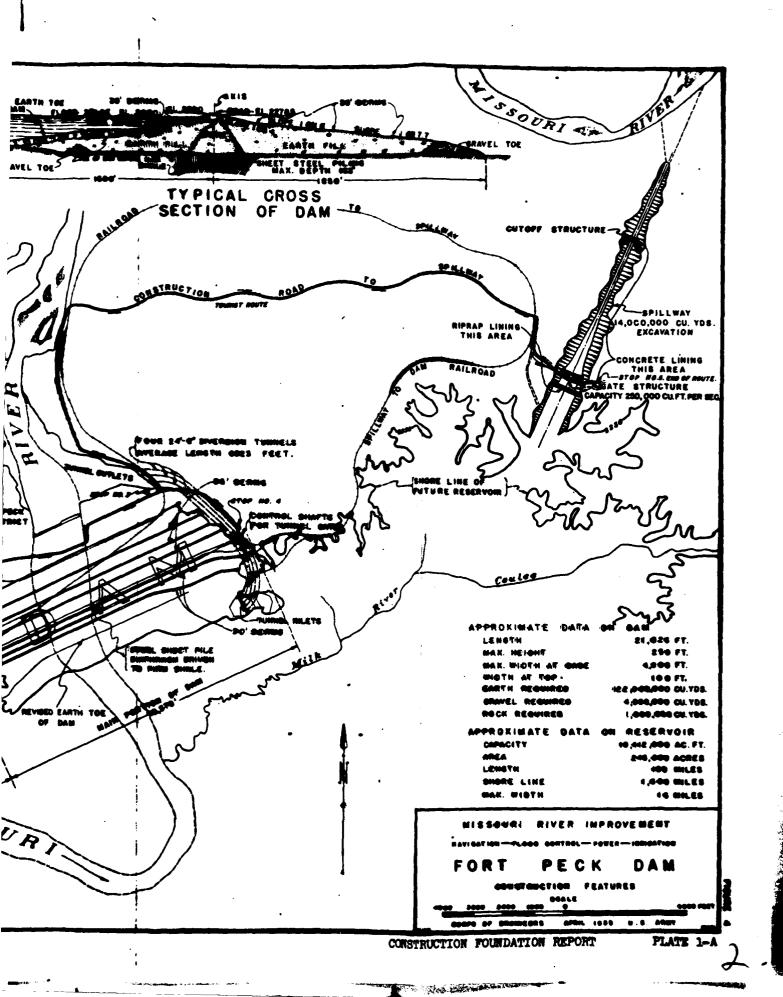
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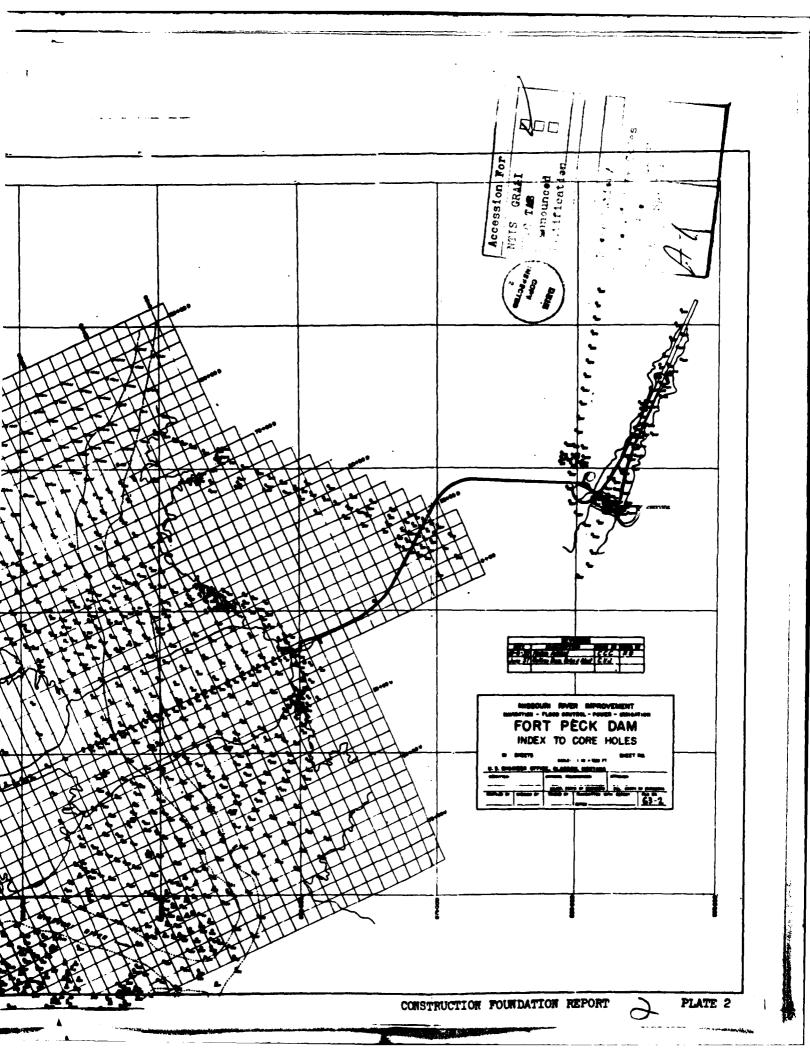
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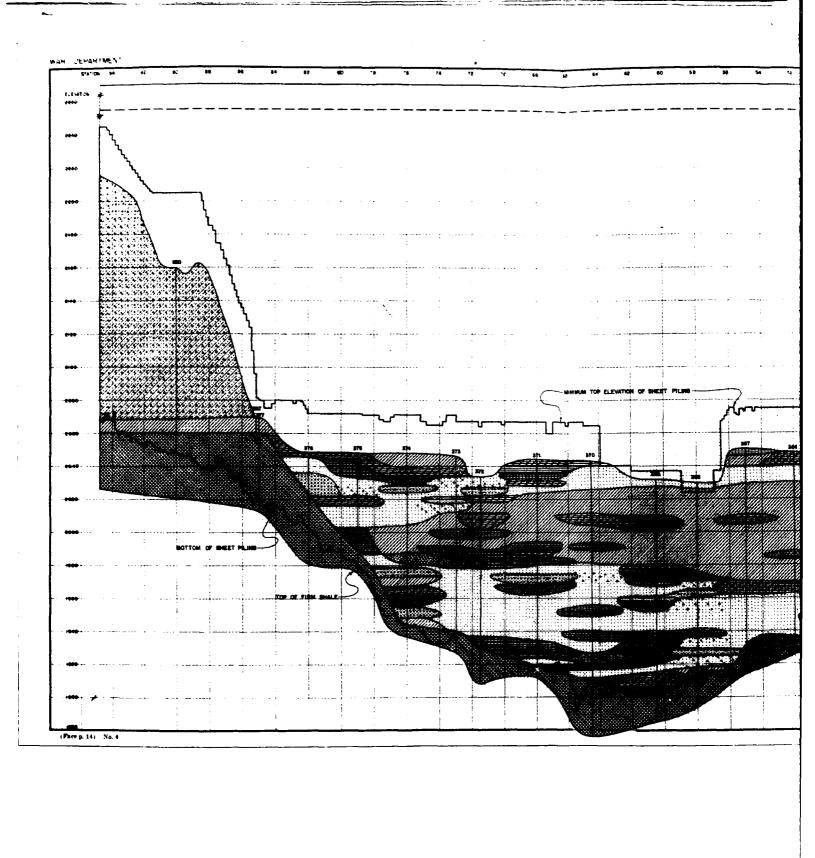


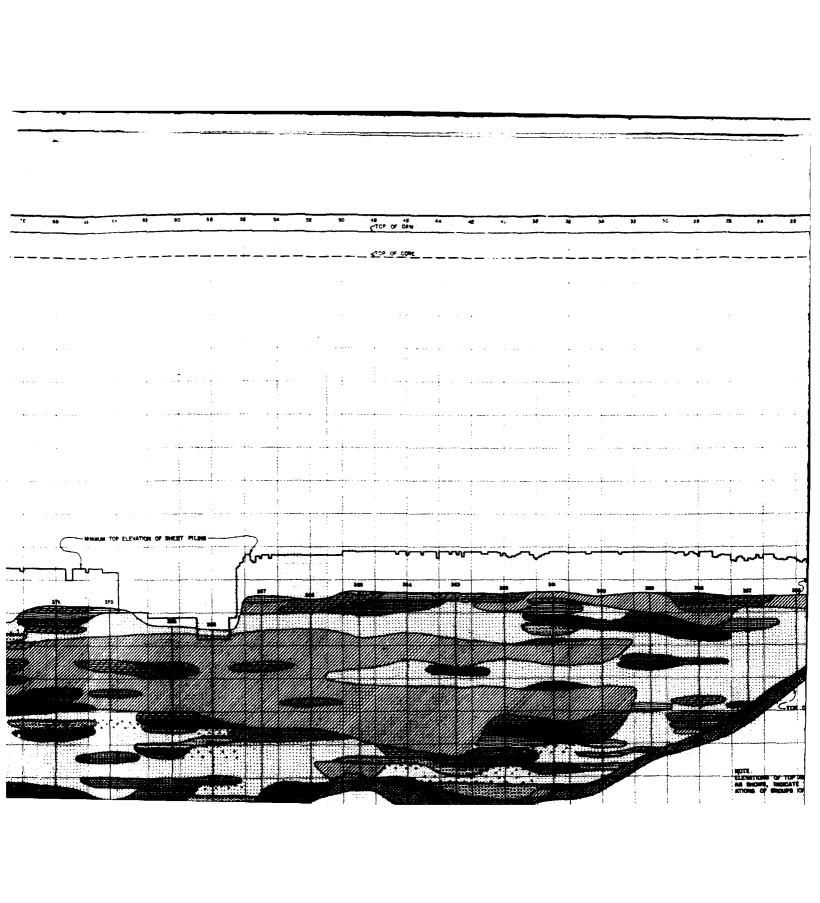


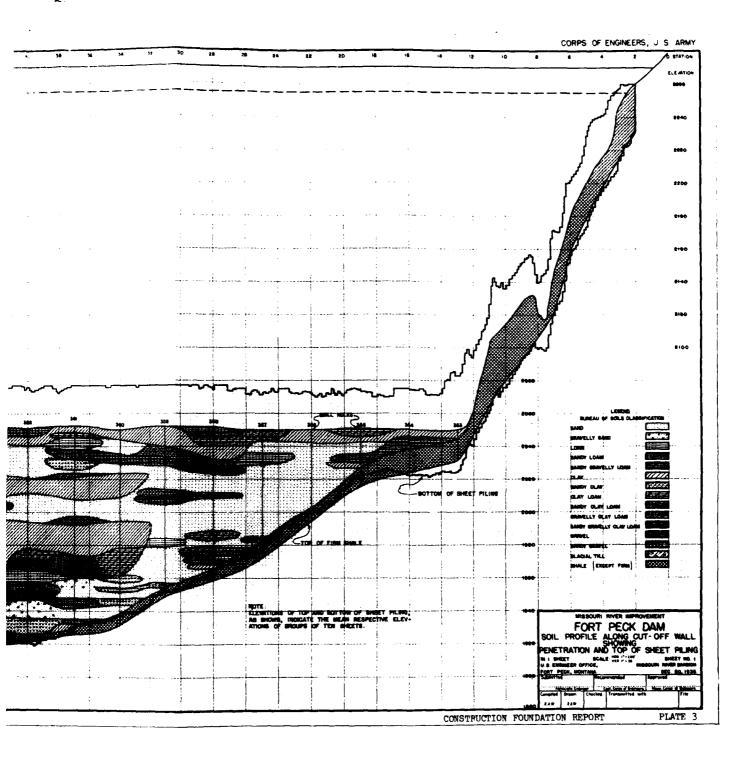
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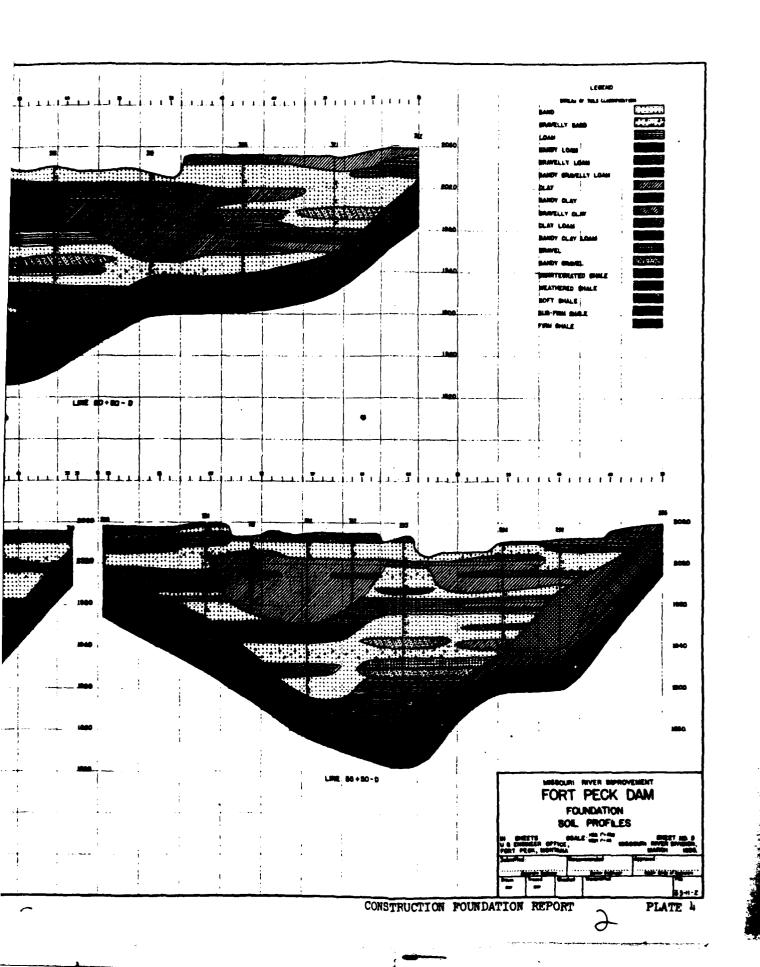




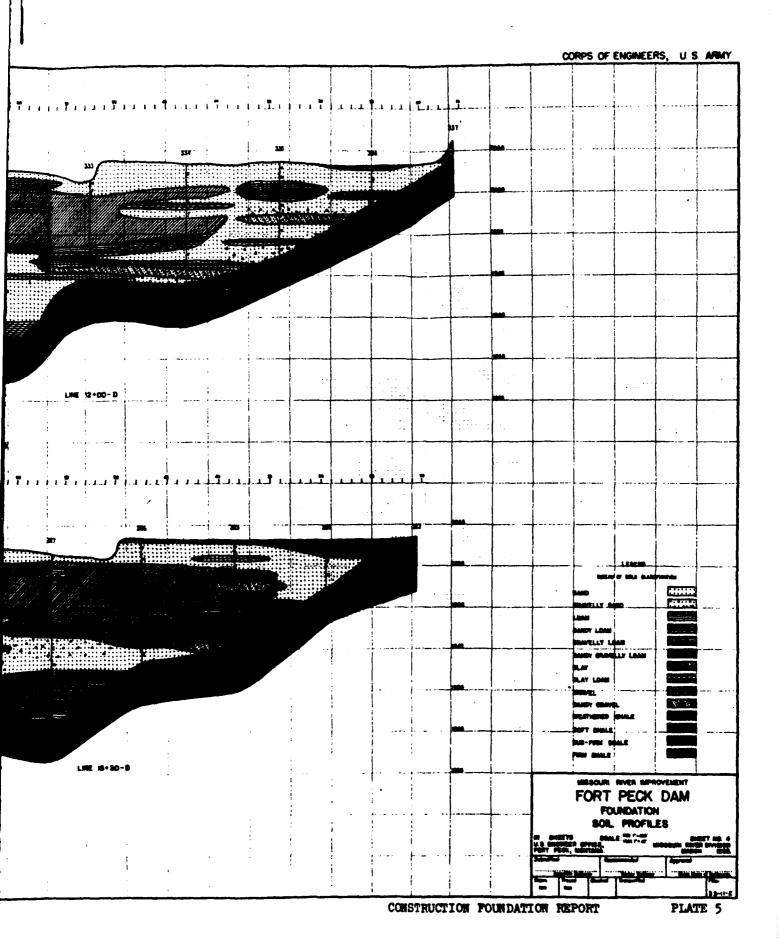


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WAR DEPARTMENT



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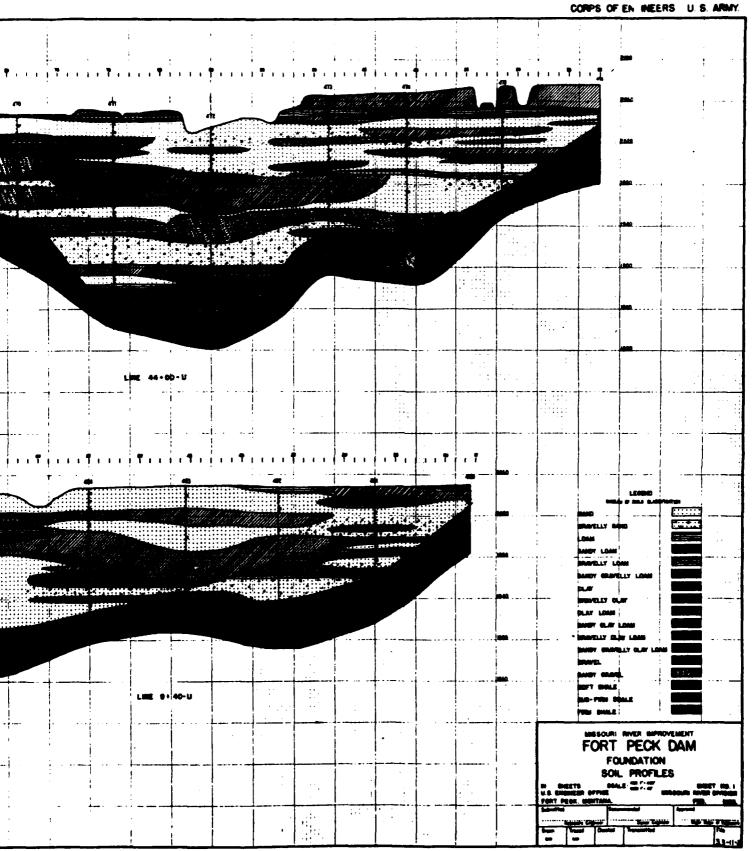
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WAR DEPARTMENT

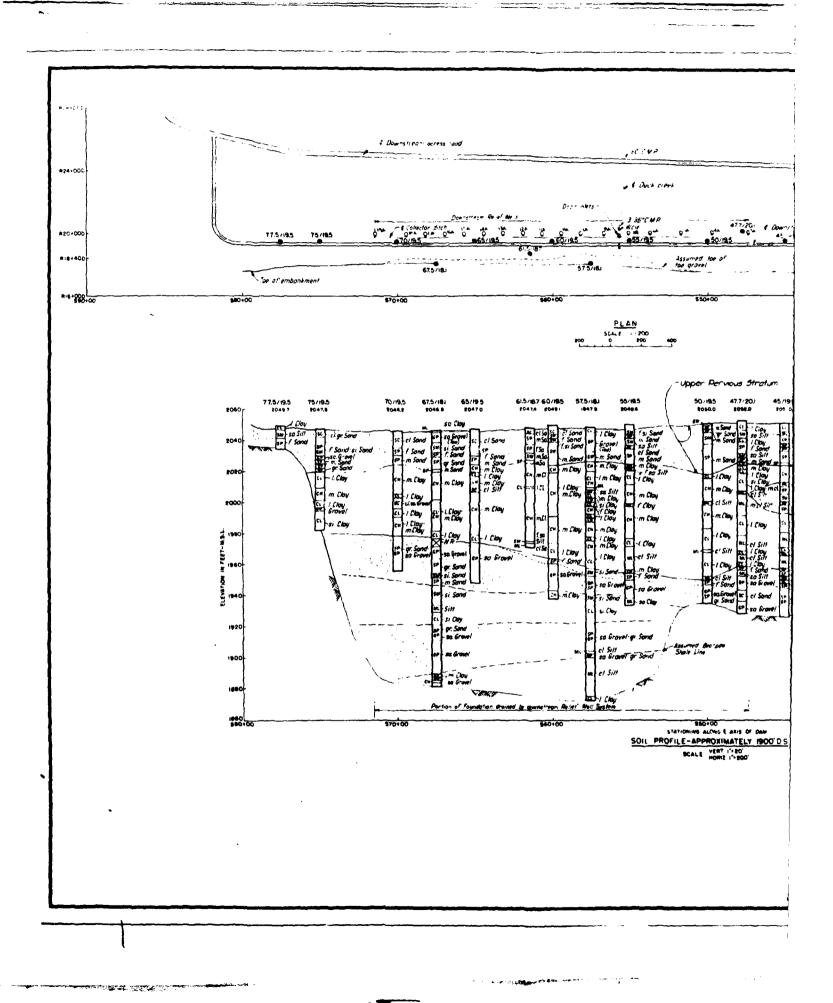
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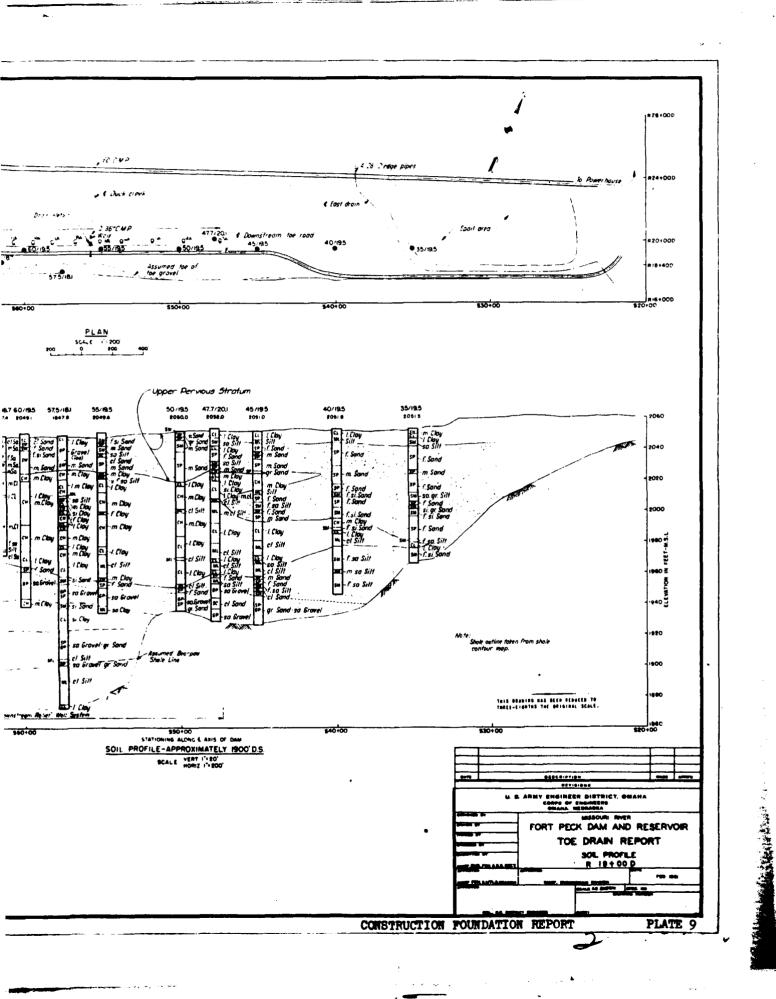
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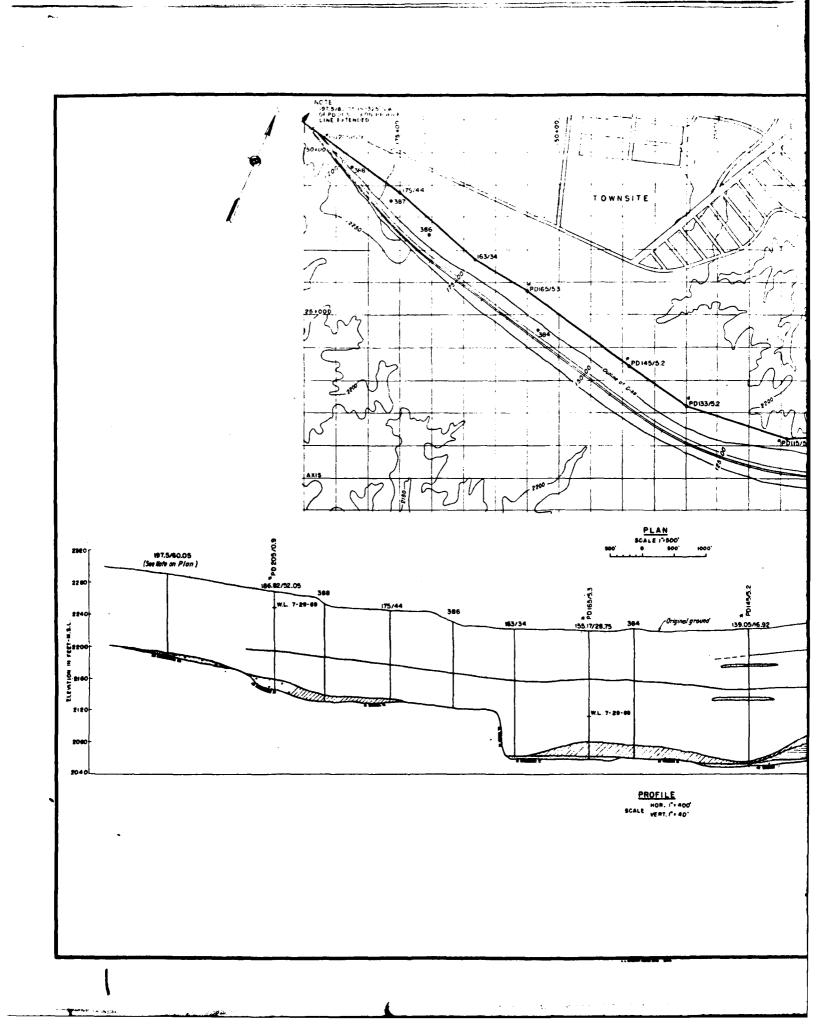


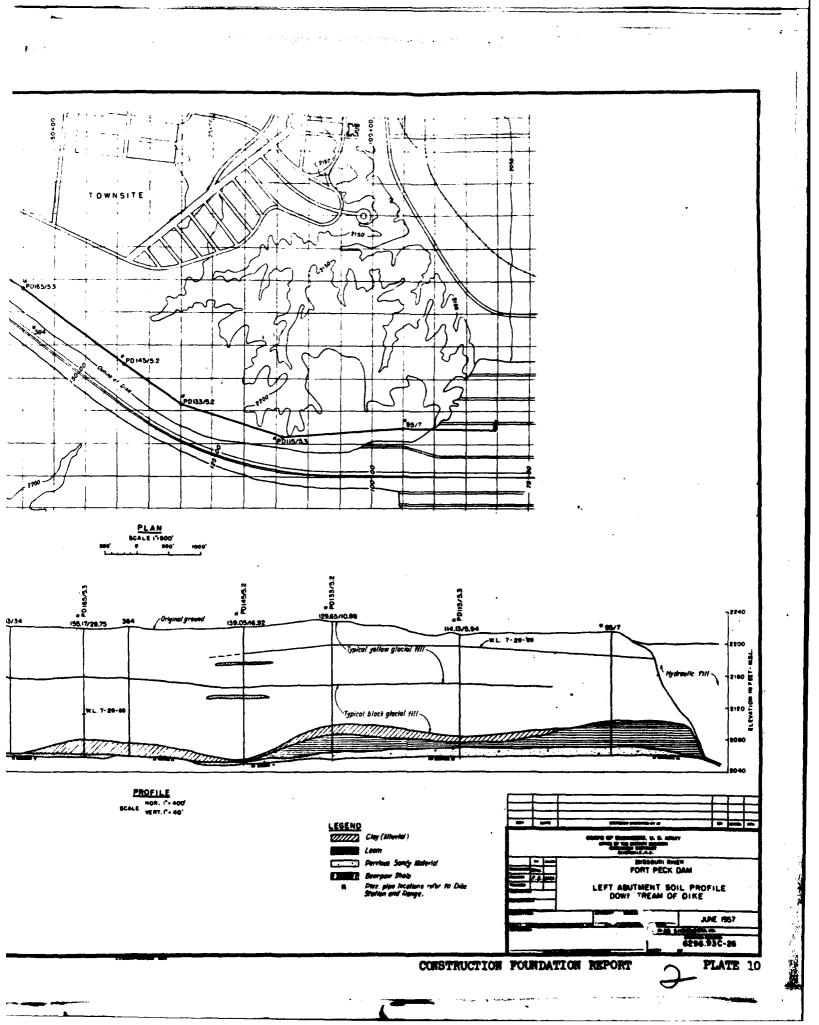
CONSTRUCTION FOUNDATION REPORT

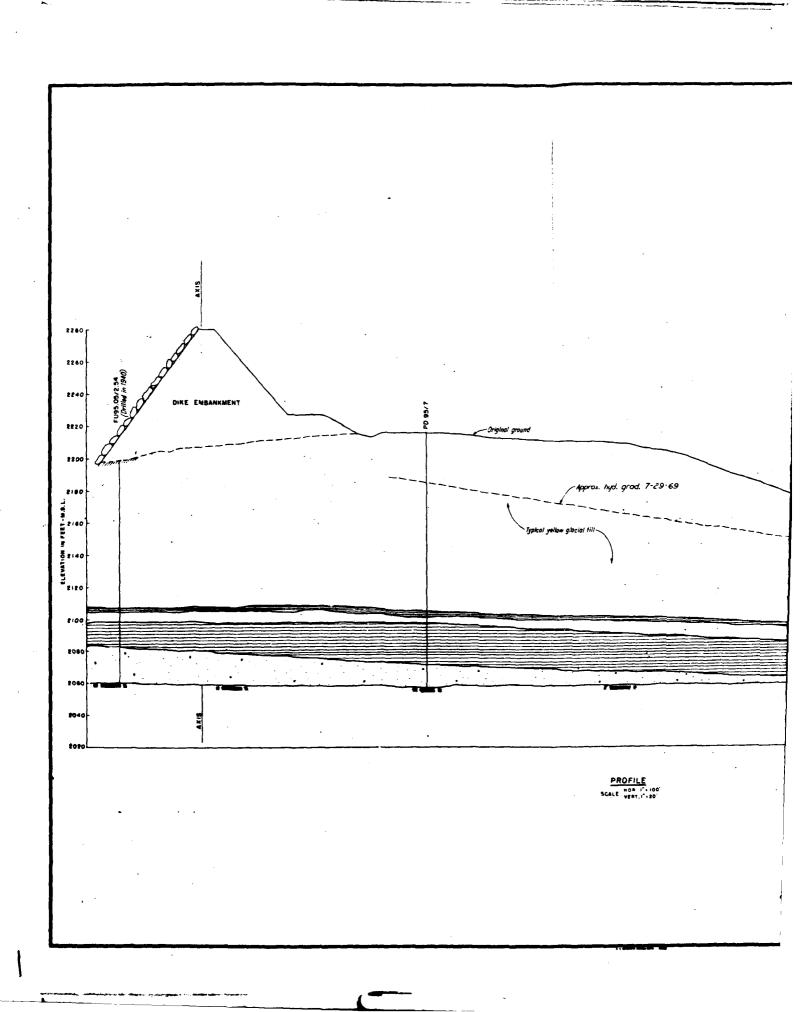
PLATE 8

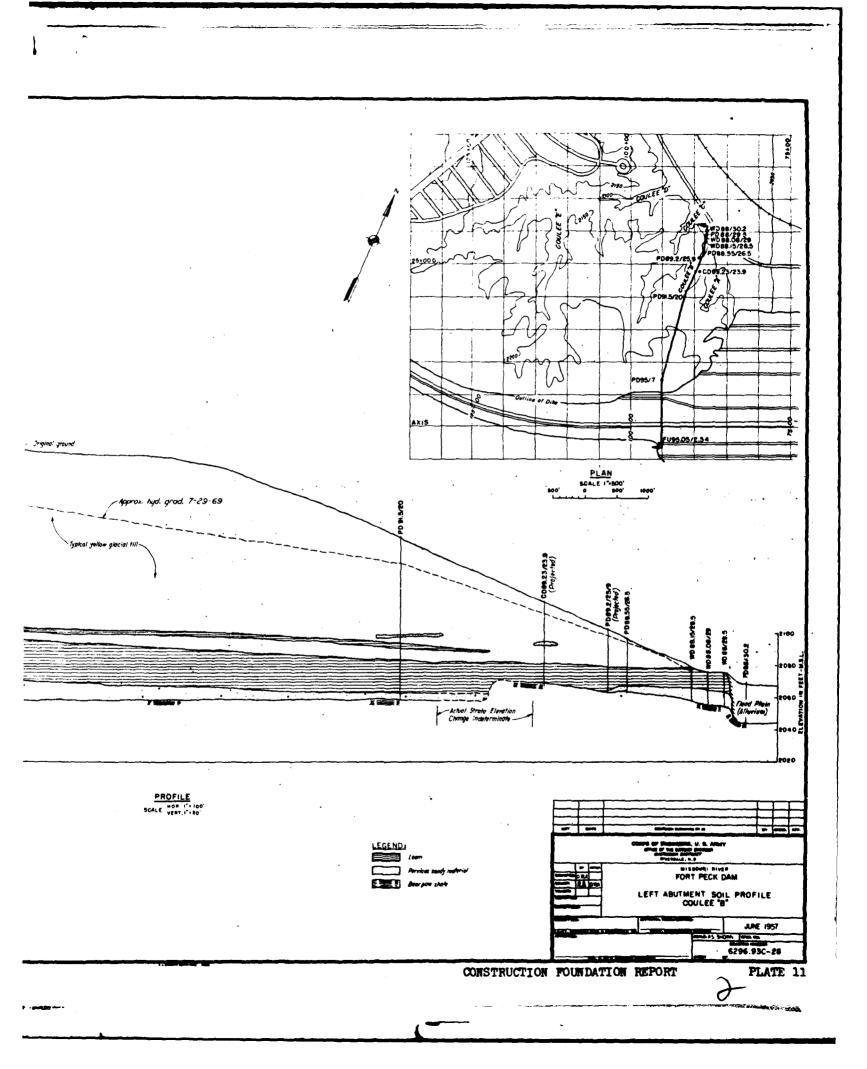


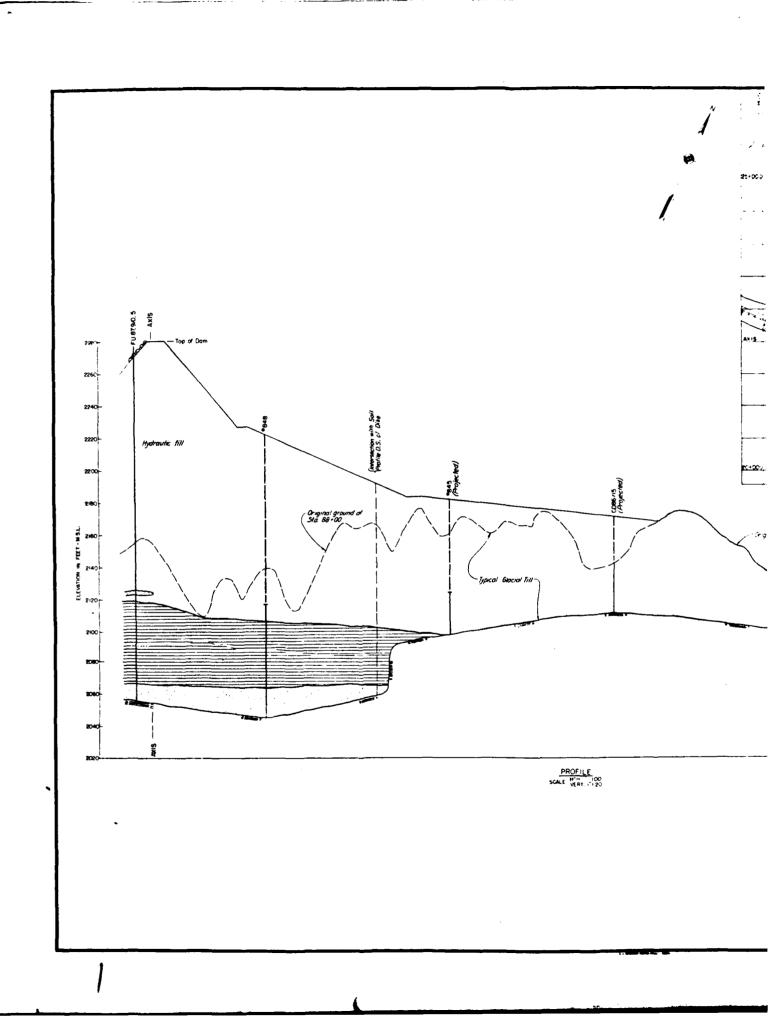


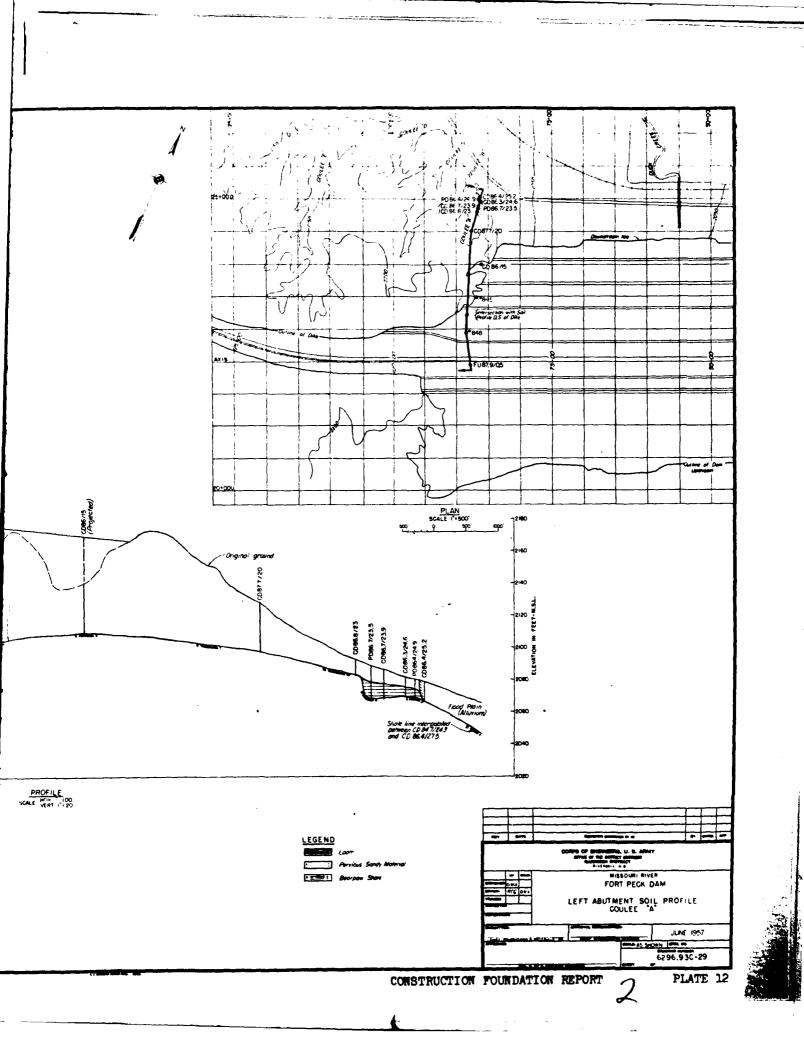


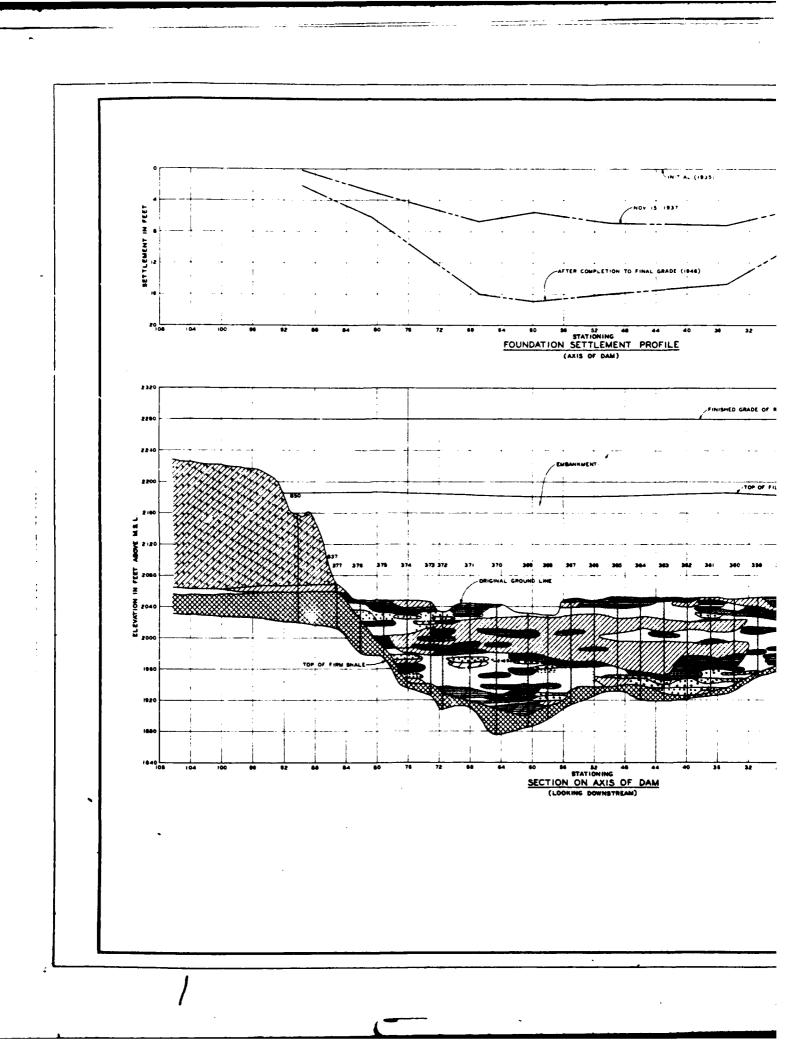


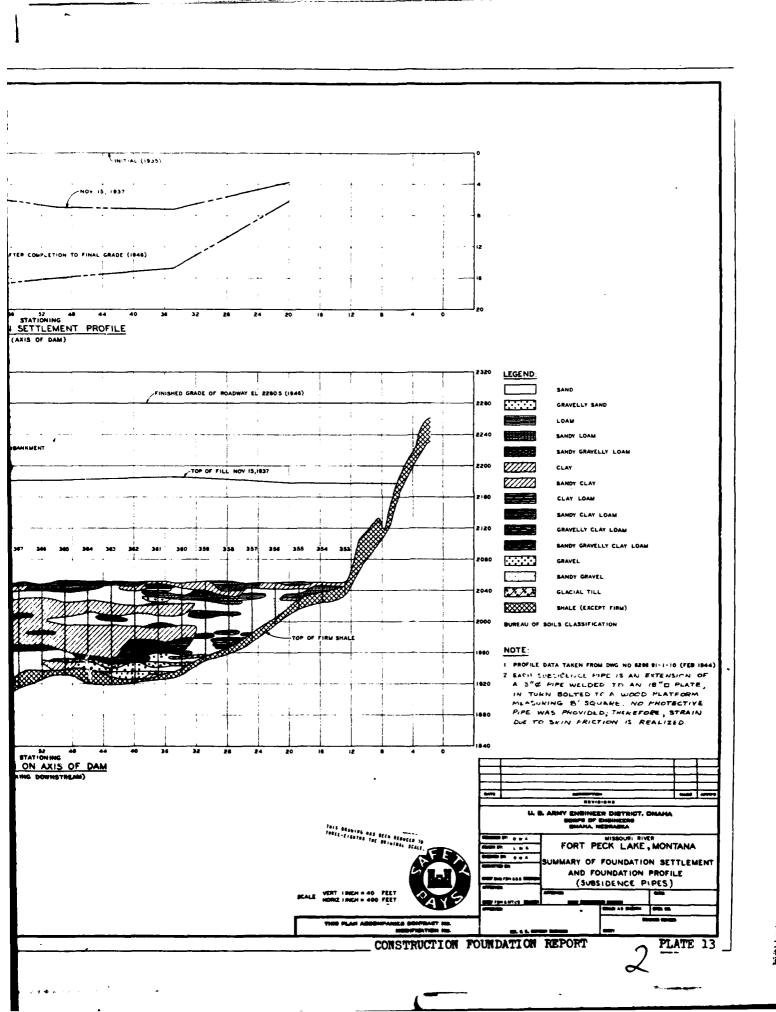


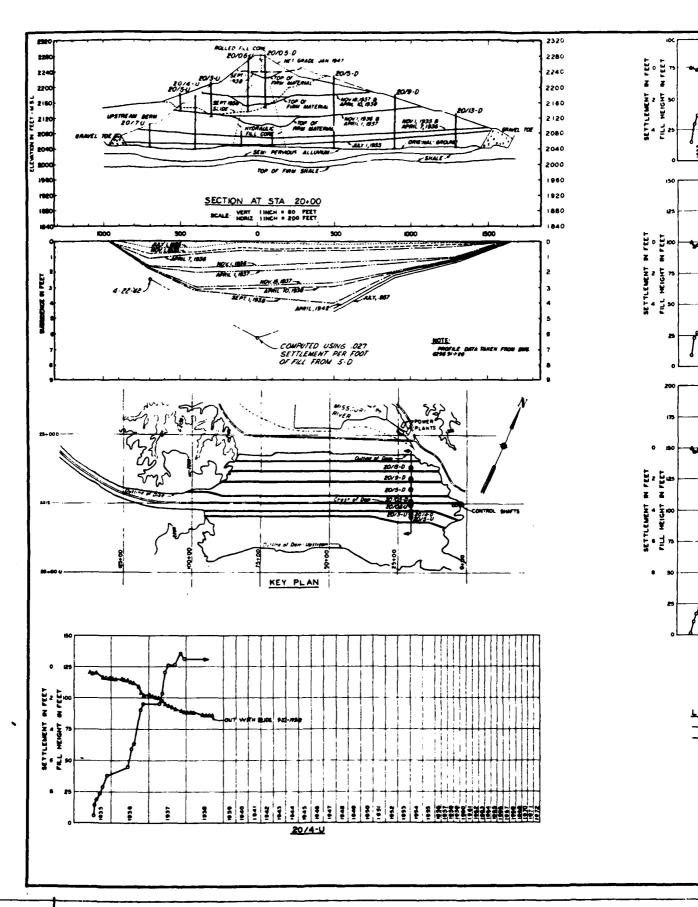


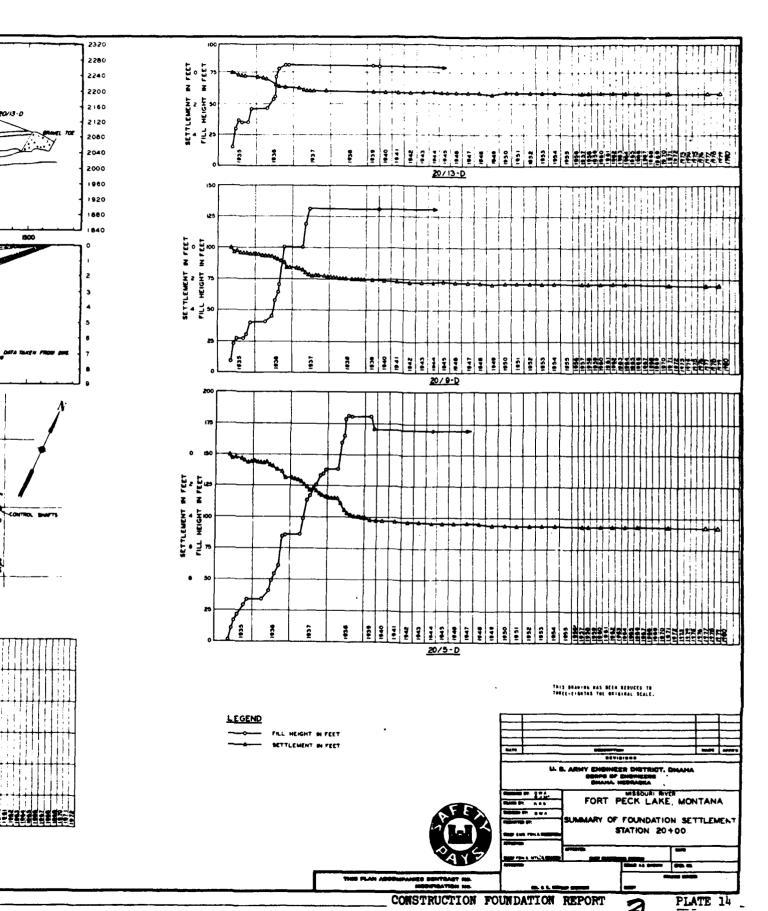


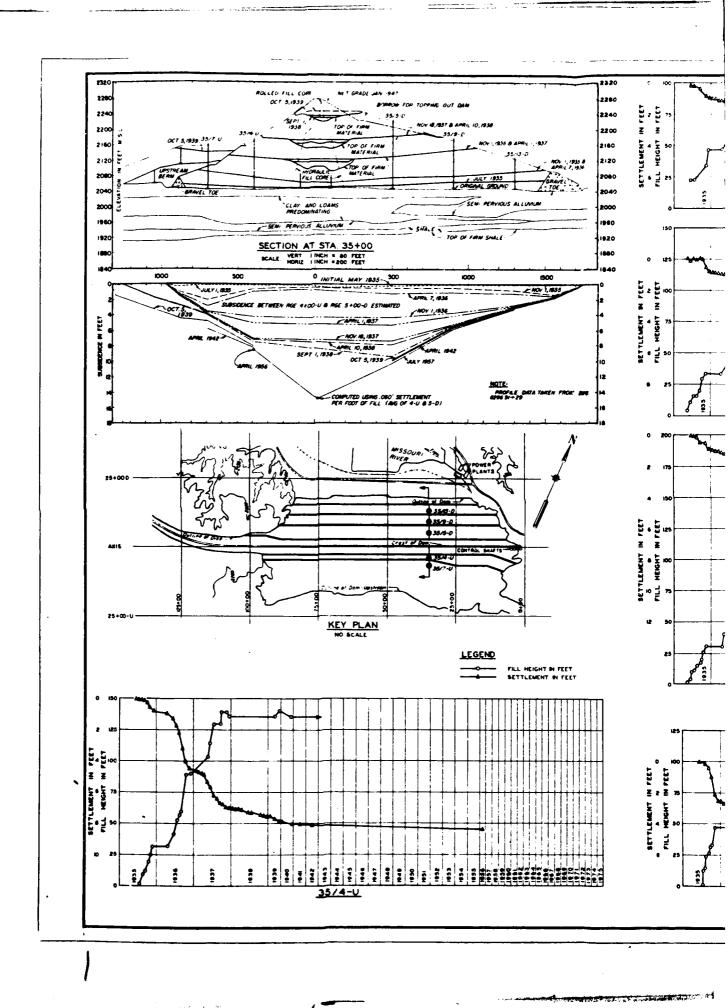


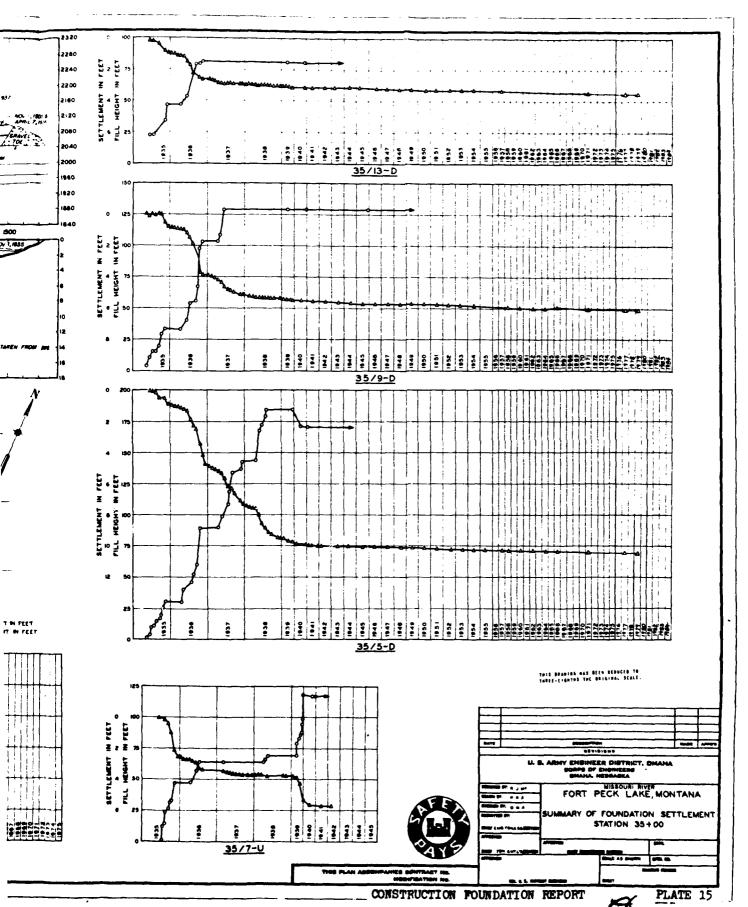


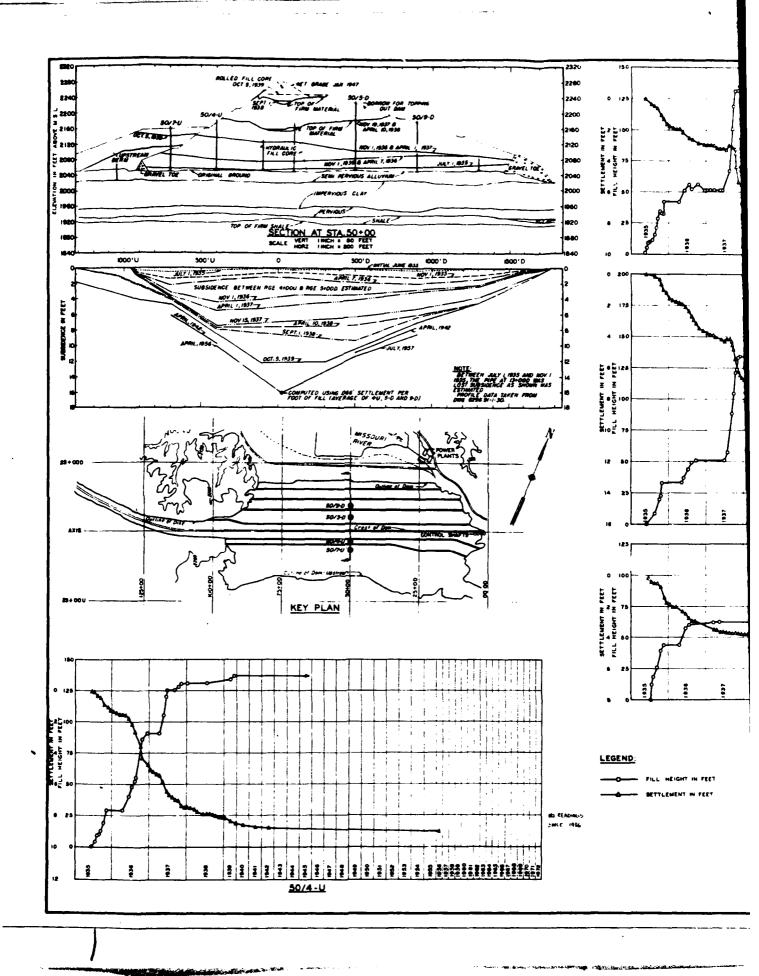




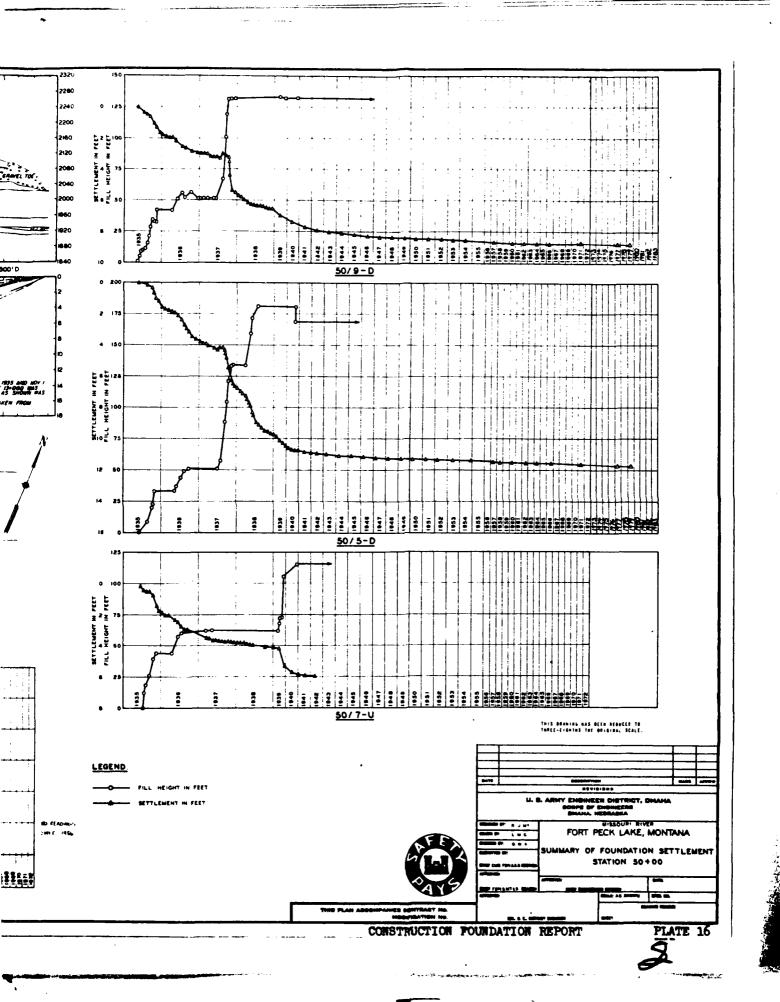


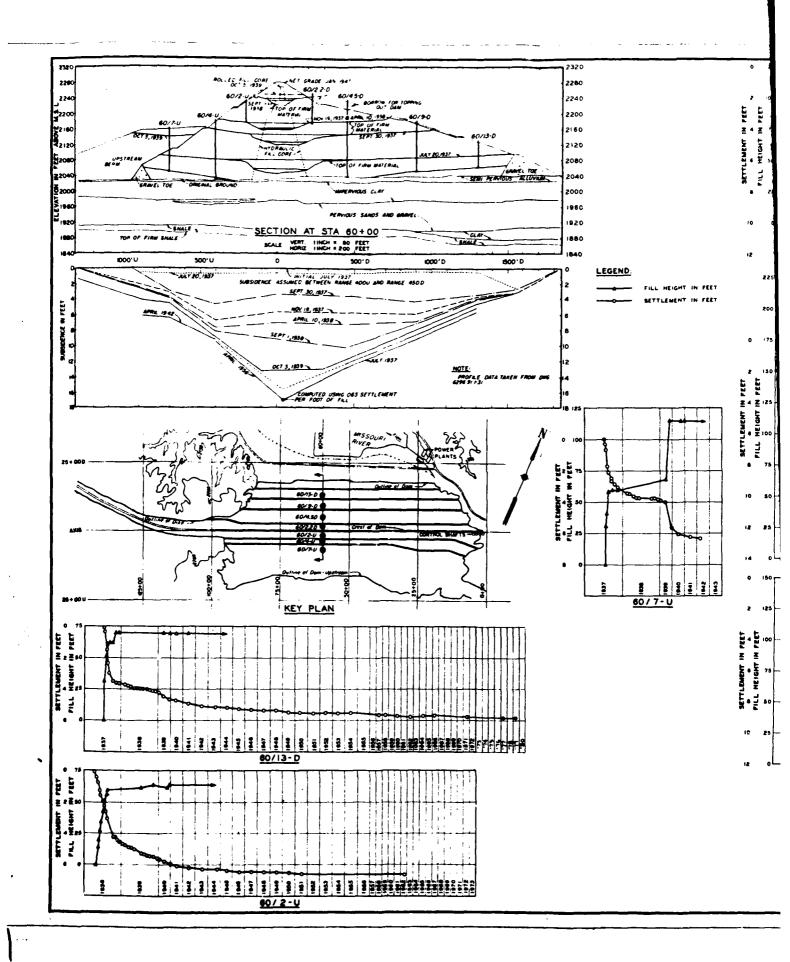




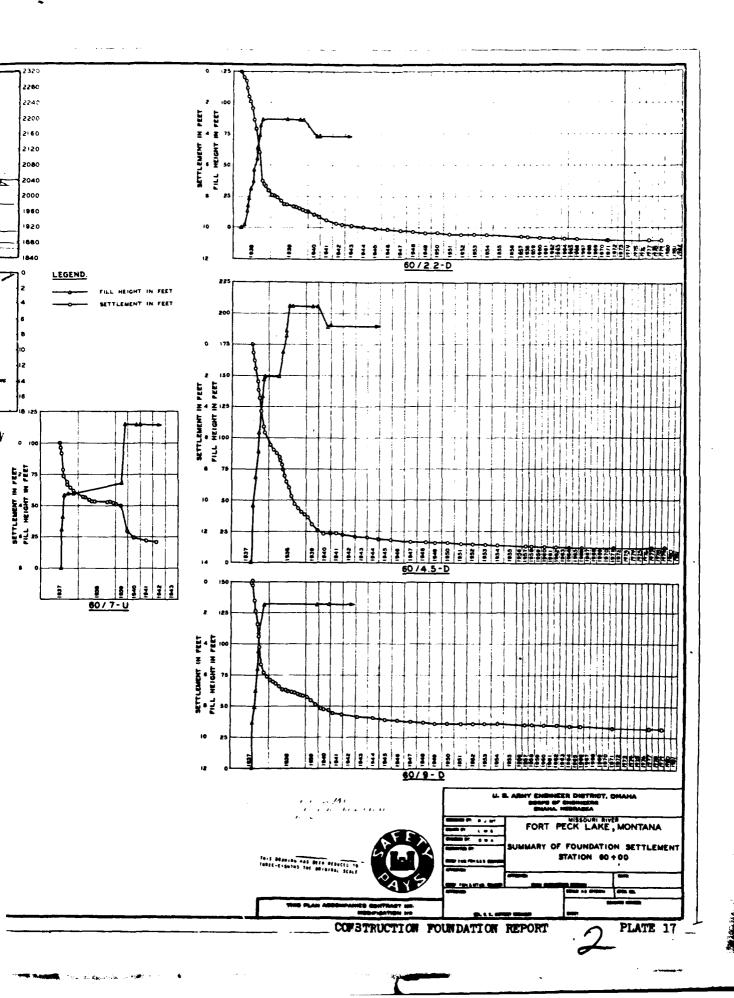


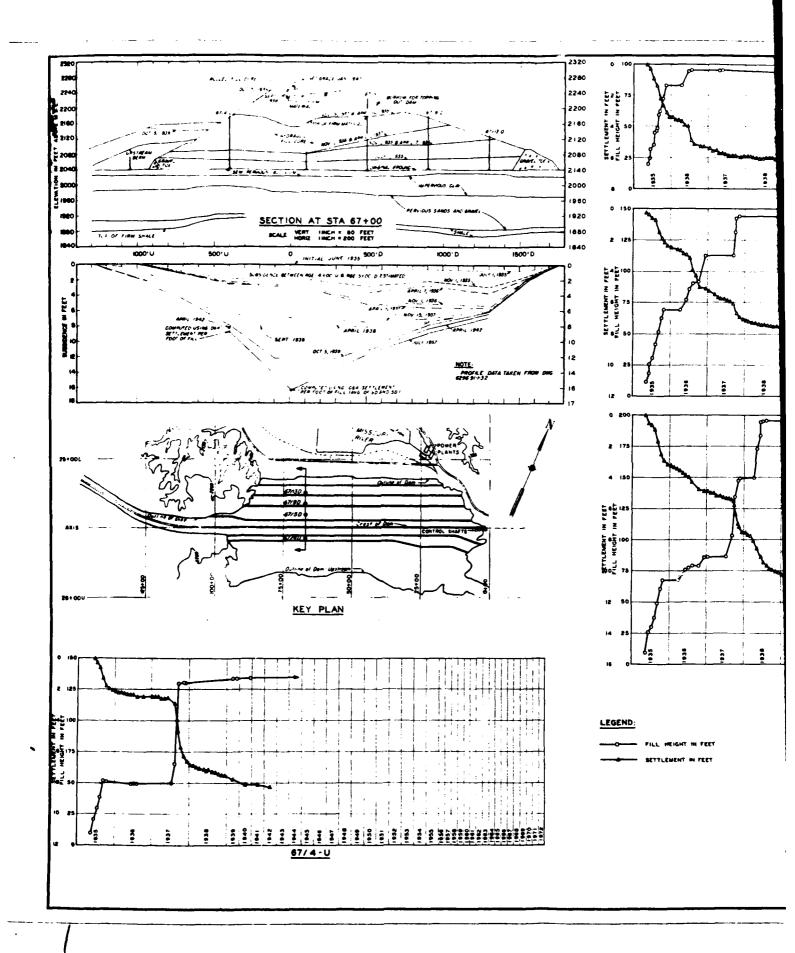
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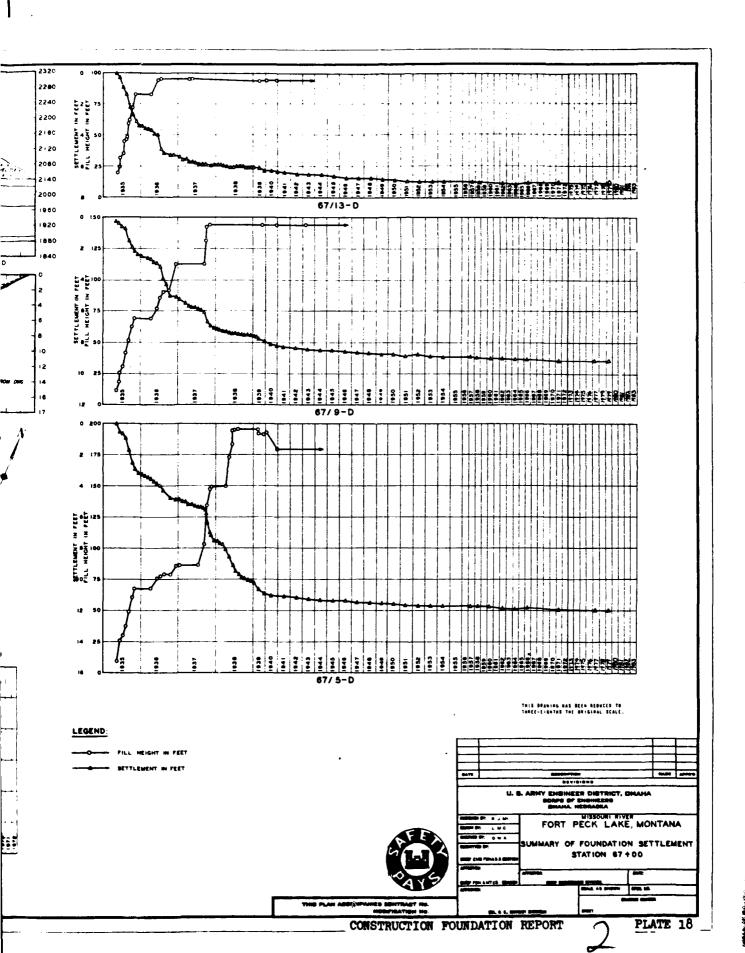




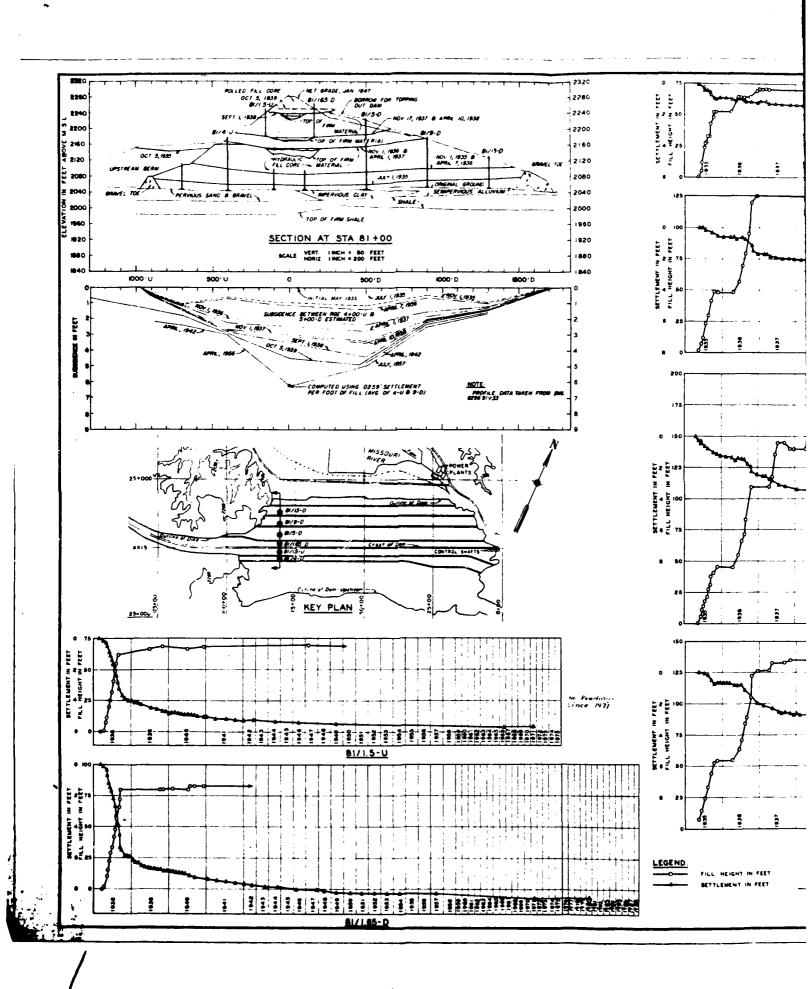
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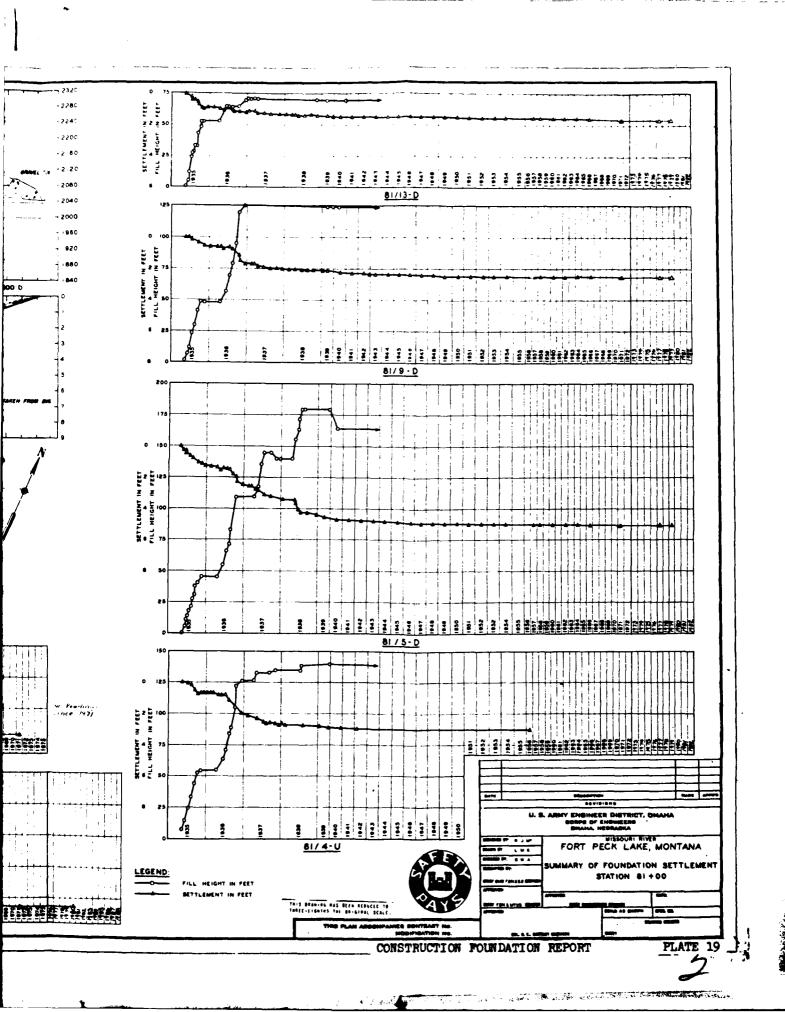


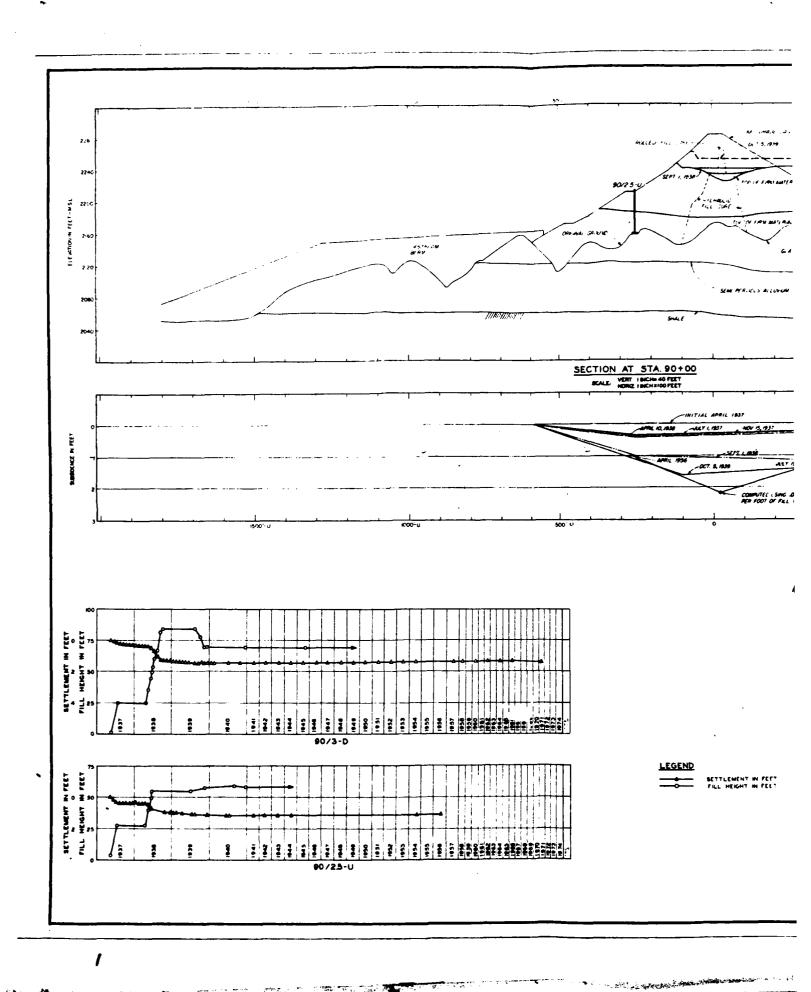


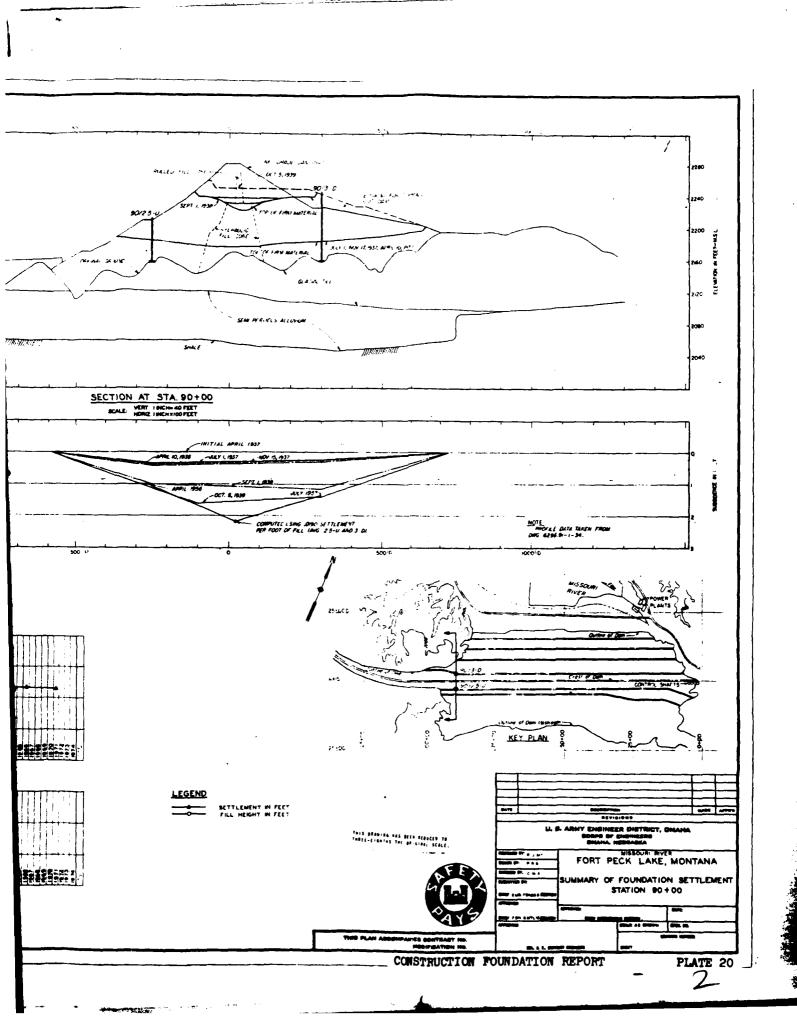


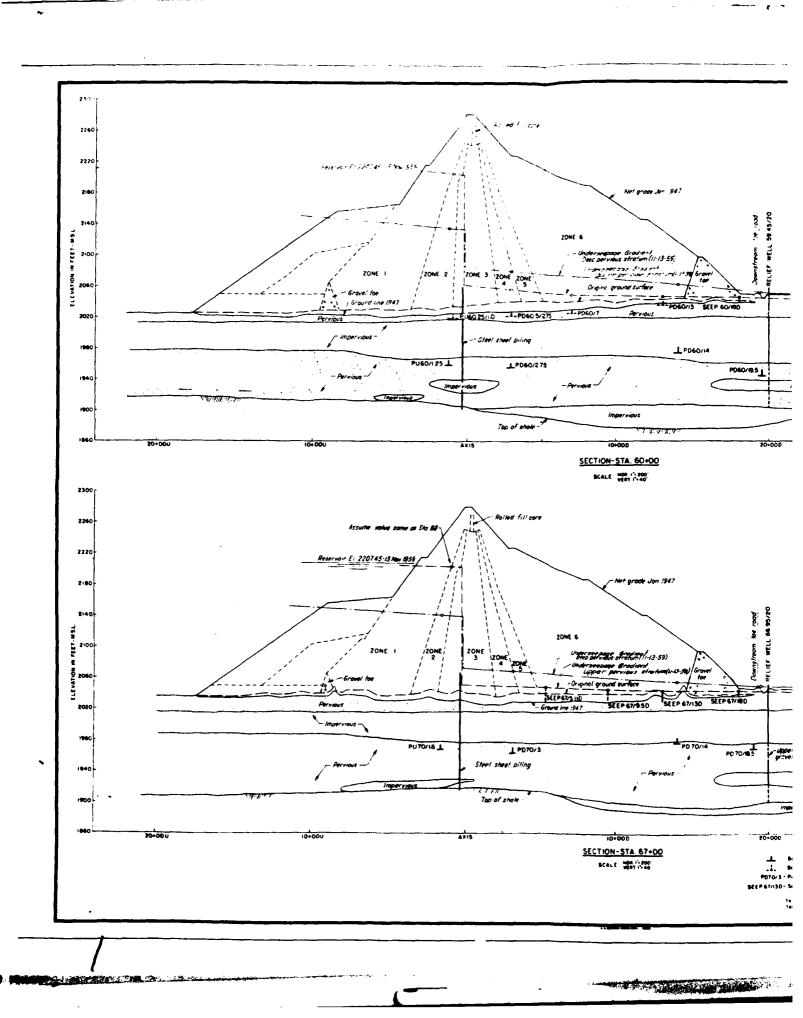
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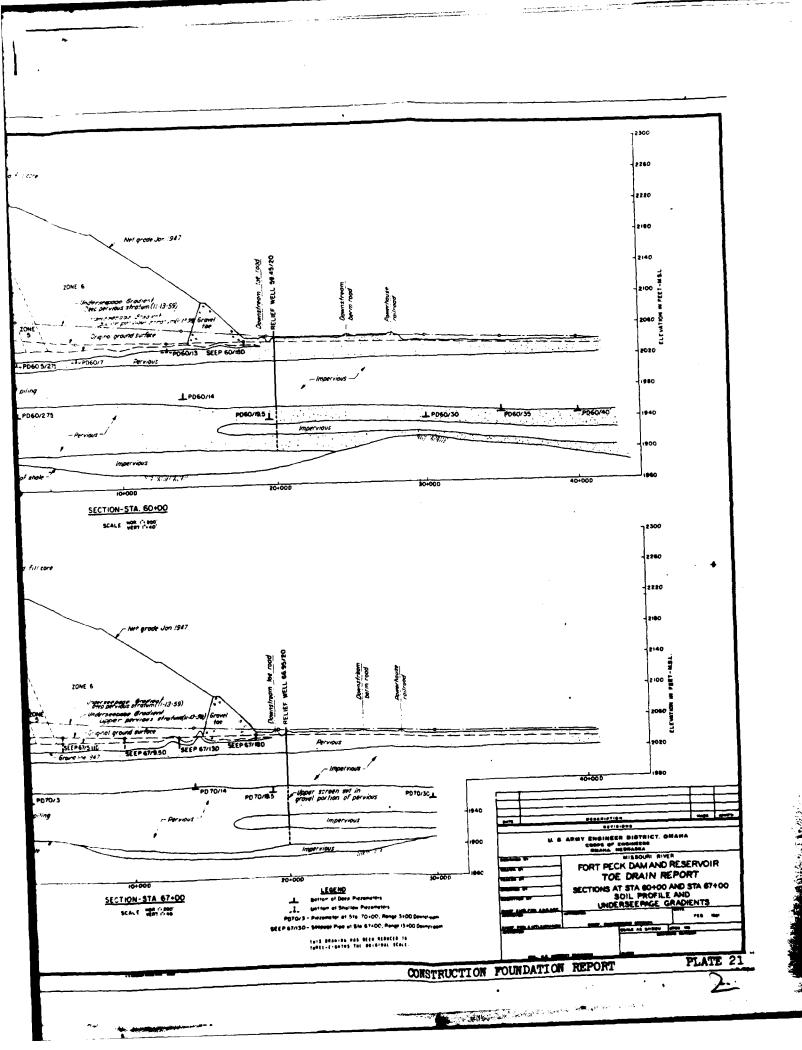


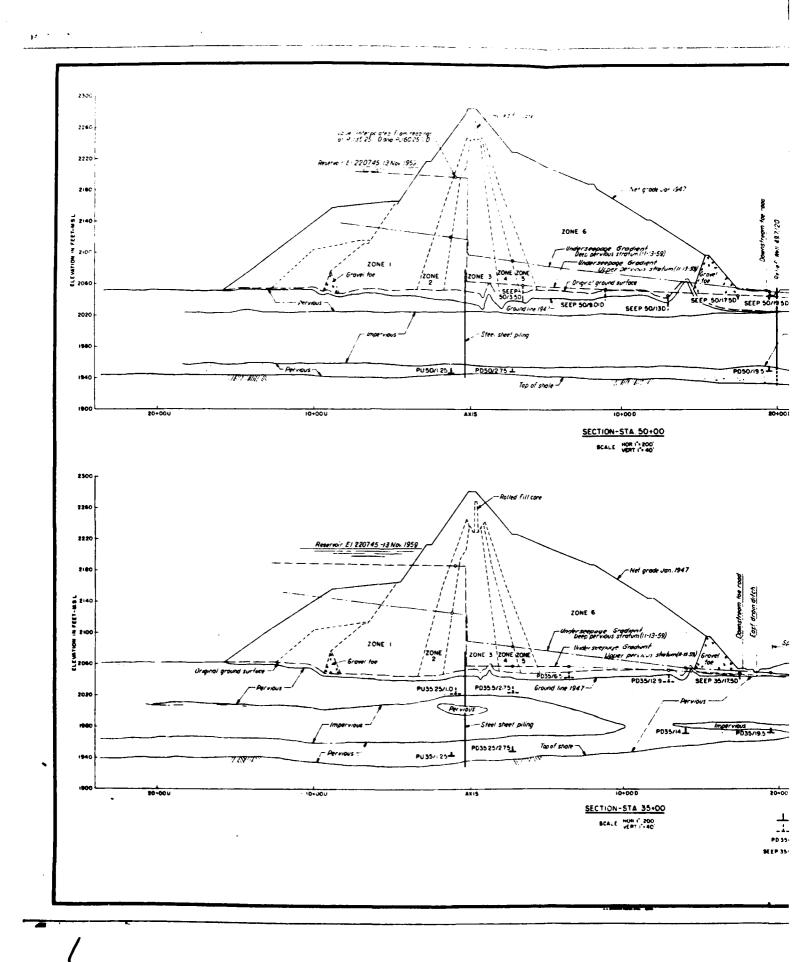




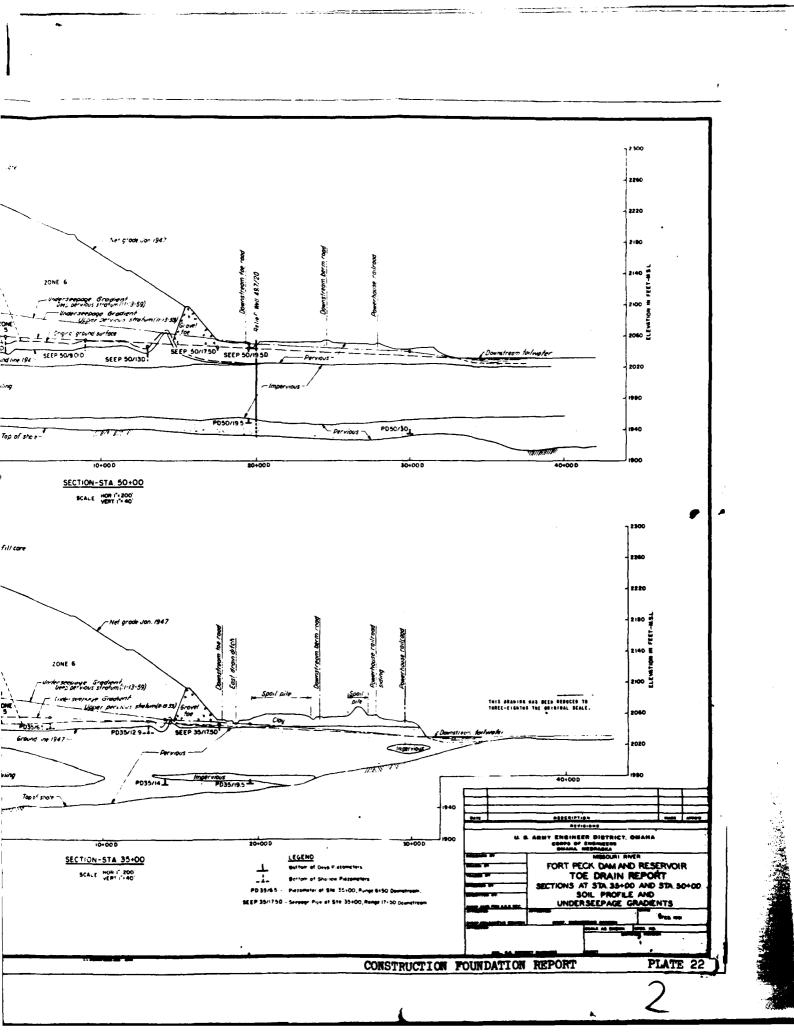








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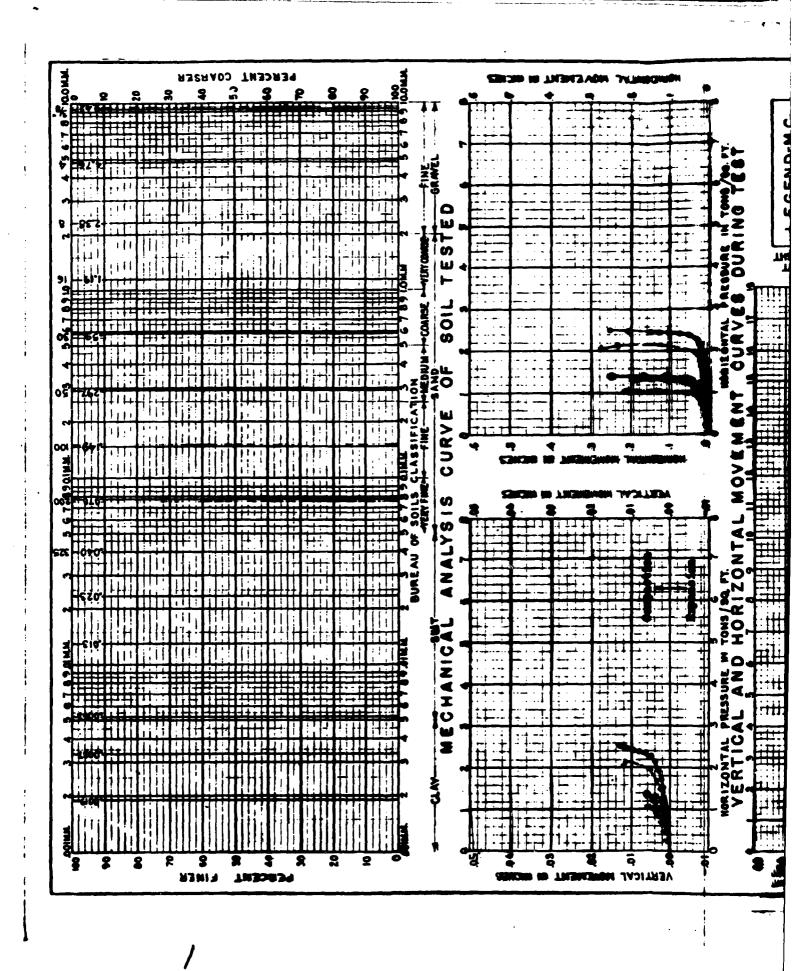


PLATE 23

SHEET 32

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Results of tests on undisturbed samples of shale taken in the Fort Peck Dam Foundation, downstream, with 6-inch sampler

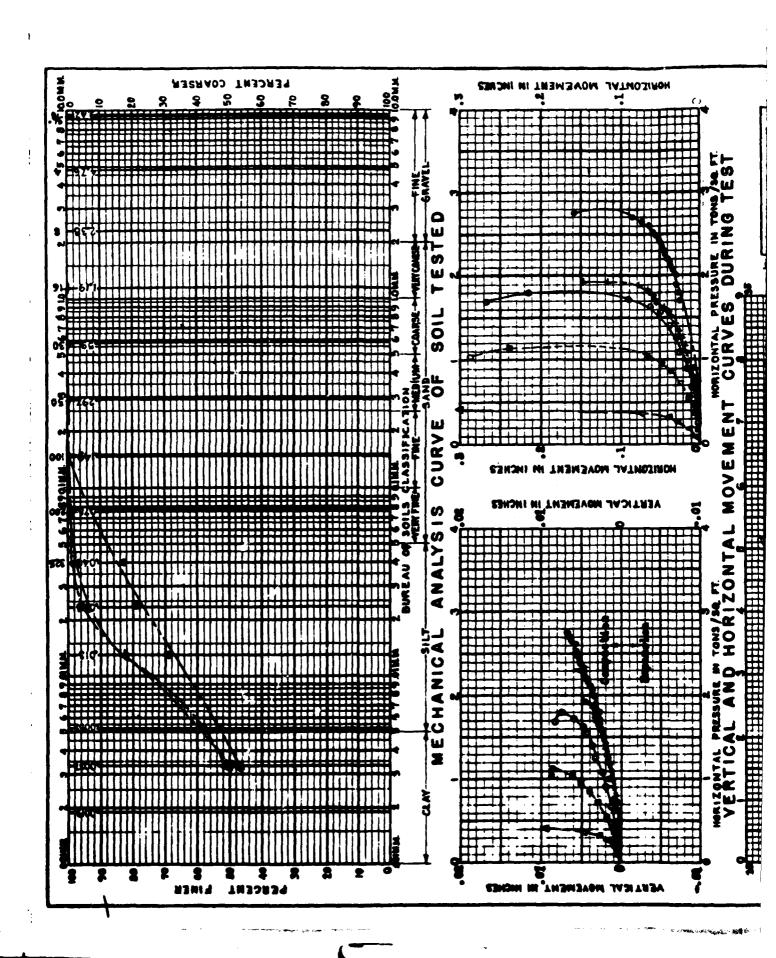
1		3				7		•
lenspin Né.	Sand orer- bardes	Depth into shale	Equivalent load in tons/	Mois- ture content, percent dry weight	Shearing strength in tous/ sq. ft.	Computed shearing strength tens/sq ft. with Tane. = 18, C = 39	Ratio 4	Type test
		HOLE (C-12 ST	ATION	10+75, R	LNOE 8+00	D	
))	14.6 14.6 14.6	1.4 2.4 3.4 7.4	4 85 .97 1.80 1.21	31.3 22.5 35.3 26.0	. A. 45 . 36 . 30	9, 35 .37 .40 .42	1.85 2.32 2.7 1.96	Quick, Consol Quick, Quick,
	•	HOLE	C-13 5T	ATION	12+00, R	ANGE 8+00	D	<u>'</u>
	X: X: X:	4.0	1. 29 1. 29 1. 41 1. 59 1. 66 1. 90 2. 01	27.7 48.8 26.0 25.5 26.0 25.0	1.35 1.66 .94 2.66 1.13 1.35 1.25	1. (2 . (3 . (4 . (6 . (8 . (8 . (8 . (8) . (8) . (8) . (8) . (8) . (8) . (8) . (8) . (8) . (9) . (9)	29 25 21 43 23 21 23	Quick. Conrol Quick. Quick. Quick. Consol Quick. Quick.
		BOLE	C-14 ST	ATION	12+ 00, B	TAGE S+4	D	
	66.3 66.3 66.3 66.3	1.7 3.7 5.7 7.2	2 49 2 90 2 72 2 94 2 18	29. 0 24. 8 21. 2 20. 2 23. 5	2. 25 1. 30 2. 4 1. 90 1. 50	• 65 - 67 - 77	2.5 1.0 2.5 2.7 1.05	Quiet. Count Quiet. Quiet. Quiet.
	<u>'</u>	BOLE	C-18 ST	ATION	13+25, R	ANGE 8+0	D	<u> </u>
	71.5 71.5 71.6	2.0 8.5 7.75 M. 78	3. 87 3. 96 4. 21 4. 46	25. 5 26. 7 26. 5 26. 0	1. 39 1. 51 2. 56 2. 65	0. 90 . 92 . 95 1. 95	1. 55 1. 64 2.7 1. 96	Quick. Consol Quick. Quick.
		BOLE (E-16. 3¶	MOLTA	14 +40 , R	ange s+0	Ð	
<u></u>	=	1.0 2.0 7.0	5.70 5.90 6.36	27.7 27.1	1.00 1.00	1.36 1.36 1.30		Quick Consul Quick
		TEST S	EAFT,	STATES	N 194-00,	RANGE 1	D D	
 L	R:	1.3	1.36	38.1 34.3 138.2	8.73 .98 1.66	. 44 . 45	1.04 2.13 2.77	Quist. Quist. Quist.
QLA	CIAL 1	TILL FI	IOM R	OLE AT	STATE	N 106+00, I	BANGE	0+06 D
	81	2.8 7.8 0.8	1 36 1 38 1 70	26.7 16.6 26.4 27.9	1.36 1.00 1.00	4.80 .80 .80	1.64 1.62 1.57 1.57	Quiek. Quiek. Consol Quiek.

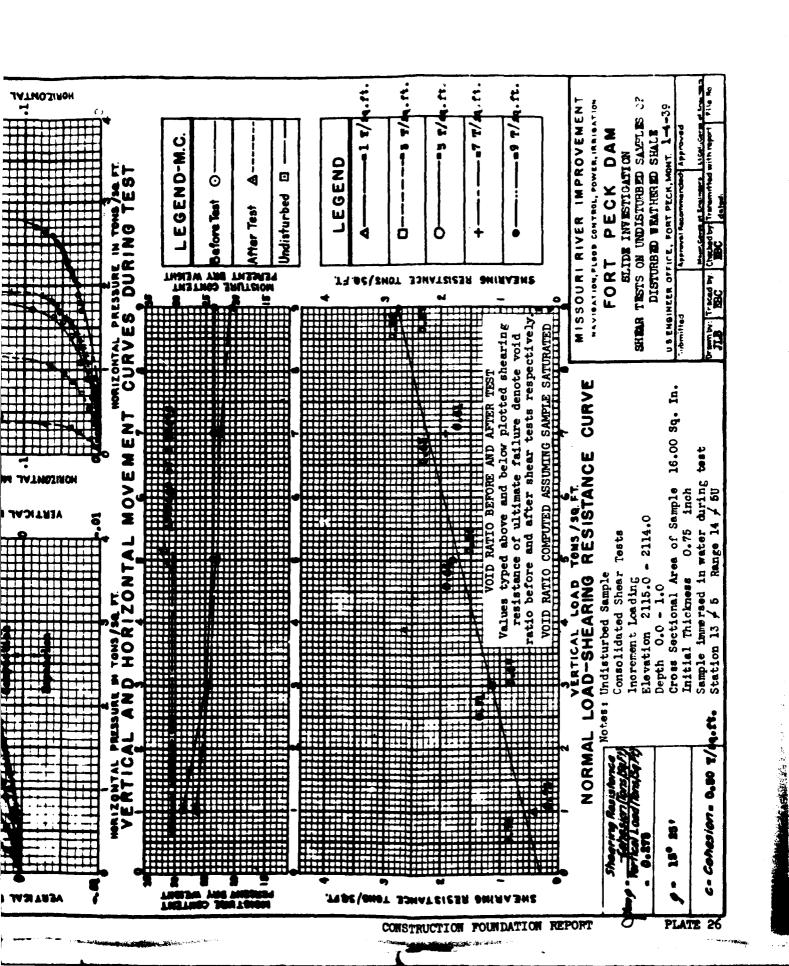
I After test.

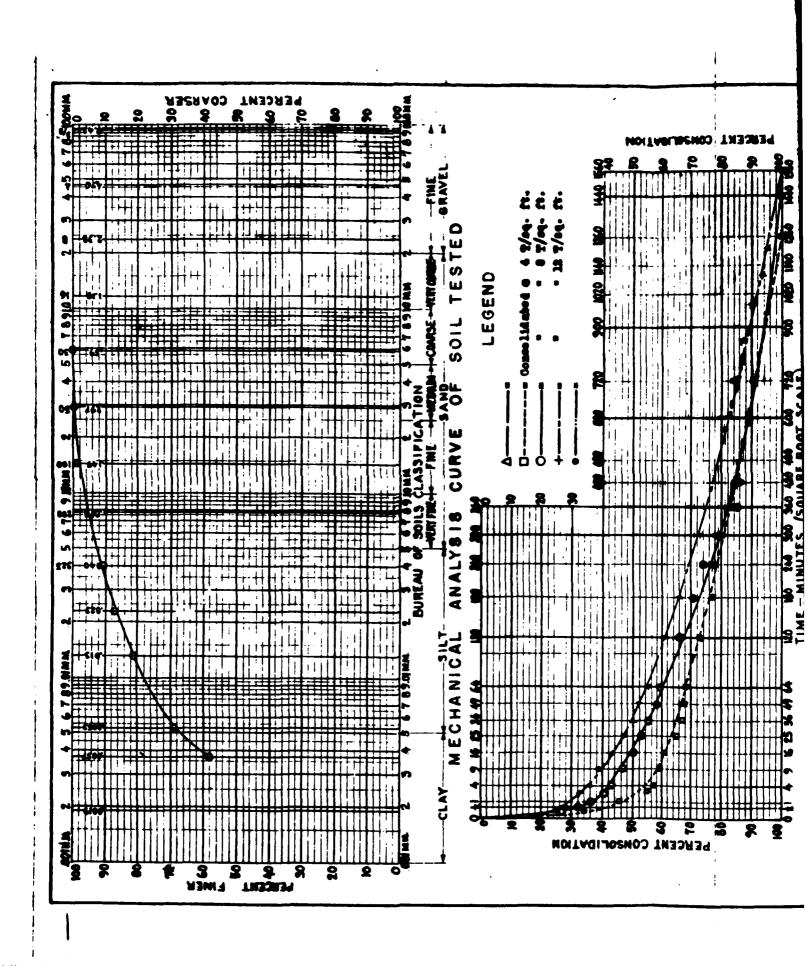
NOTES.—Except for passples I and 2 from the test short all samples were 6" drive

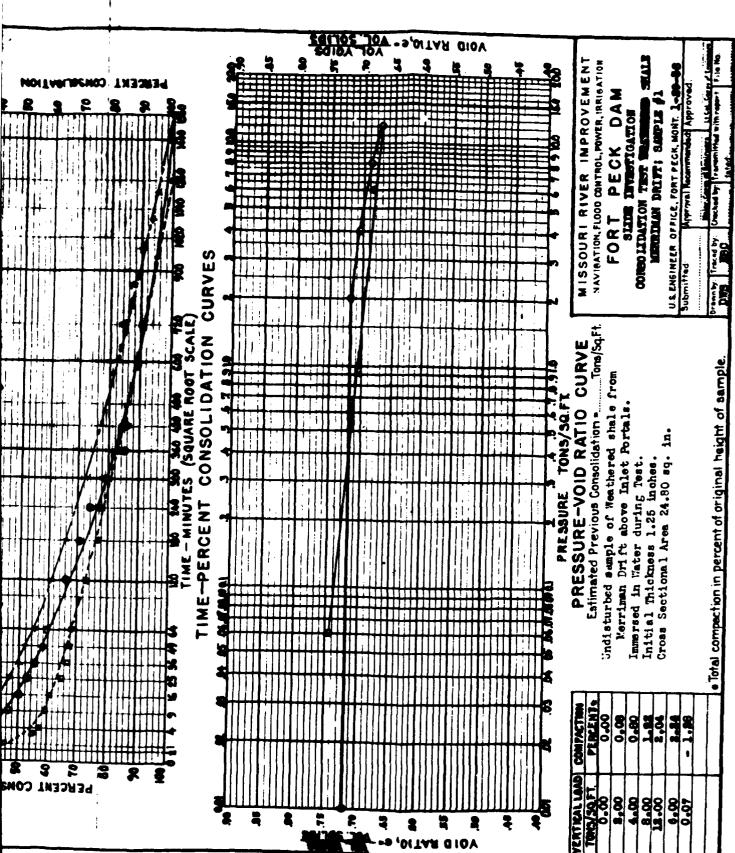
Direction of test for Quick shear varied from 1.5 to 2 minutes.
The vertical lead for the duration of the test was as judicated in Column 4.
The deal 18. Cod 28 were conflicted to the leading of the reconstruction is

For computed shearing strength for Clarici Till from Mole 8, D. 196/4. 96 coefficients









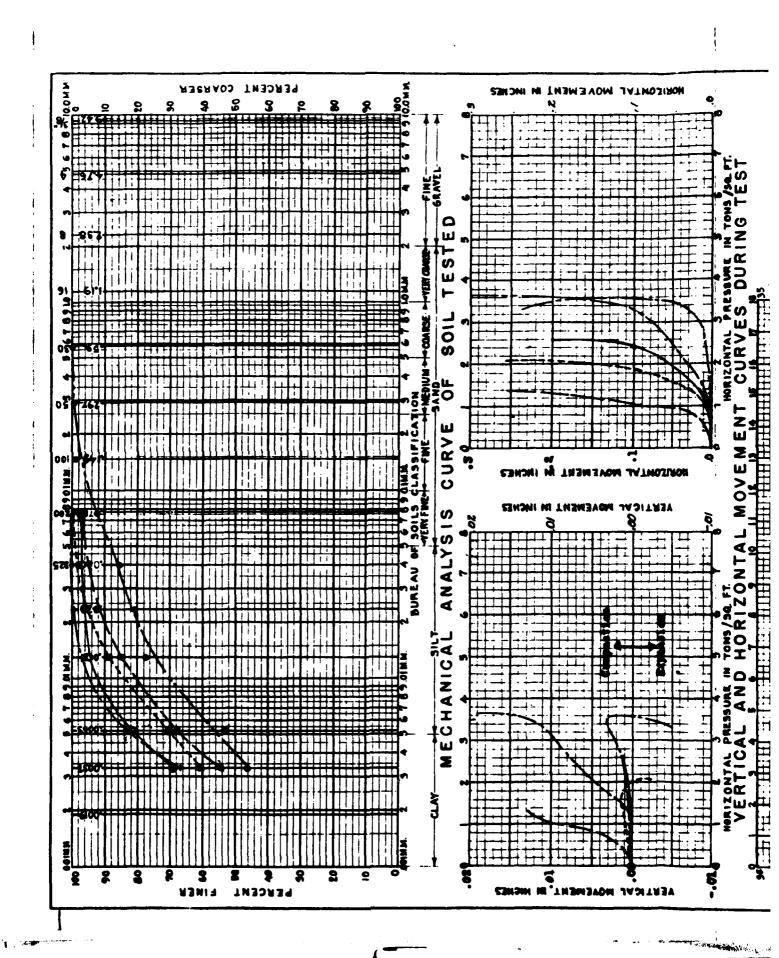
Face p. 80) No 13

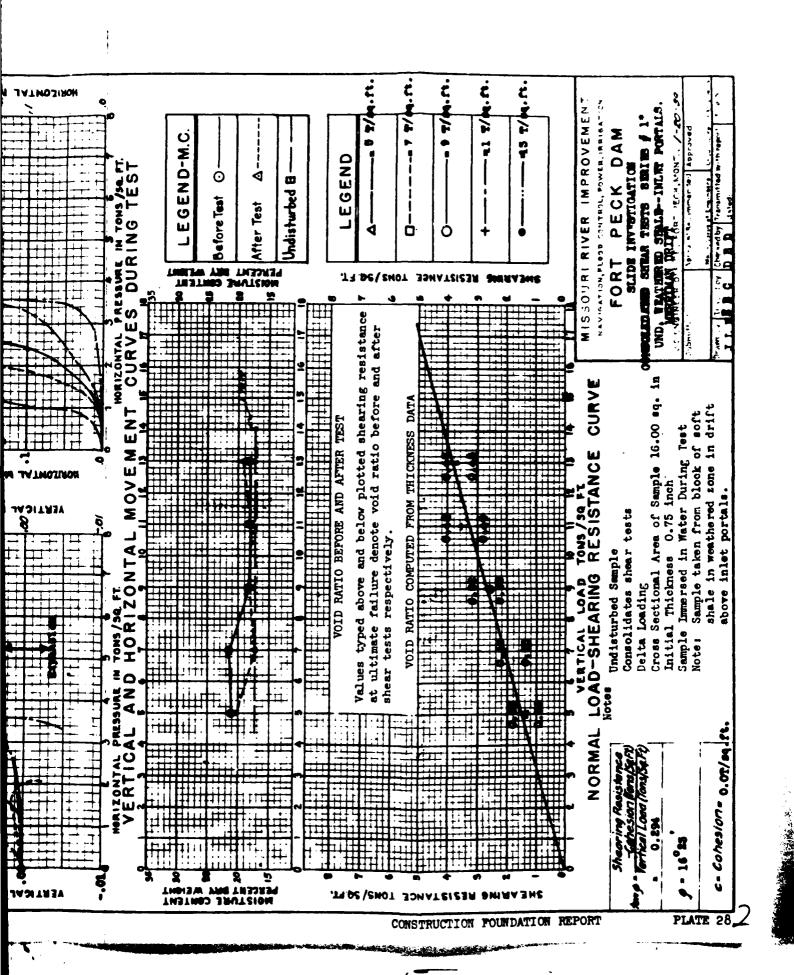
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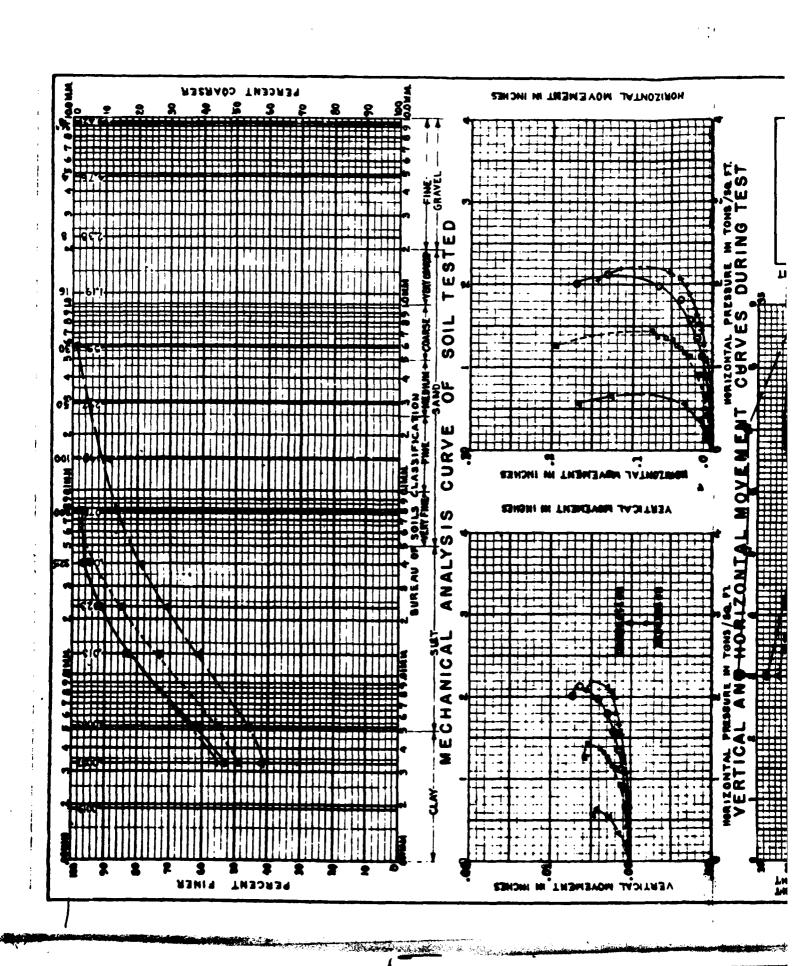
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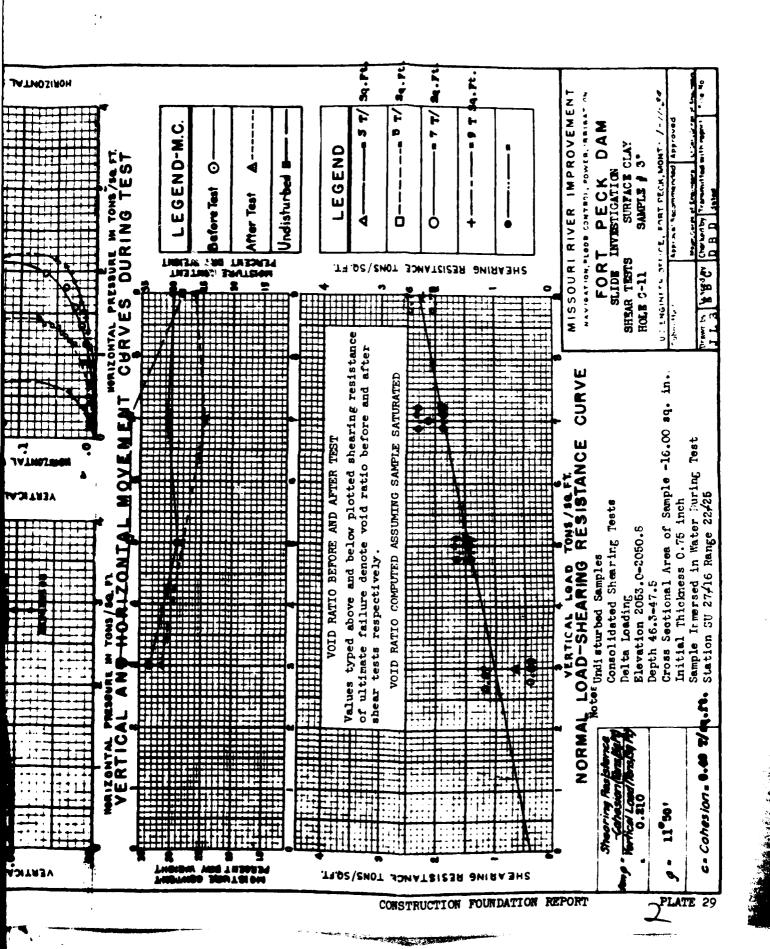
CONSTRUCTION FOUNDATION REPORT

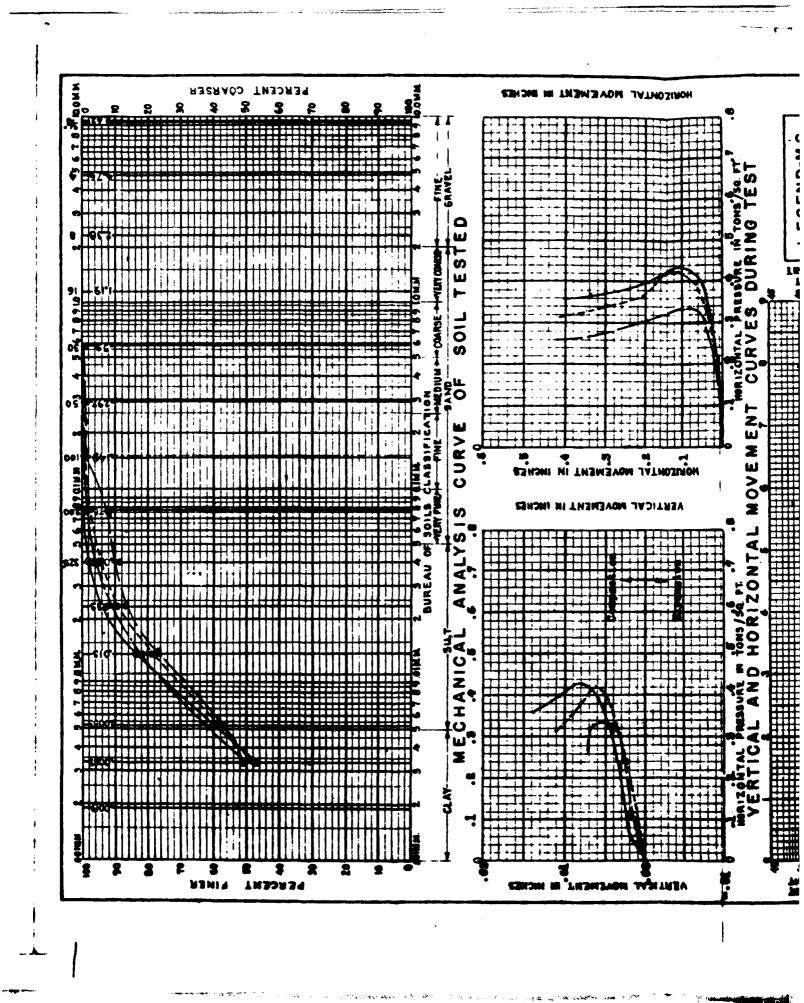
PLATE 27

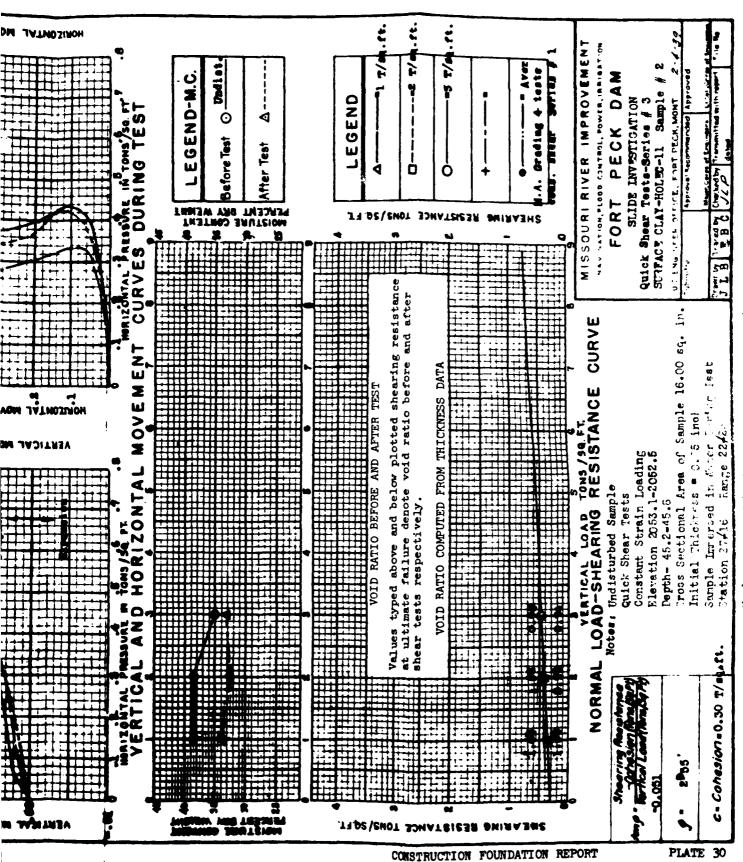






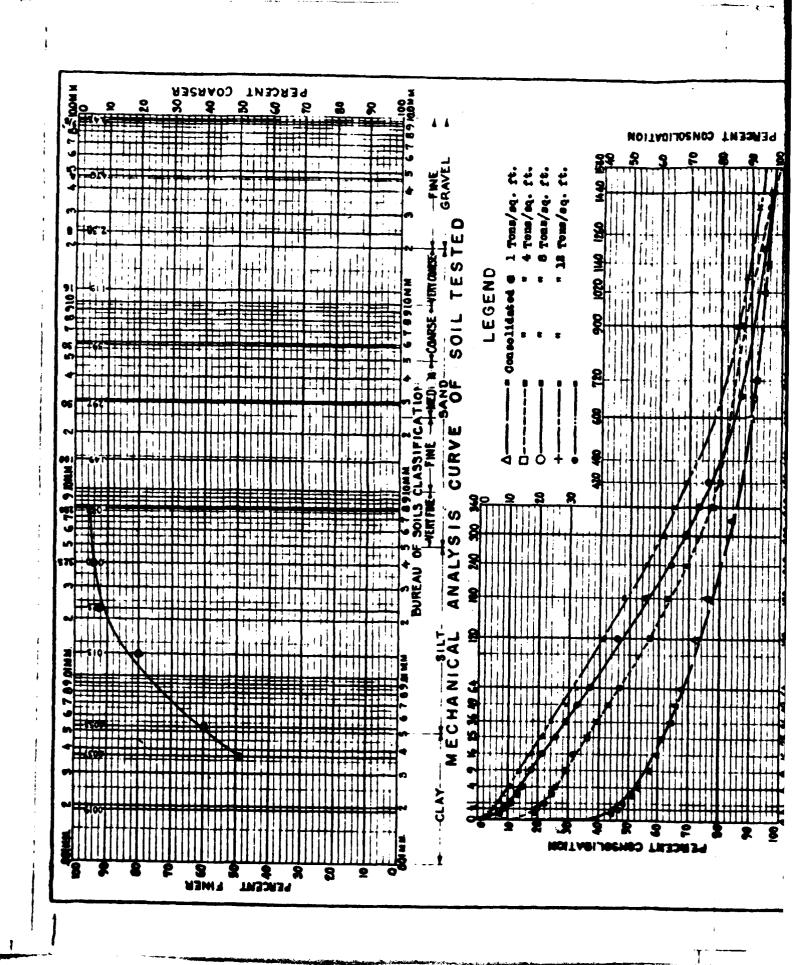


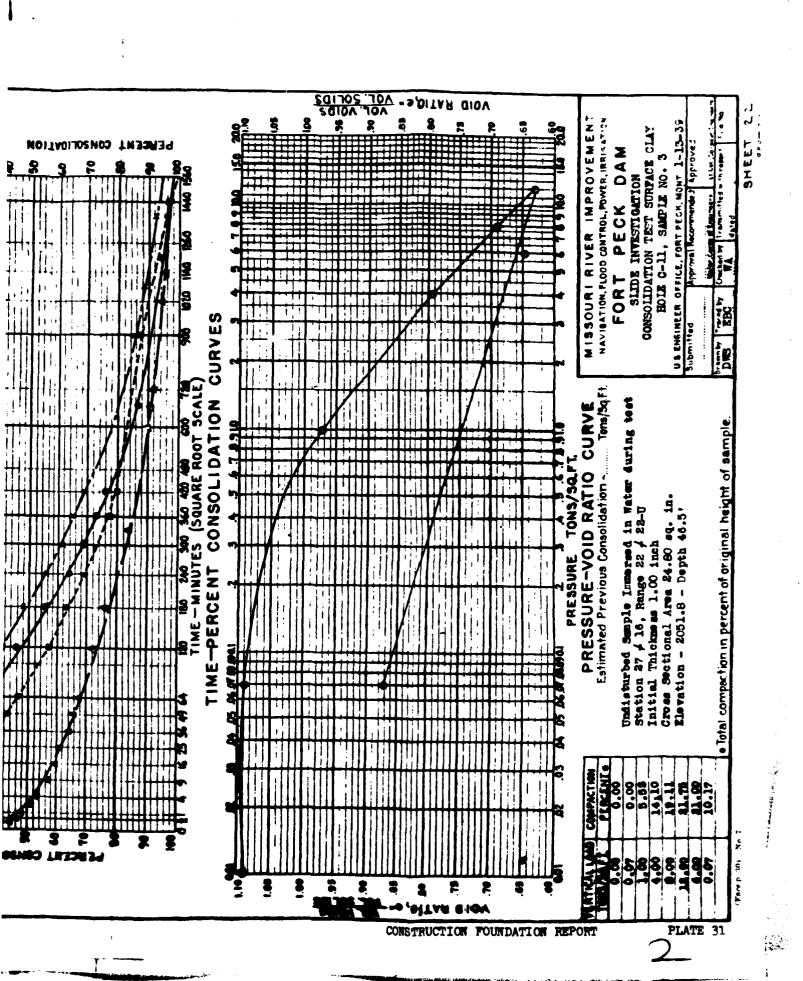


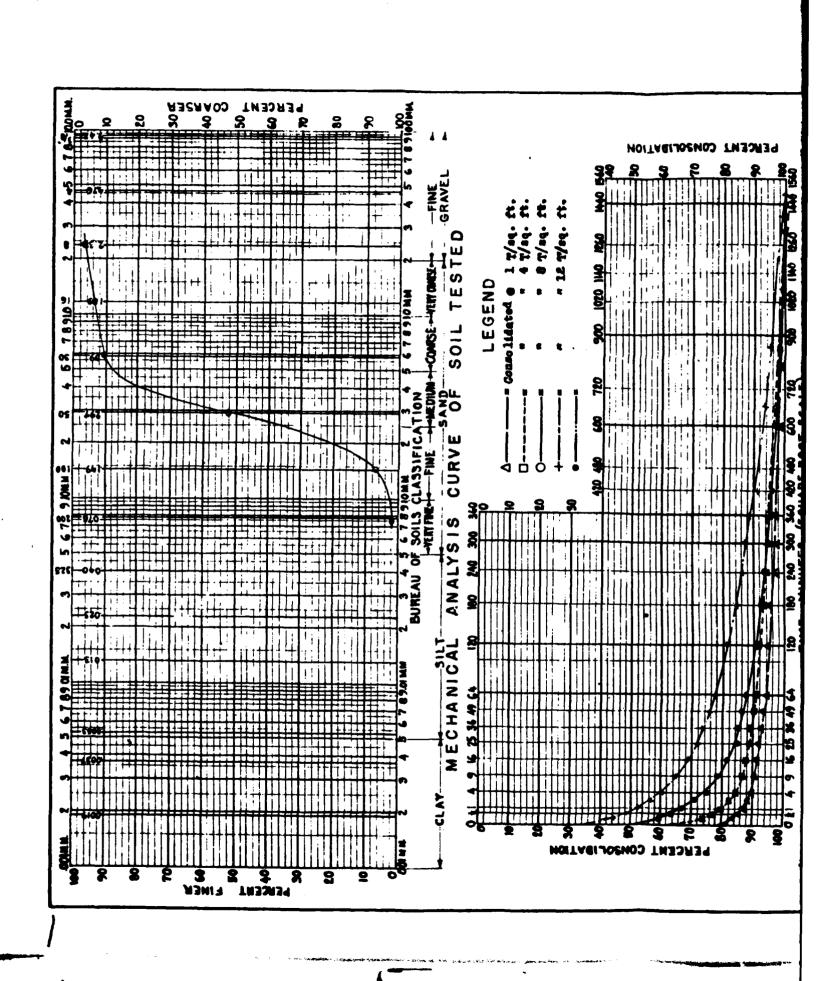


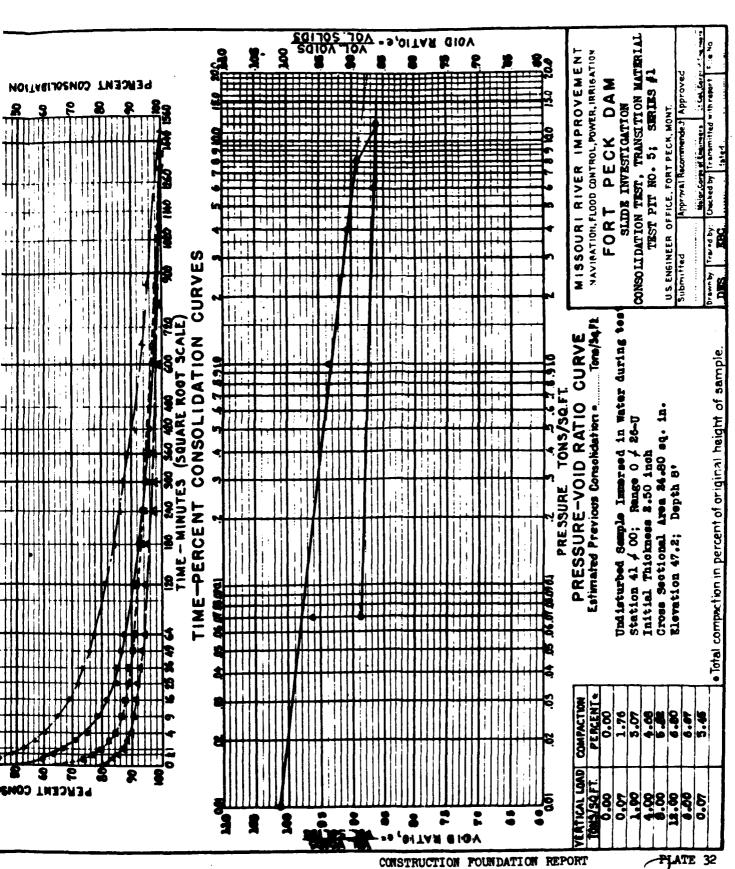
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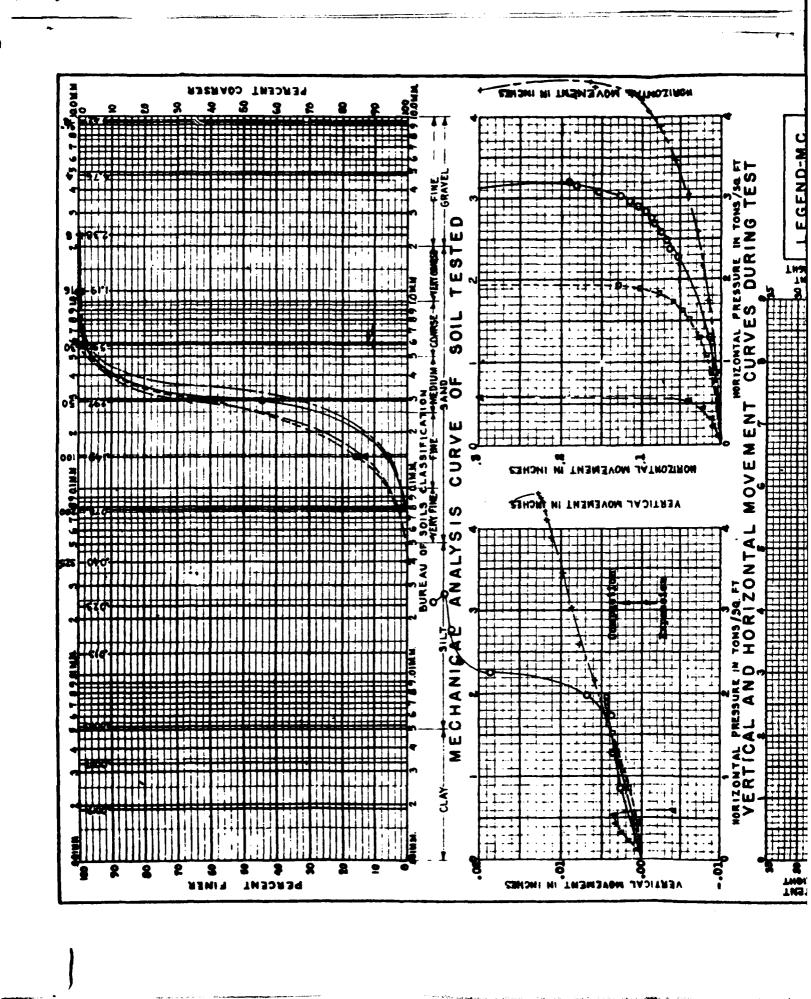
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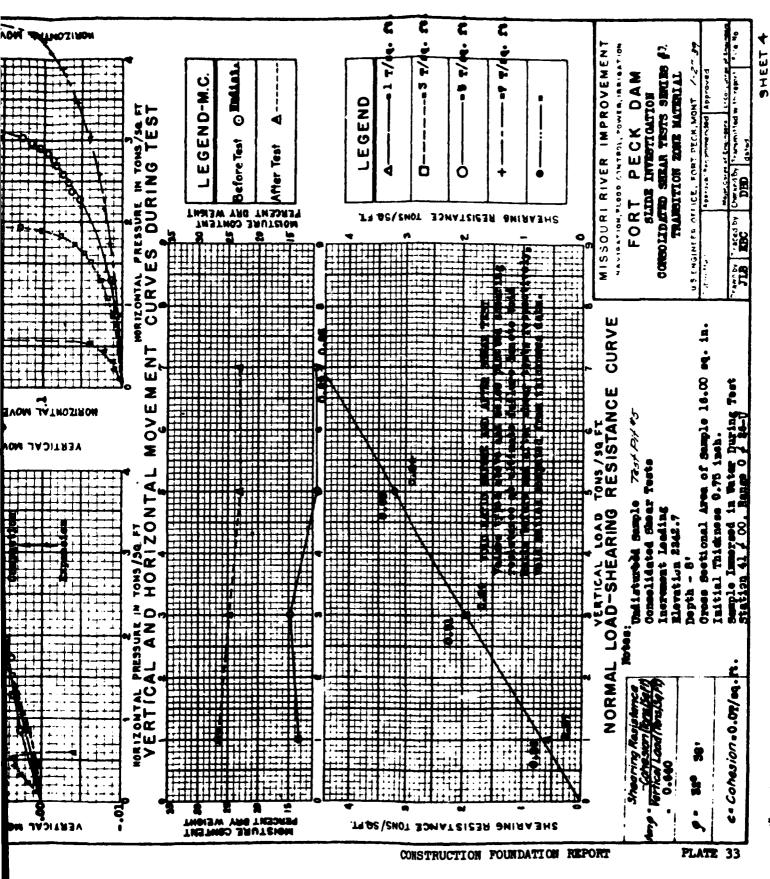








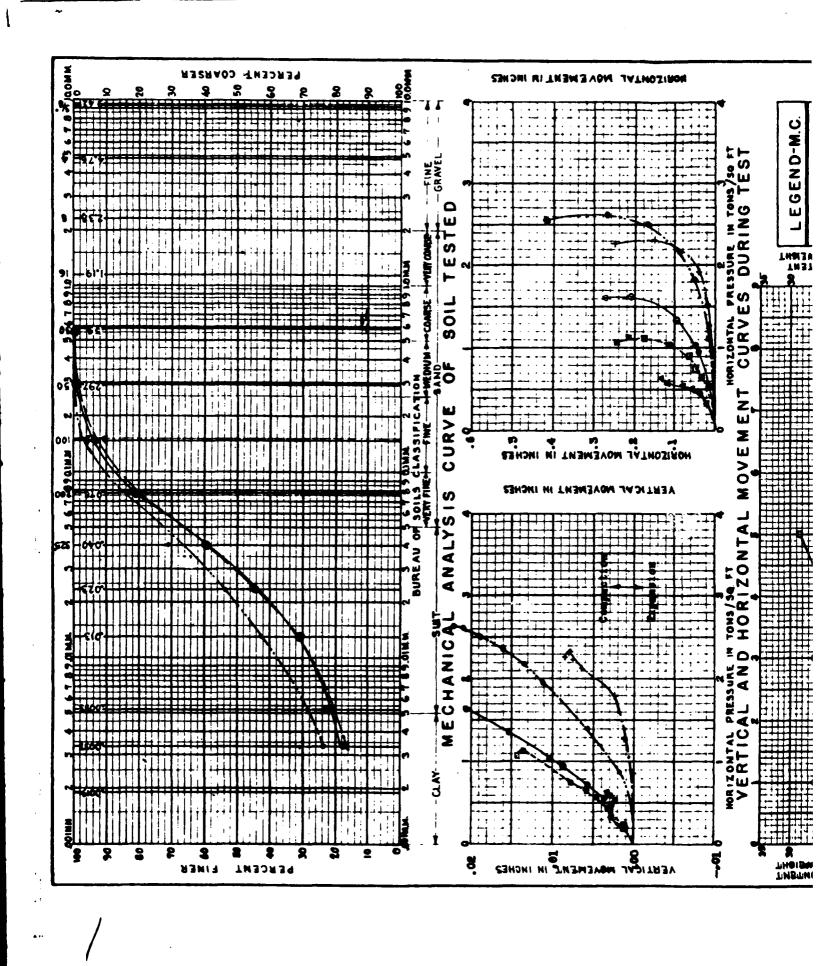


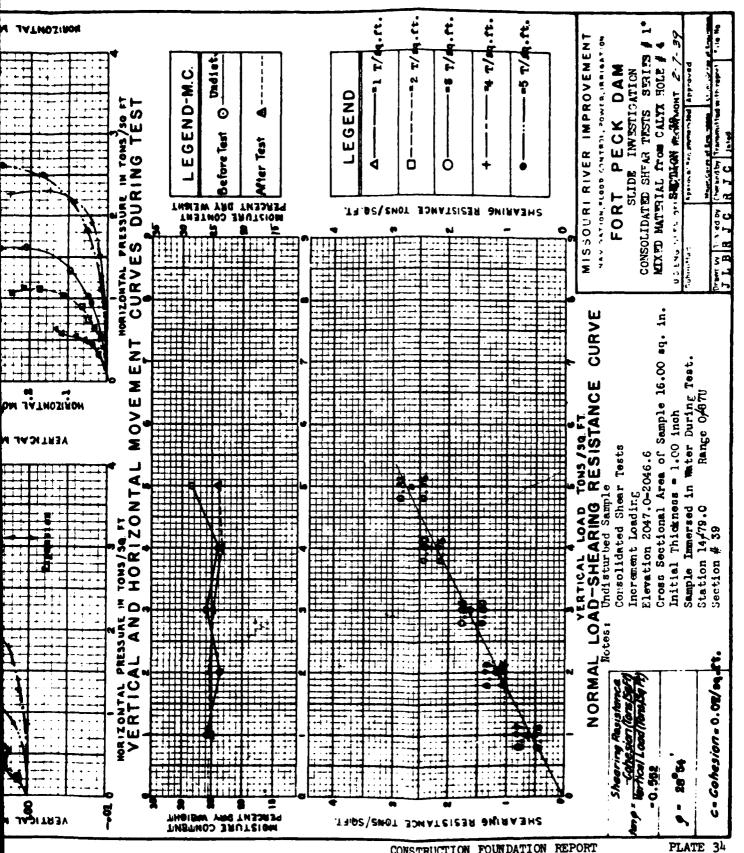


CALYX HOLE NO. 4—STATION 14+79, RANGE 0+87-U (Original sheets 2 and 3)

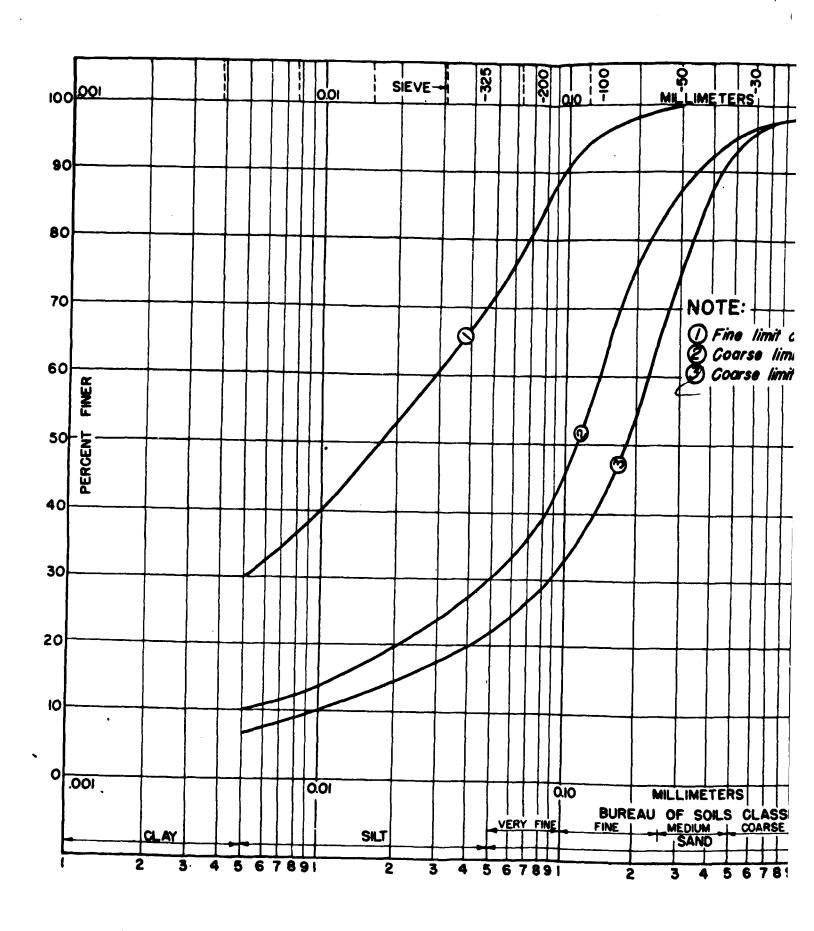
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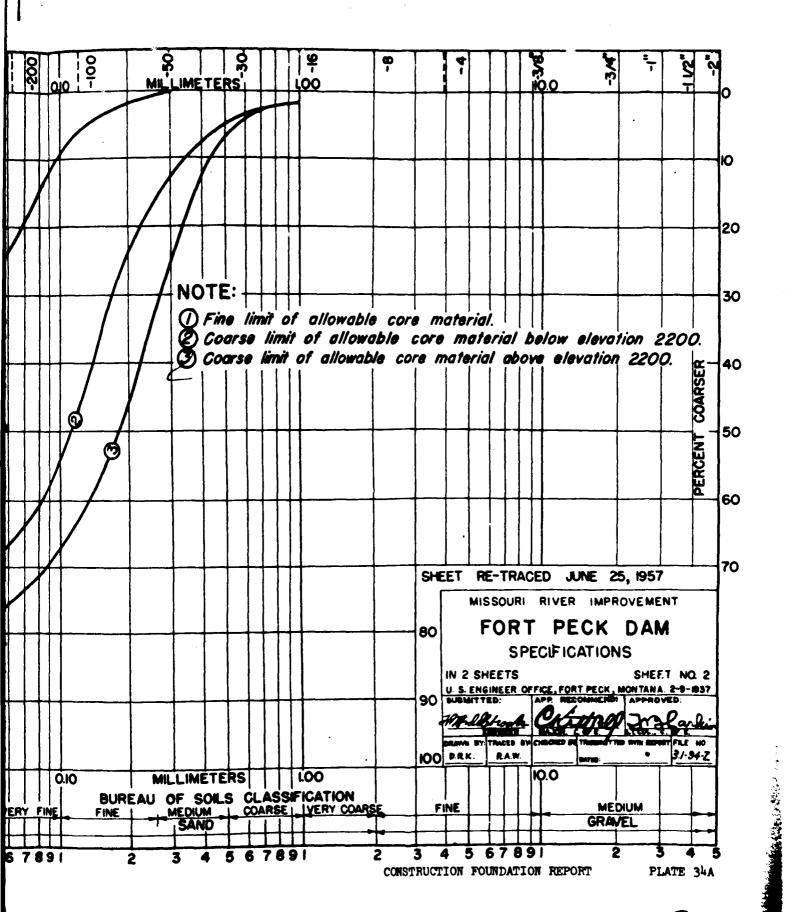
¹ First half destroyed, no sample obtained from other helf of core.

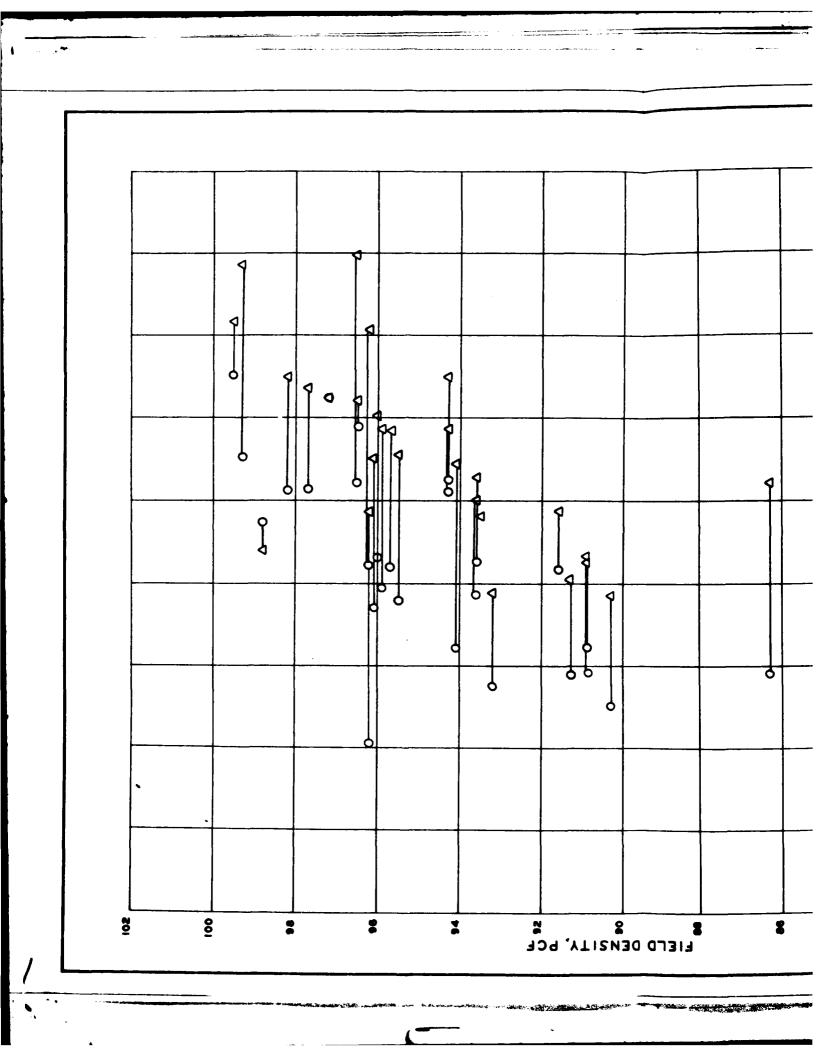




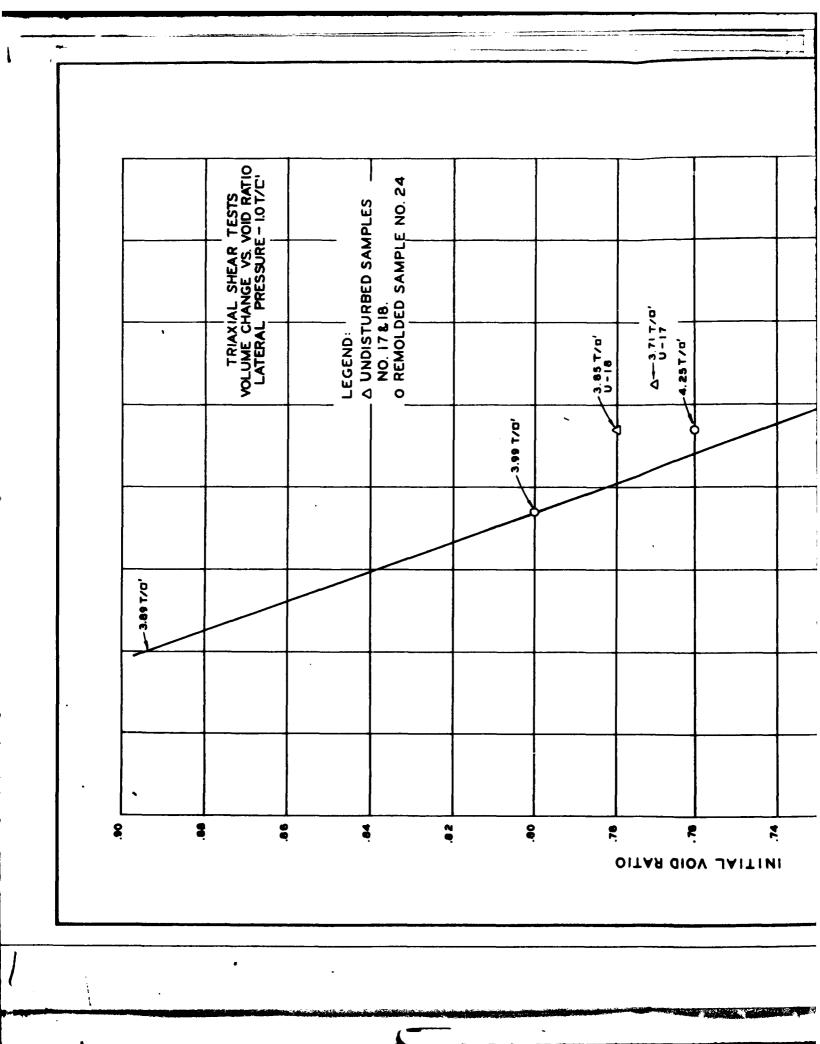
CONSTRUCTION FOUNDATION REPORT

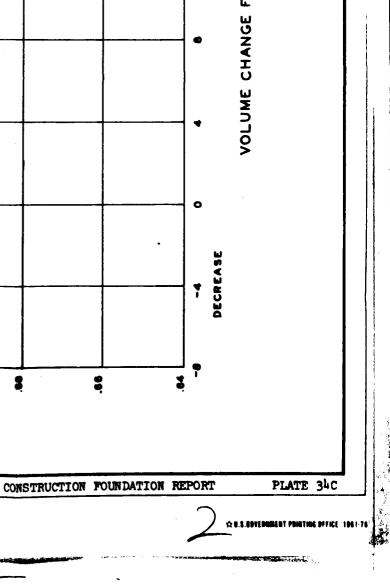


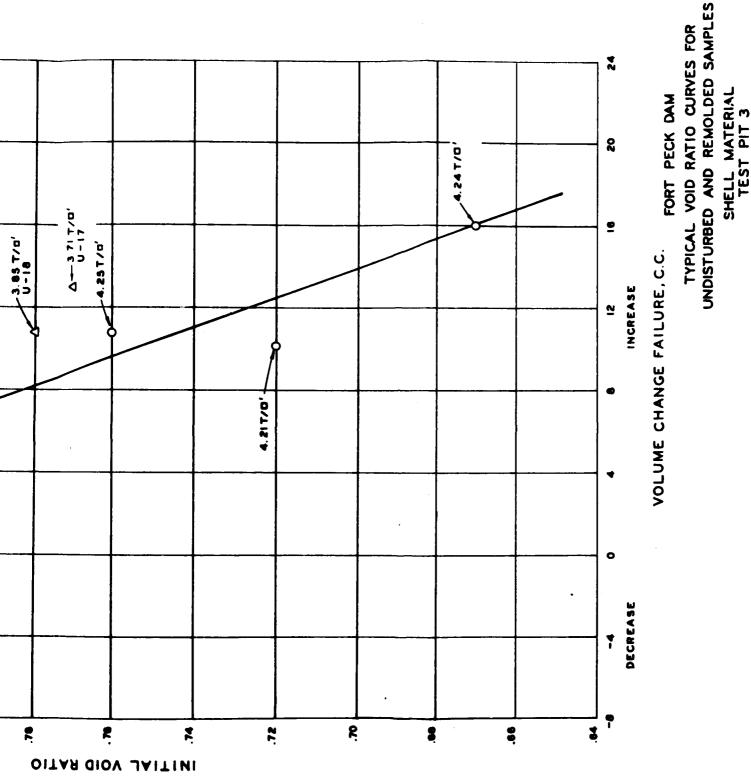


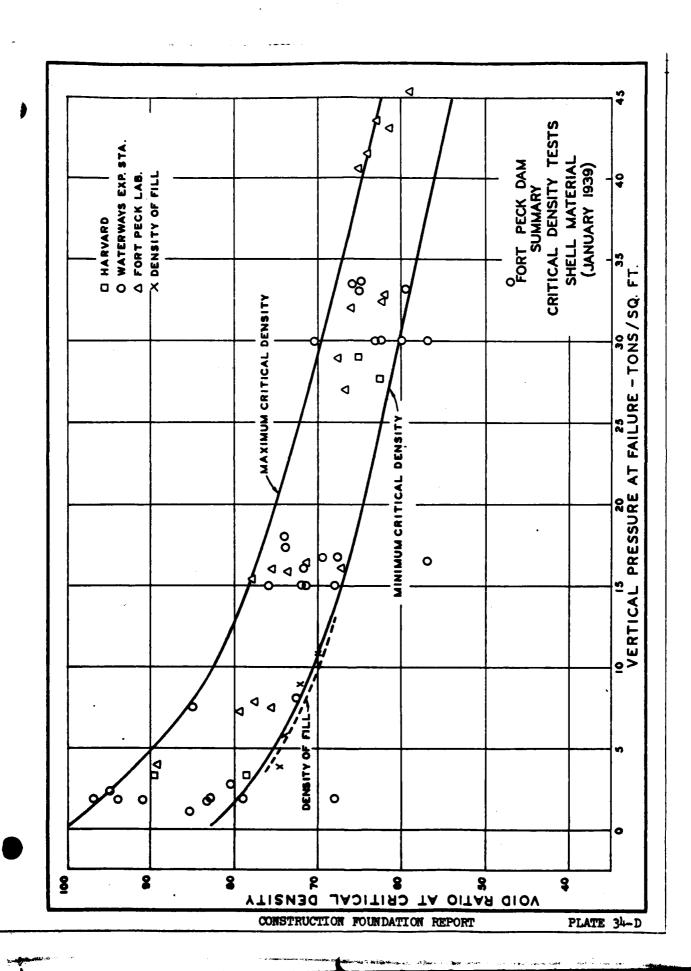


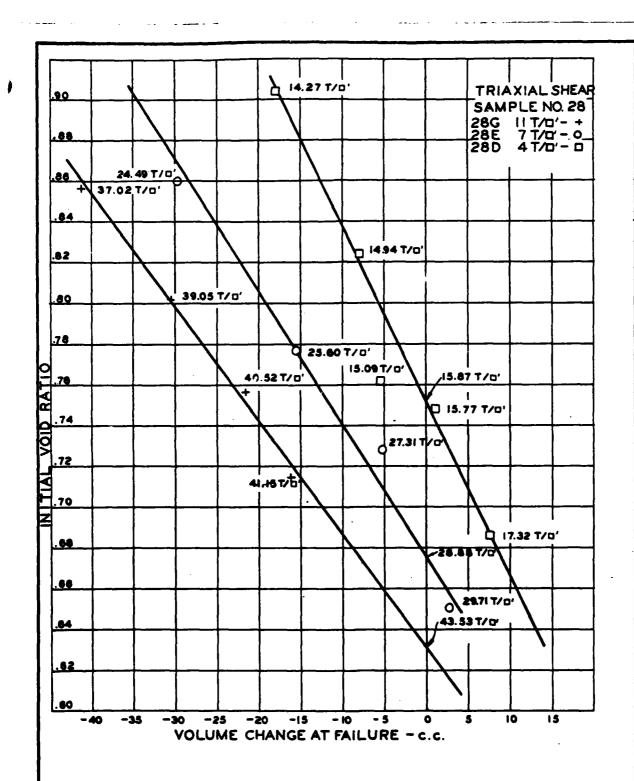
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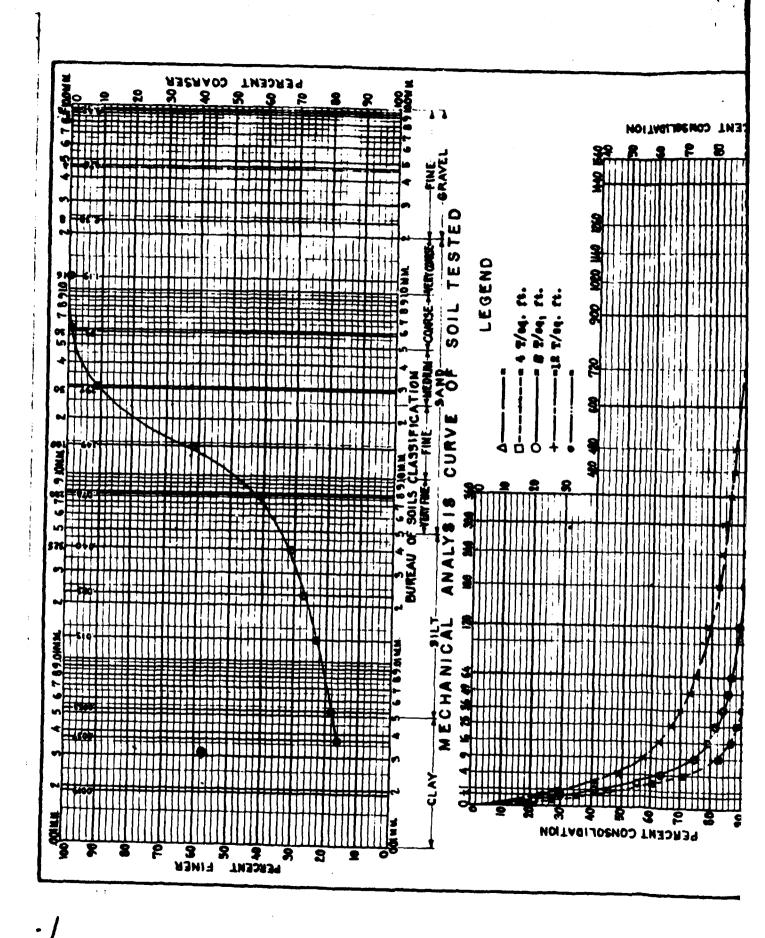




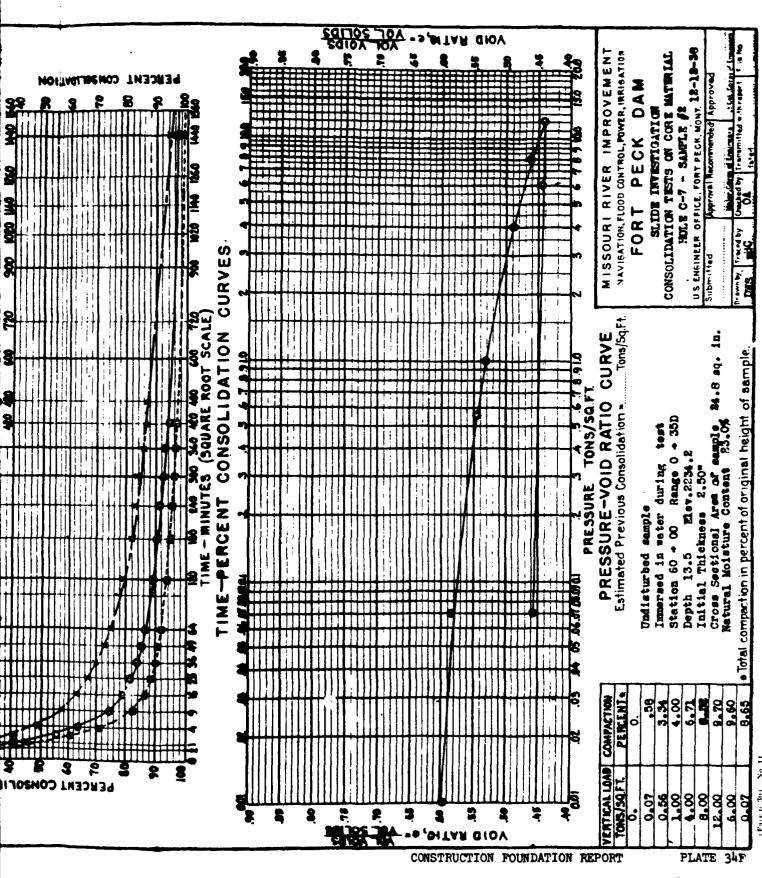
FO PECK DAM

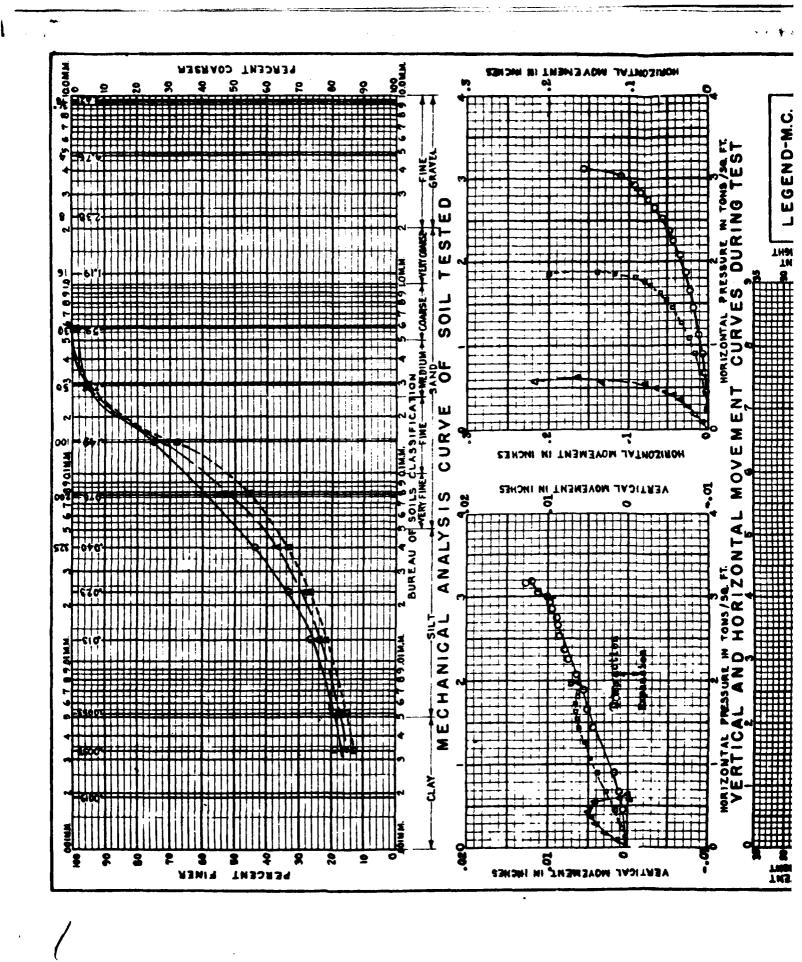
TYPICAL CRITICAL VOID RATIO TESTS

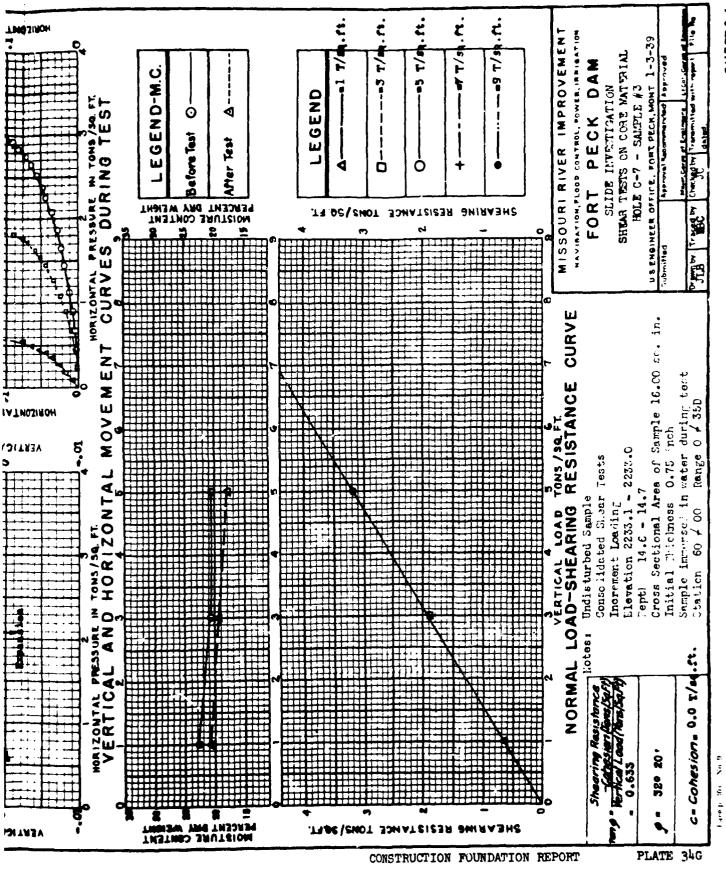
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A. GENERAL.

A comprehensive program of laboratory and field tests was made to determine the structural properties of the different types of materials in the damaged area, as well as in unaffected portions of the dam. These tests are grouped as follows:

Tests on overburden materials in the damaged

Tests on shell and transition zone materia; in unaffected portions of the dam.

Tests on typical foundation sands and clays.

Tests on core materials.

Tests on shale and bentonite.

These investigations are each discussed briefly.

1. Overburden materials in damaged area. The overburden in the damaged area included both shell and foundation sands, as well as cliuvial clays and masses of core material that became intermixed during the movement.

Mechanical analyses for classification purposes were performed on overburden samples from the churndrill holes. Overburden cores from the Calyx holes were split and photographed, and then samples for laboratory tests were cut from one of the halves. These samples, consisting of 4-inch (102 mm) cubes, were carefully selected and cut to represent typical material from each core. Tests on these included mechanical analyses, specific gravity, moisture content, and determination of the natural voids in the material. The samples were prepared in a coid-storage room, packed with dry ice to keep them frozen, and transported to the laboratory for testing.

Two series of shear tests were made on samples of overburden from Calyx hole No. 4. Plates 5-4 and 5-5 give typical results of tests on overburden materials.

2. Shell and transition-zone materials in unaffected portions of dam. Samples of typical shell materials were secured from undisturbed portions of the shell immediately west of the damaged area and from three test pits, located along the 2212 upstream berm, driven down to the saturation line.

A continuous photographic record was kept of the stratification of the material in the deepest test pit. On all samples, the tests included mechanical analyses, specific gravity, relative density (both wet and dry), and determination of natural voids. In addition, triaxial tests were made on disturbed and on several undisturbed samples of typical shell material from one of the test pits.

in order to check the results of critical-density tests performed on the triaxial shear machines, several series of direct-shear tests were also performed and critical density determined by the Taylor methodIndisturbed samples of material from the tion come between the come and the upstrawine secured from a shaft mean the wart youndamaged section. On these samples, manalyses, critical-density tests, determine natural voids, relative density tests, determined tests, and snear tests were performed. In to the physical tests, a complete mineralogic ination was made of a typical sample of sherial. Plates 5-6 through 5-13 give results on these materials.

An experimental section of hydraulic fill structed to investigate the feasibility of ing this type of material by means of catetractors. This fill was placed in 6-inch (12-inch (305 mm), 18-inch (457 mm), and (610 mm) layers to a depth of from 6 feet (1.8 feet (2.4 m). Each layer was compacted three, six, or nine passes of a 95-horsepower tor operating at half and full speed.

Continuous undisturbed samples were take test pits in each sampling area, and mechanics ysis, specific gravity, void determinations, a ative-density tests were made on each sample results on these samples are shown on Plates 5-17.

3. Foundation sends and clays. A test p driven into the flood plane downstream from the in order to secure undisturbed samples of a materials similar to the foundation materials the section of the dam affected by the earthment. A continuous photographic record was the natural strata in this pit, and mechanical ses, specific gravity, void determinations, redensity and critical-density tests were perforthly material.

Undisturbed samples of the surface clays we cured at the upstream edge of the damaged are mechanical analyses, consolidation tests, and didated-shear tests were performed on these samples 5-18 to 5-21 show the results of terfoundation sands and clays.

4. Core materials. At a selected location closure section, the undamaged core on the bank, and in the center of the silde area, (152 mm) drive samples were taken down to the of the core. Mechanical analyses, natural moderate, consolidation tests, and consolidated tests were performed on samples from 10-foot (intervals in elevation. In addition, triaxis) tests, consolidation tests, and Atterberg tests were made on samples from elevations 2 2080. The results of typical tests on core materials on Plates 5-22 to 5-24.

5. Shale and bentonite. Samples of wed

TESTS OF MATERIALS

indistances samples of material from the transition cone between the cone and the upstream shell wine secured from a shaft wear the east and of the undamaged section. On these samples, mechanical analyses, critical-density tests, determination of natural voids, relative density tests, consolidation tests, and snear tests were performed. In addition to the physical tests, a complete mineralogical examination was made of a typical sample of shell material. Plates 5-6 through 5-13 give results of tests on these materials.

An experimental section of hydraulic fill was constructed to investigate the feasibility of compacting this type of material by means of caterpillar tractors. This fill was placed in 6-inch (152 mm), 12-inch (305 mm), 18-inch (457 mm), and 24-inch (610 mm) layers to a depth of from 6 feet (1.8 m) to 3 feet (2.4 m). Each layer was compacted with three, six, or nine passes of a 95-horsepower tractor operating at half and full speed.

Continuous undisturbed samples were taken from test pits in each sampling area, and mechanical analysis, specific gravity, void determinations, and relative-density tests were made on each sample. Test results on these samples are shown on Plates 5-14 to 5-17.

3. Foundation sands and clays. A test pit was driven into the flood plane downstream from the dam, in order to secure undisturbed samples of alluvial materials similar to the foundation materials under the section of the dam affected by the earth movement. A continuous photographic record was kept of the natural strata in this pit, and mechanical analyses, specific gravity, void determinations, relative-density and critical-density tests were performed on this material.

Undisturbed samples of the surface clays were secured at the upstream edge of the damaged area, and mechanical analyses, consolidation tests, and consolidated-shear tests were performed on these samples-Plates 5-18 to 5-21 show the results of tests on foundation sands and clays-

4. Core materials. At a selected location in the closure section, it's undamaged core on the right bank, and in the center of the slide area, 6-inch (152 mm) drive samples were taken down to the base of the core. Mechanical analyses, natural moisture content, consolidation tests, and consolidated-shear tests were performed on samples from 10-foot (3.0 m) infervals in elevation. In addition, triaxial-shear tests, consolidation tests, and Atterberg limit terms were made on samples from elevations 2170 to 2080. The results of typical tests on core material and given on Plates 5-22 to 5-24.

5. Shele and bentonite. Samples of weathered

share were taken from the Calyx holes, from the Merniman drift above the inlet portals, and from several points in the damaged area, as well as from five holes and a test pit driven into the weathered shale downstream from the damaged section. Samples of fault-zone material were also secured from the Crosby drift near the shafts. Mechanical analyses, consolidation tests, and both consolidated and quick-shear tests were performed on these samples.

Samples of bentonite were secured from Calyx holes, the Merriman drift, the Crosby drift, and from exposed seams at other points on the right abutment. Both quick and consolidated-shear tests were performed on these samples. The coefficient of friction of bentonite on shale was also determined for some samples. The results of these tests are given on Plates 5-25 to 5-30.

In addition to the laboratory tests on the bentonite, a series of shear tests was made in the field on the two bentonite seams in the Merriman drift. These seams were lying approximately horizontal and were separated by 8 inches (203 mm) of shale. Both the normal loads and shearing loads were applied by means of hydraufic jacks. The center section of shale was confined by a steel jacket, to prevent its being crushed by the vertical load and to properly distribute the shearing forces.

B. EQUIPMENT AND PROCEDURE FOR LABORATORY TESTS.

- 1. Mechanical analyses. All mechanical analyses were made by the sleve and hydrometer method and were usually run wet. Samples composed of distinct-ry different types of material, such as sand with quantities of shale fragments or clay balls and clay samples mixed with gravel, were segregated and the percentage of each kind of material determined separately. These samples were run dry.
- 2. Specific-gravity determinations. Specific-gravity determinations were made on material from every sample, so that void determinations could be made more accurately. Specific-gravity determinations were made by the vacuum method on 200-gram samples.
- 3. Void determinations. For the purpose of determining the natural void ratio in undisturbed samples of materials from the shells, transition zones, foundation sands, and the experimental rolled hydraulic fill, 6-inch-diameter (152 mm) samples were taken in accurately calibrated cylinders 6 inches (152 mm) in length.

Void determinations of material from the frozen Calyx cores were made on the 4-inch (102 mm) cubes. The volume of the cubes was accurately determined by submerging them in a pan filled to the overflow with mercury and weighing the mercury displaced.

4. Relative-density tests. Relative-density tests

were performed on all undist material, transition-zone mate rial from the test pit in the dam, as well as on all samples rolled hydraulic fill. The lar density tests made it necessar c'al device for compacting + density. This apparatus consi tals, on which the tubes conta placed, the pedestals and sa and down by cams on a motor-dr mining the lowest possible deg materials were carefully depo dens through specially designed density tests were made on ea and saturated condition.

- on shell materials were performatory of the Graduate Scholarvard University, at the Wattion, Vicksburg, Miss., and a trict laboratory. Tests on a cohesionless materials were milaboratory.
- 6. Consolidation tests. All were made according to stand Fort Peck type of consolidation were all 5-5/8 inches (143 mm) of transition-zone material assumples of core material were in thickness, while samples of rials, such as clays and a 1.0 inch (25 mm) or 1-1/4 inches

Consolidation of core and samples prior to making shear in consolidation devices, although the same dated directly in the shear box

7. Shear tests. Consolld transition-zone material, when the tests on core material were made in the while the direct-shear tests tests on core material were material were machine. All quick in the Zanesville-type shear test samples were 4 inches 3/4-inch (10 mm) thick.

Consolidated shear tests were identing the sample to the desiing the shearing loads in incrtil movement ceased before a increments. Quick-shear test: stant strain loading, the load uously, so that failure or minutes after start of the test

each from the Tallyx halles, from the Mermove the inlet pontals, and from severthe damaged area, as well as from five test pit driven into the weathered ream from the damaged section. Samples ne material were also secured from the near the shafts. Mechanical analyses, tests, and both consolldated and tests were performed on these samples. bentonite were secured from Calyx Merriman drift, the Grosby drift, and seams at other points on the right Both quick and consolidated-shear tests med on these samples. The coefficient bentonite on shale was also deterome samples. The results of these tests Plates 5-25 to 5-30.

on to the laboratory tests on the bentones of shear tests was made in the field bentonite seams in the Merriman drift, were lying approximately horizontal and ted by 3 inches (203 mm) of shale. Both loads and shearing loads were applied by ydrautic jacks. The center section of confined by a steel jacket, to prevent rushed by the vertical load and to propoute the shearing forces.

NT AND PROCEDURE FOR LABORATORY TESTS.

Icat analyses. All mechanical analyses by the sleve and hydrometer method and y run wet. Samples composed of distinction types of material, such as sand with of shale fragments or clay balls and s mixed with gravel, were segregated and age of each kind of material determined

These samples were run dry.

Ic-gravity determinations. Specificterminations were made on material from the, so that void determinations could be accurately. Specific-gravity determinamade by the vacuum method on 200-gram

natural void ratio in undisturbed sammaterials from the shells, transition undation sands, and the experimental traulic fill, 6-inch-diameter (152 mm) re taken in accurately calibrated cylines (152 mm) in length.

erminations of material from the frozen were made on the 4-inch (102 mm) cubes of the cubes was accurately determined ing them in a pan filled to the overflowry and weighing the mercury displaced.

The density tests. Relative—density tests.

were performed on all undisturbed samples of shell material, transition-zone material, and sandy material from the test pit in the flood plane below the dam, as well as on all samples from the experimental rolled hydraulic fill. The large number of relativedensity tests made it necessary to construct a spac'al device for compacting the samples to maximum density. This apparatus consisted of several pedestals, on which the tubes containing the samples were placed, the pedestals and samples being jarred up and down by cams on a motor-driven shaft. For determining the lowest possible degree of compaction, the materials were carefully deposited in glass cylinders through specially designed funnels. Relativedensity tests were made on each sample in both dry and saturated condition.

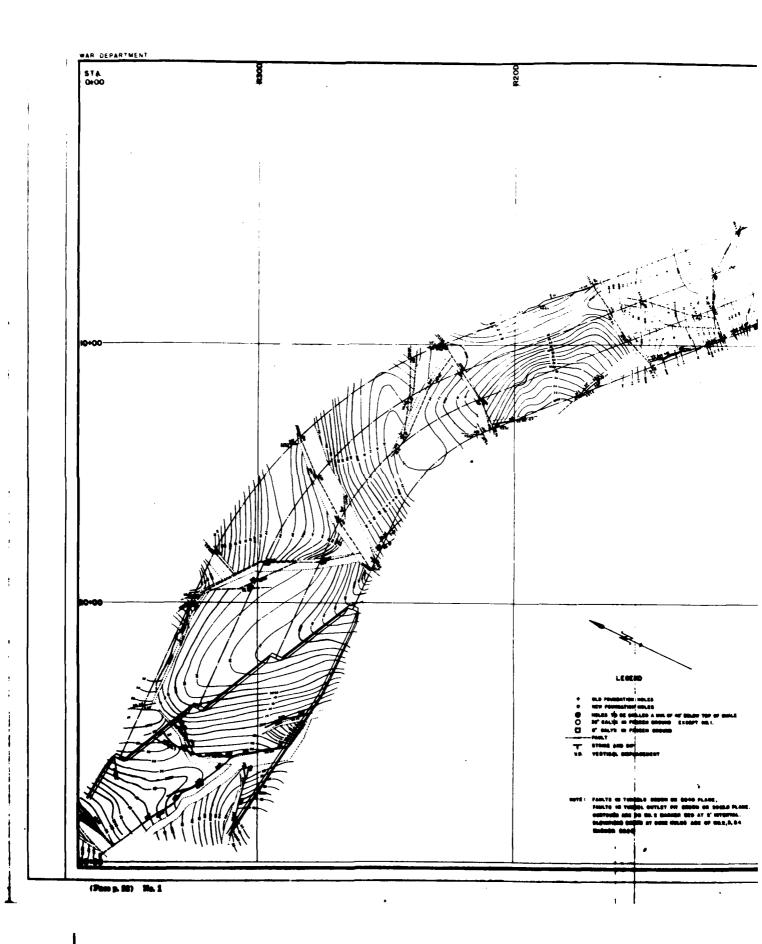
5. Critical-density tests. Critical-density tests on shell materials were performed in the soils laboratory of the Graduate School of Engineering of Harvard University, at the Waterways Experiment Station, Vicksburg, Miss., and at the Fort Peck District laboratory. Tests on undisturbed samples of cohesionless materials were made at the Fort Peck laboratory.

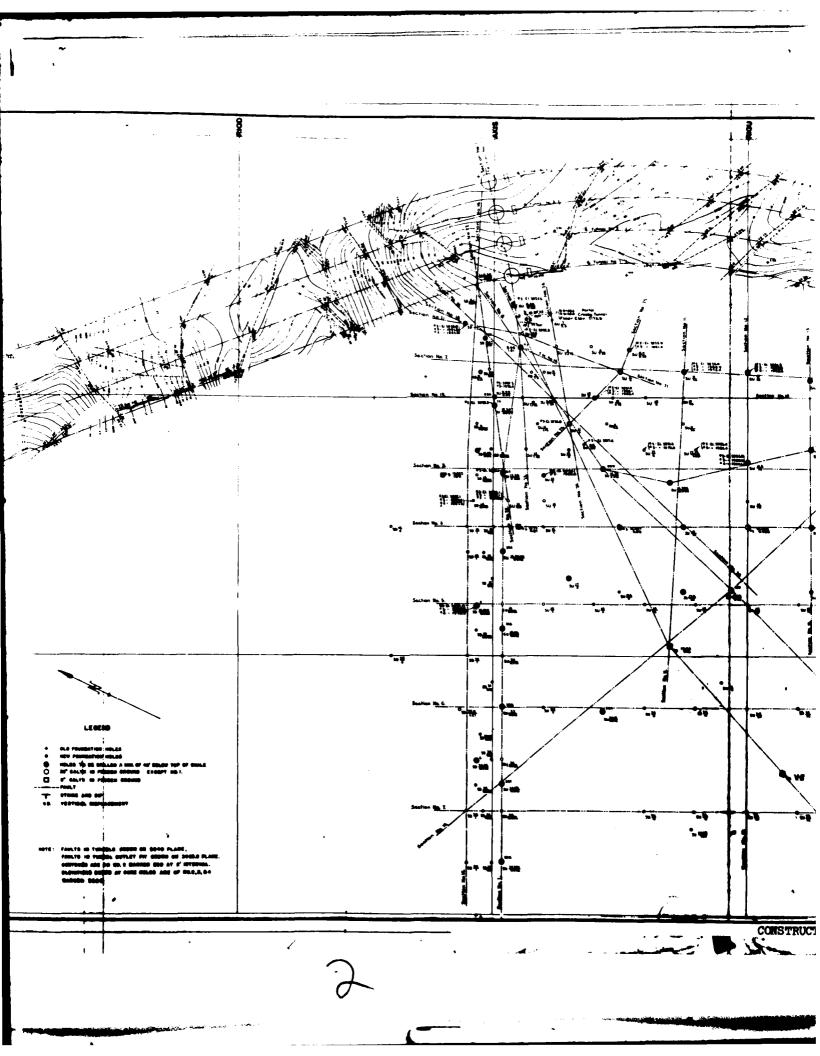
6. Consolidation tests. All consolidation tests were made according to standard procedure in the Fort Peck type of consolidation equipment. Samples were all 5-5/8 inches (143 mm) in diameter. Samples of transition-zone material and the more pervious samples of core material were 2-1/2 inches (64 mm) in thickness, while samples of very impervious materials, such as clays and weathered shale, were 1.0 inch (25 mm) or 1-1/4 inches (32 mm) thick.

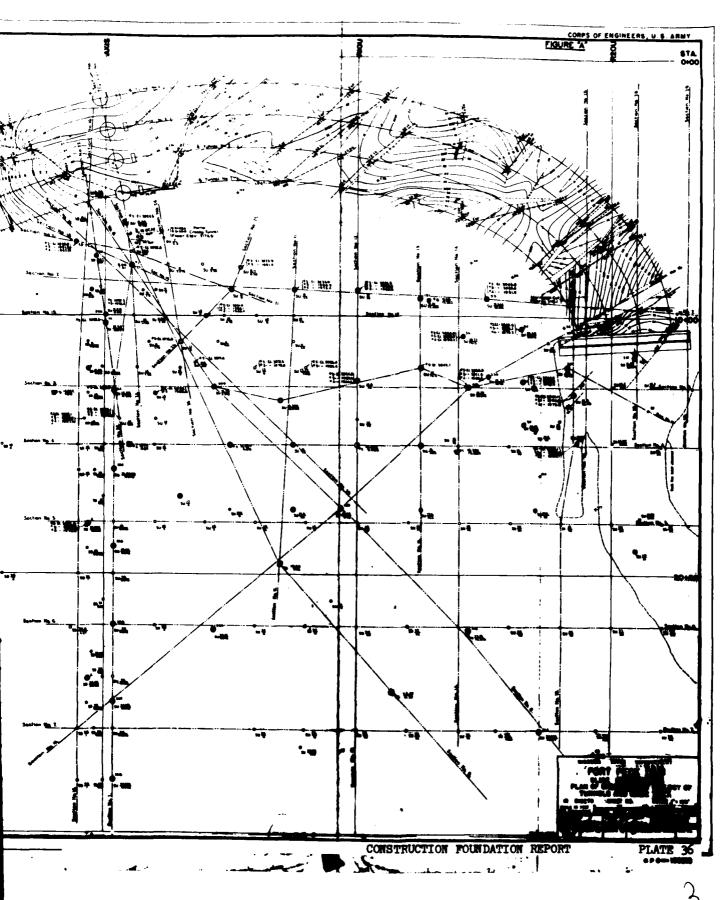
Consolidation of core and a few weathered-shale samples prior to making shear tests was accomplished in consolidation devices, although most of the bentonite and weather-shale samples were preconsolidated directly in the shear boxes.

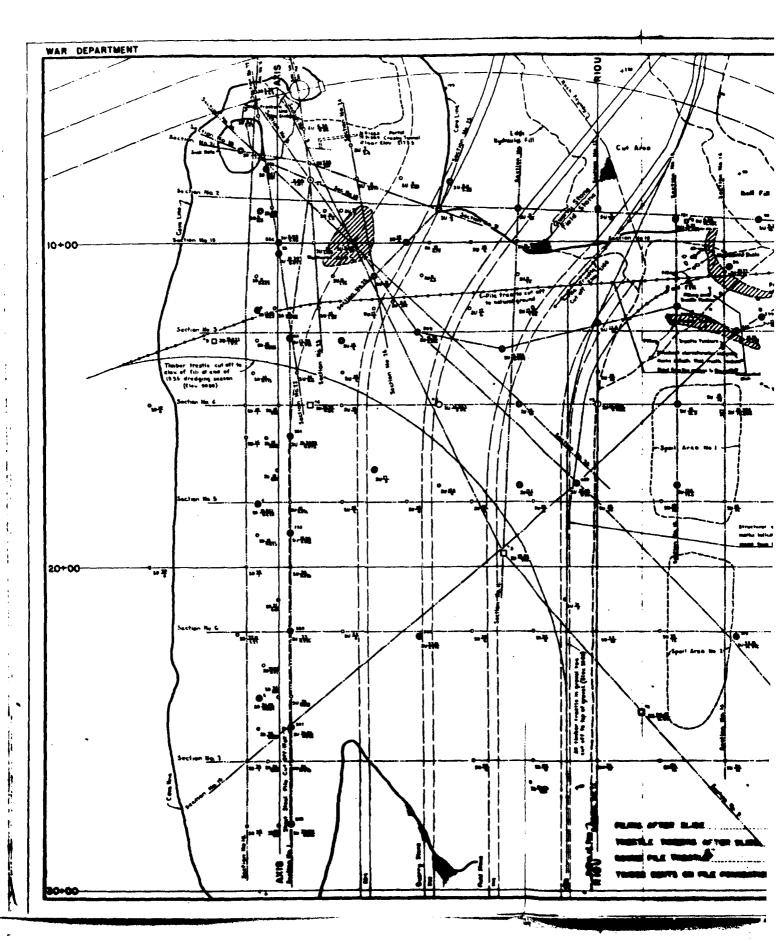
7. Shear tests. Consolidated-shear tests on transition-zone material, weathered shale and bentonite were made in the M.I.T. shear machine, while the direct-shear tests on shell material and tests on core material were made in the Zanesville-type shear machine. All quick-shear tests were made in the Zanesville-type shear machine. The (shear test samples were 4 inches (102 mm) square and 3/4-inch (10 mm) thick.

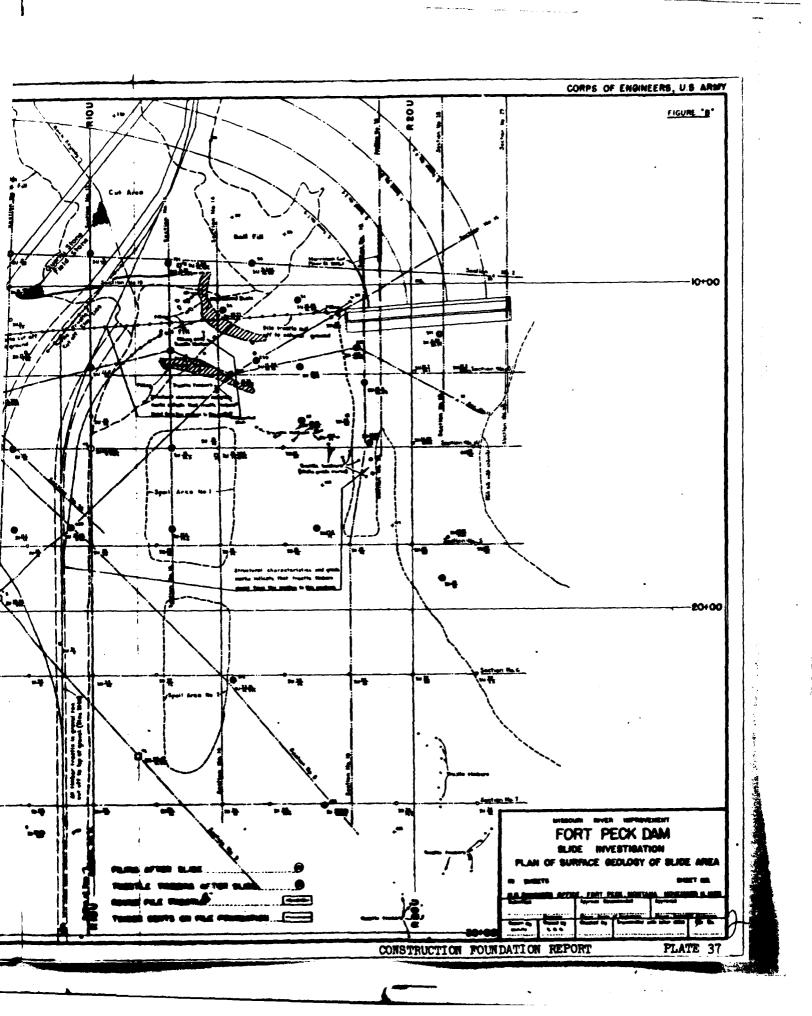
Consolidated shear tests were made by first consolidating the sample to the desired load and then adding the shearing loads in increments and waiting until movement ceased before adding additional load increments. Quick-shear tests were made with constant strain loading, the load being applied continuously, so that failure occurred within a few minutes after start of the test.

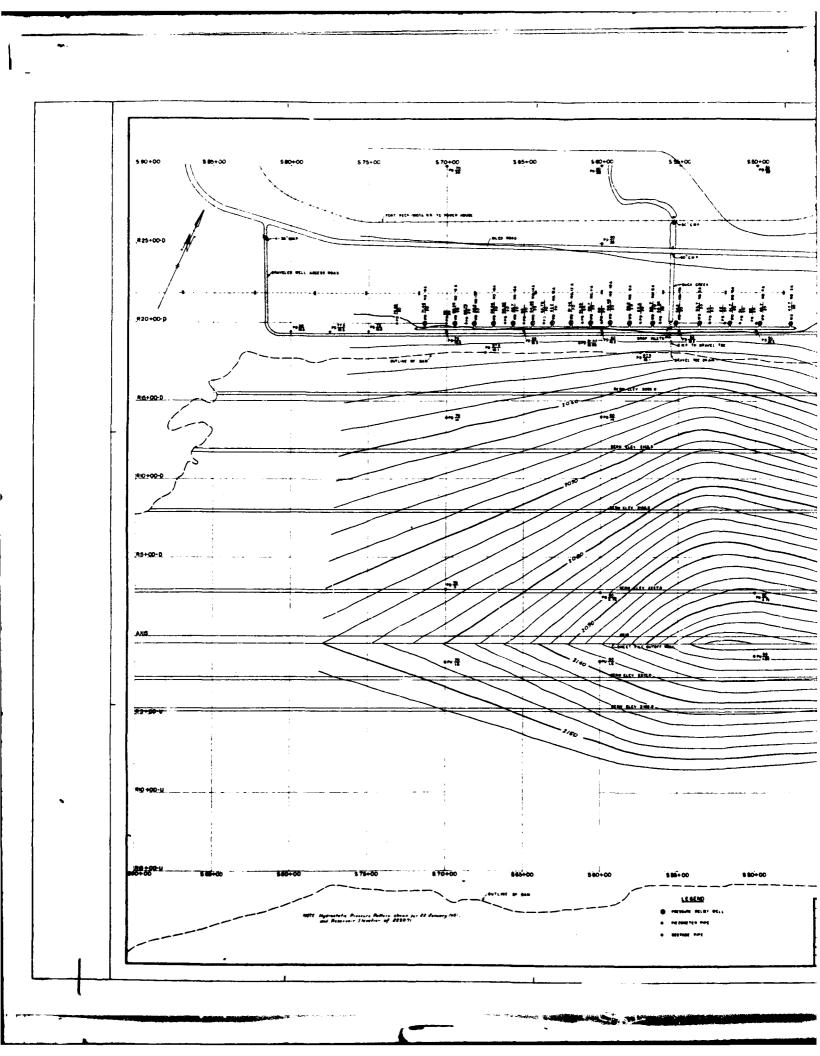


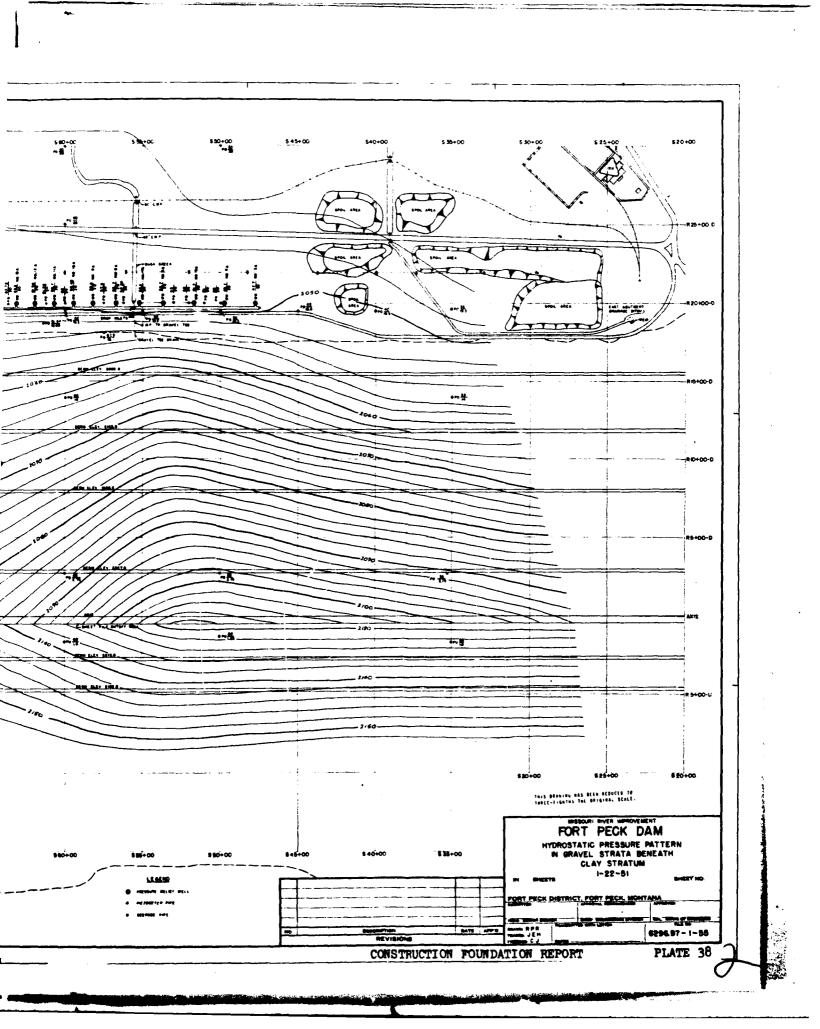




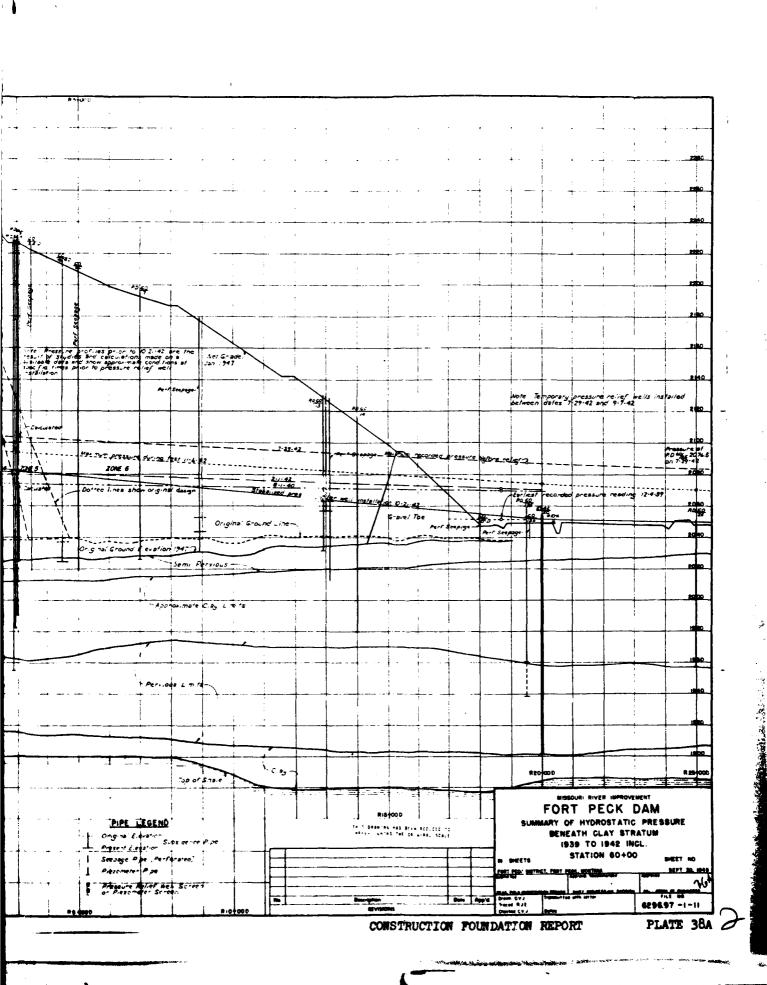


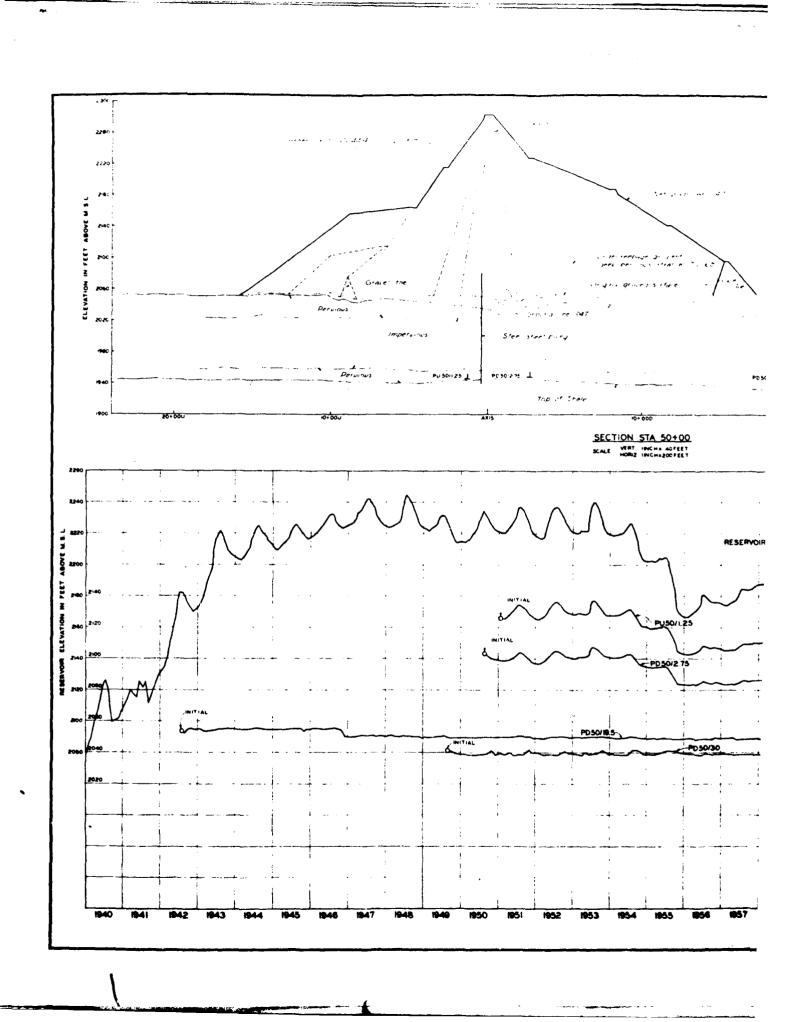






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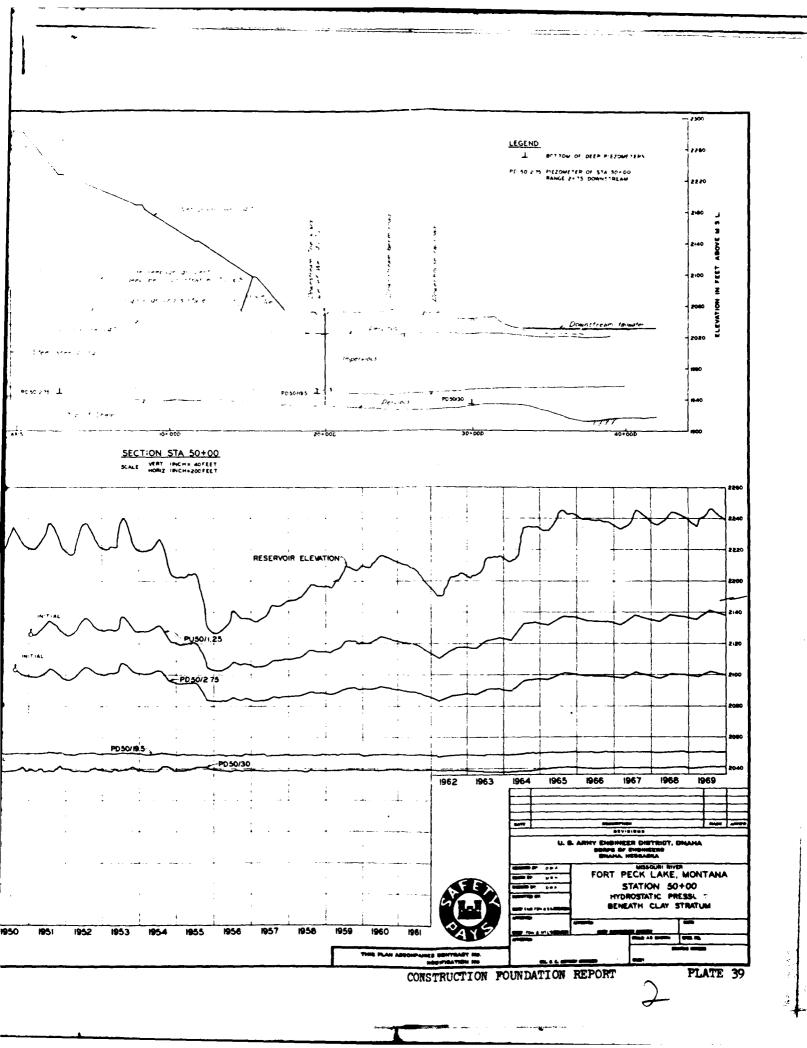


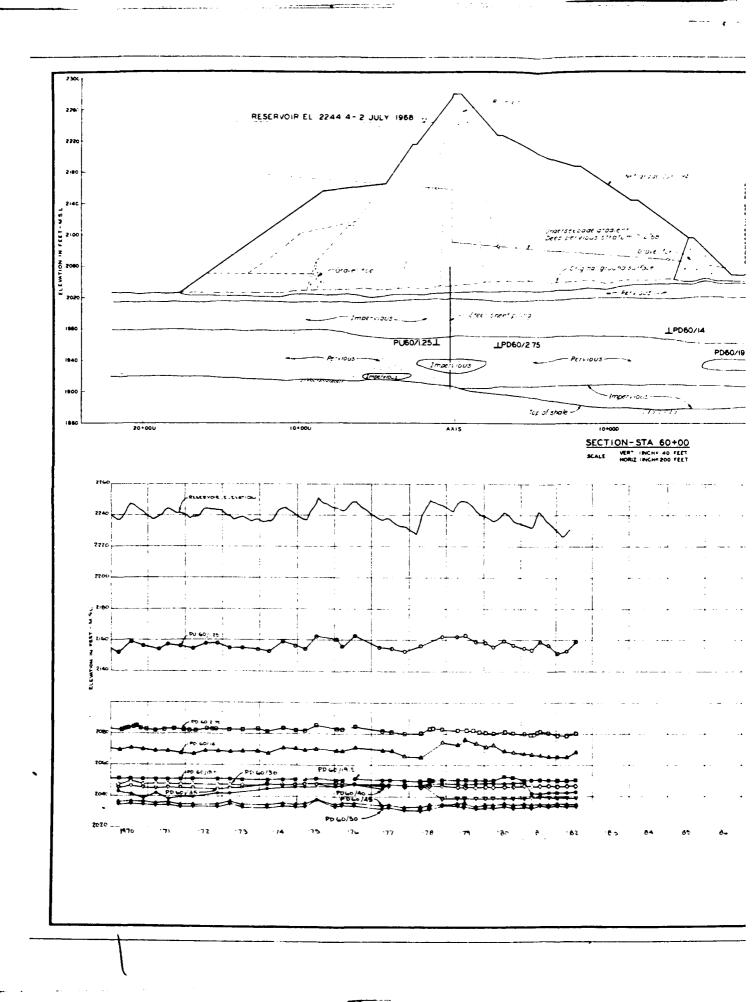


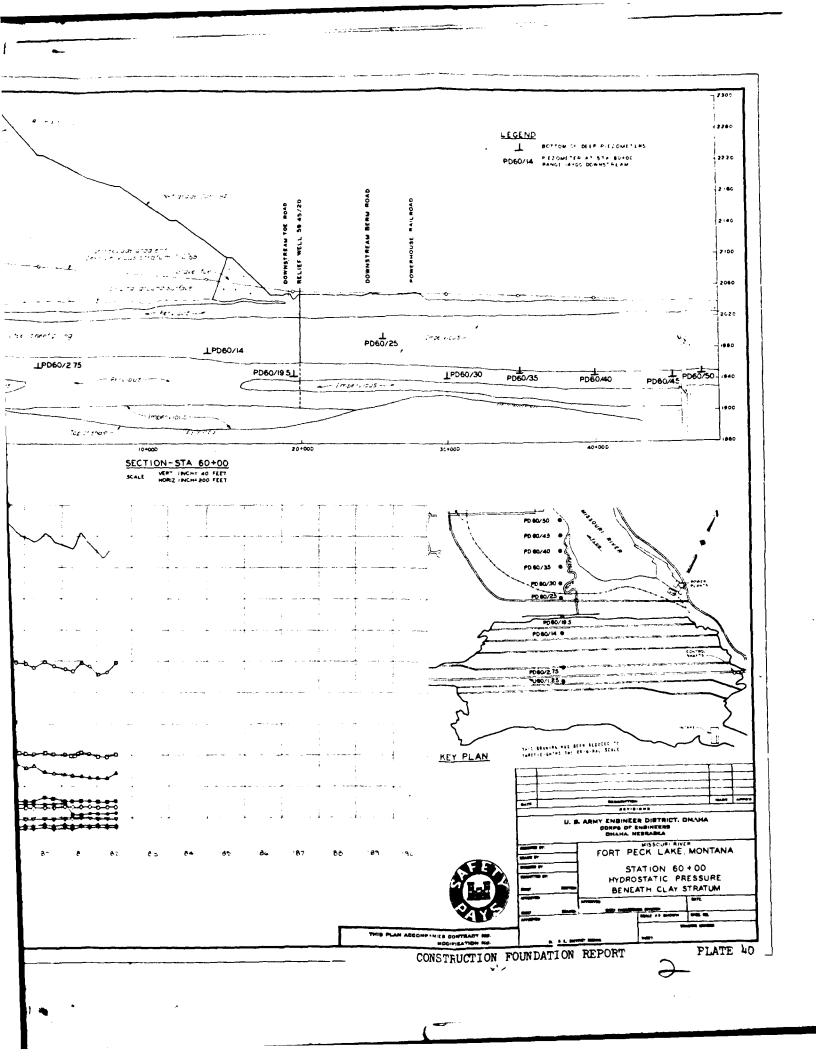
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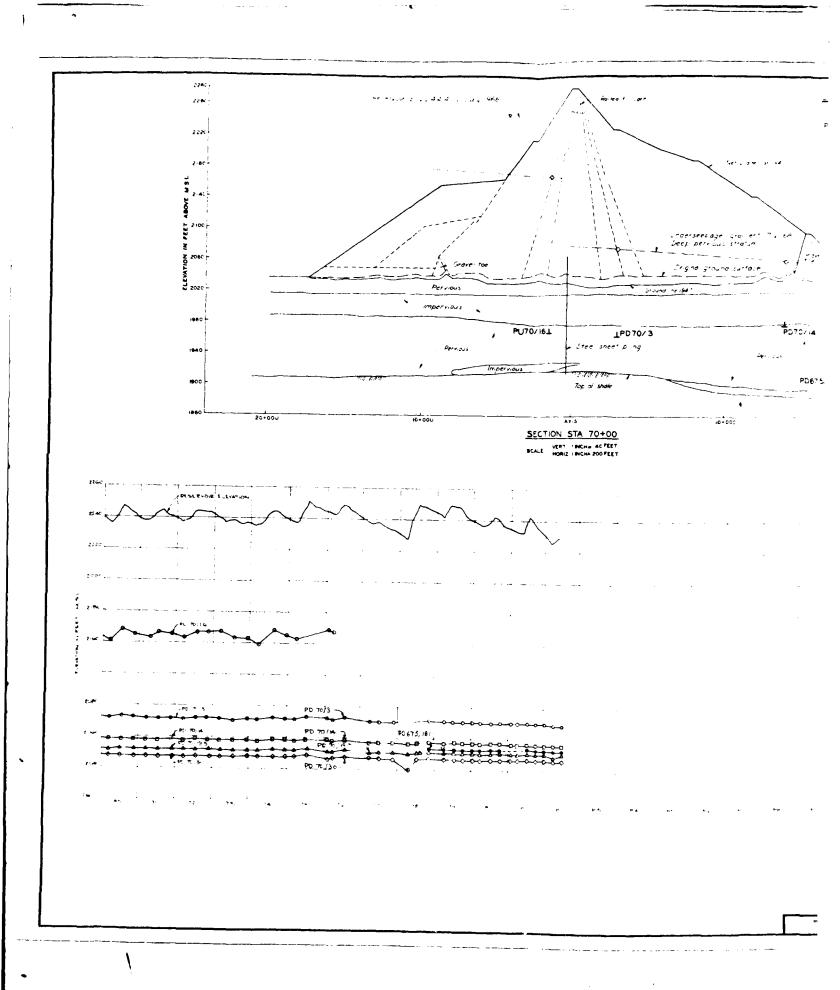


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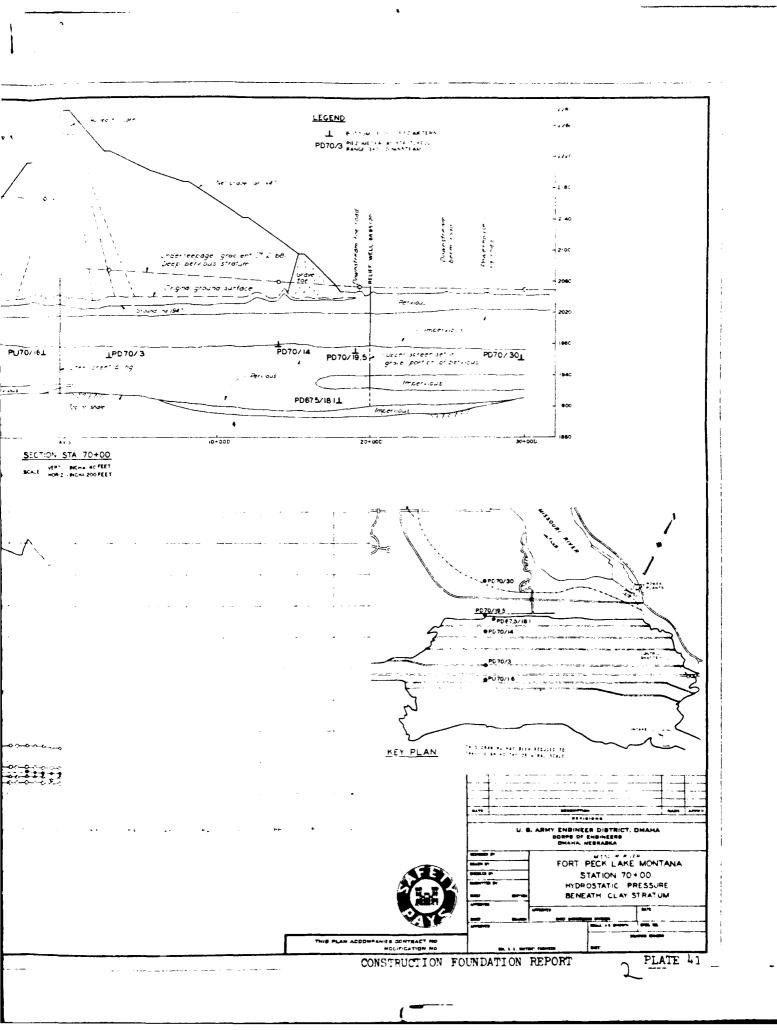


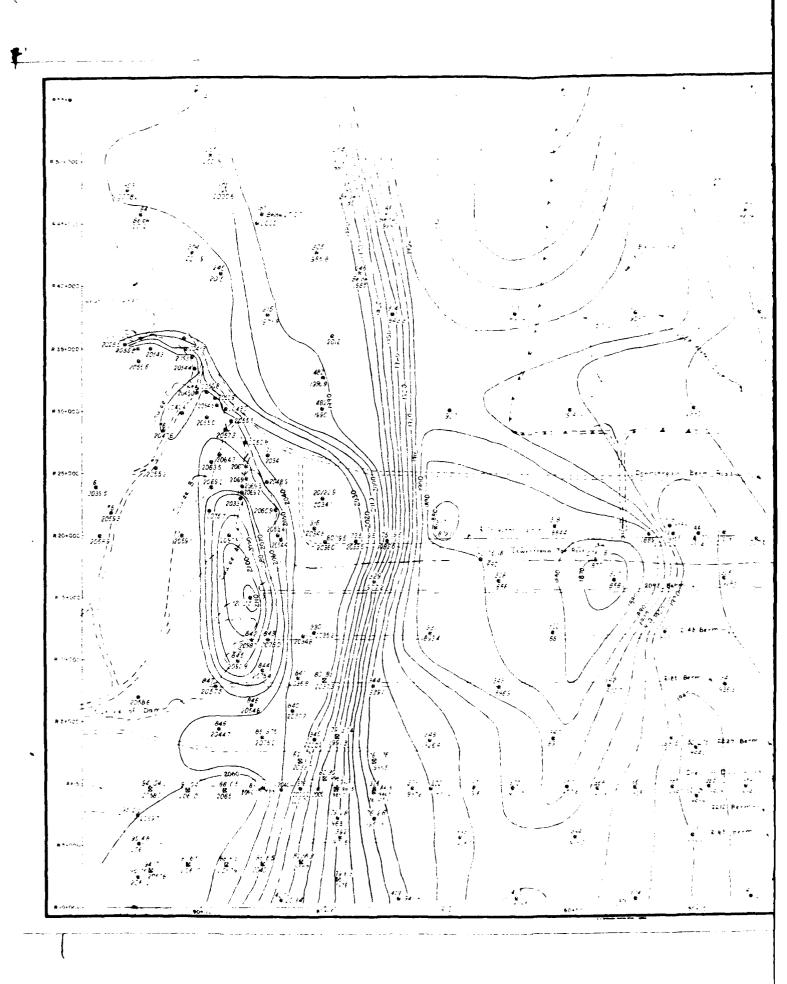






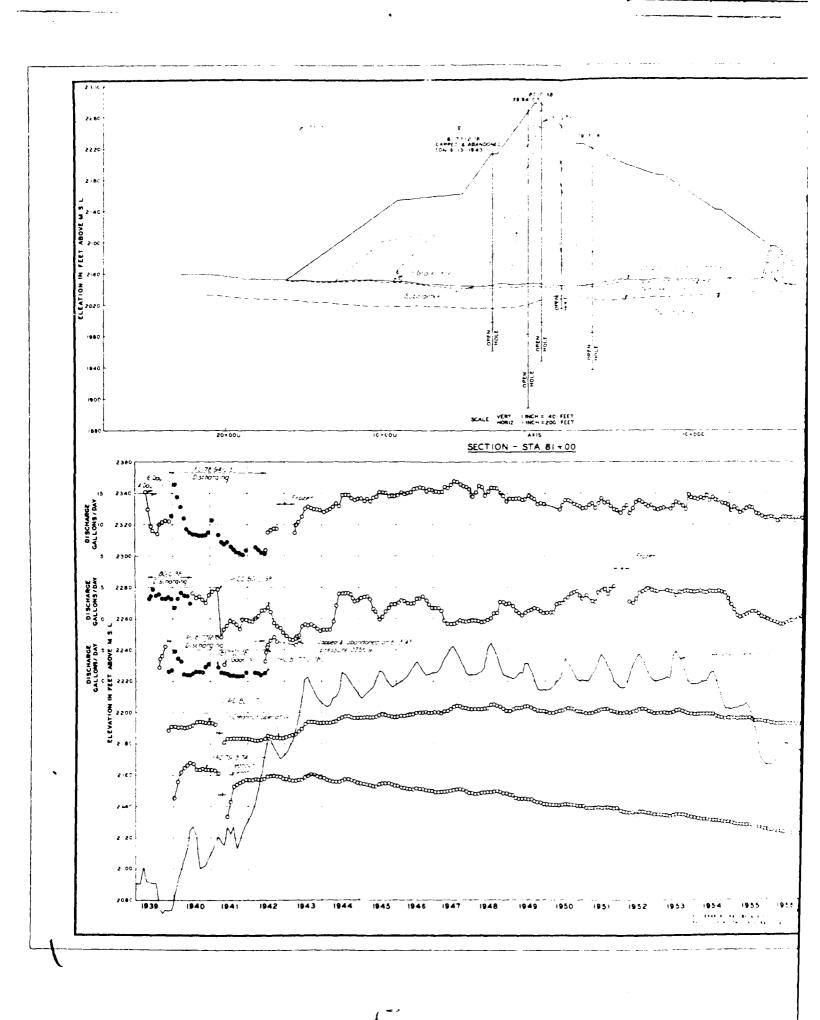
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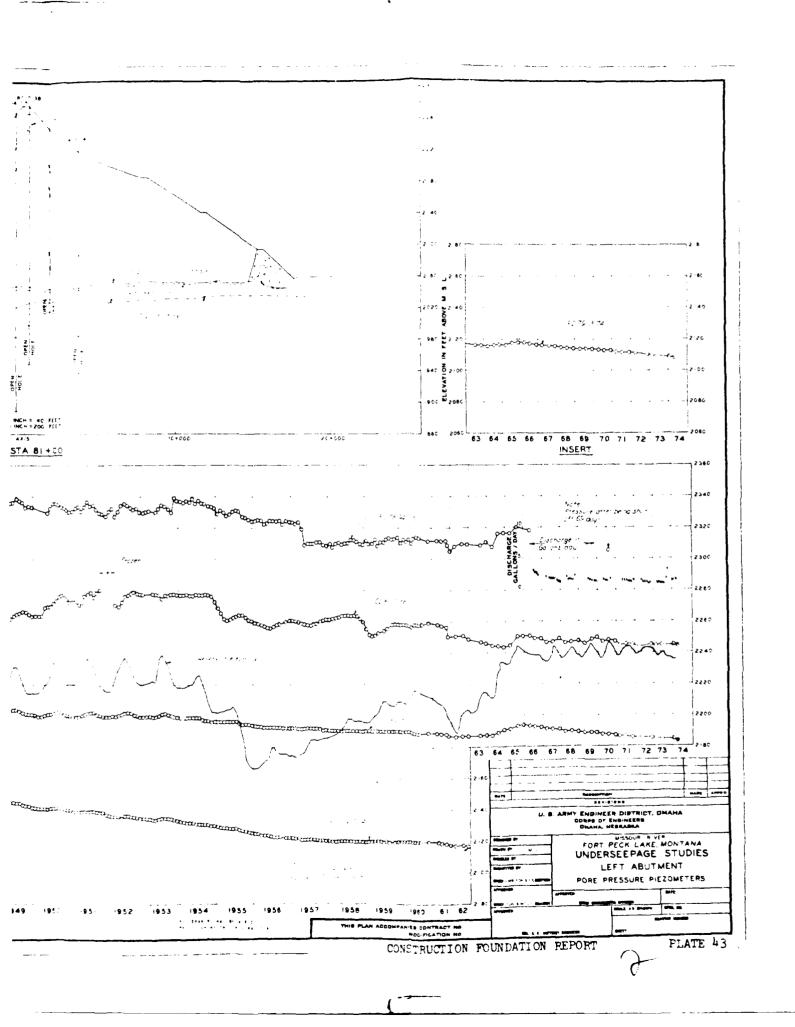


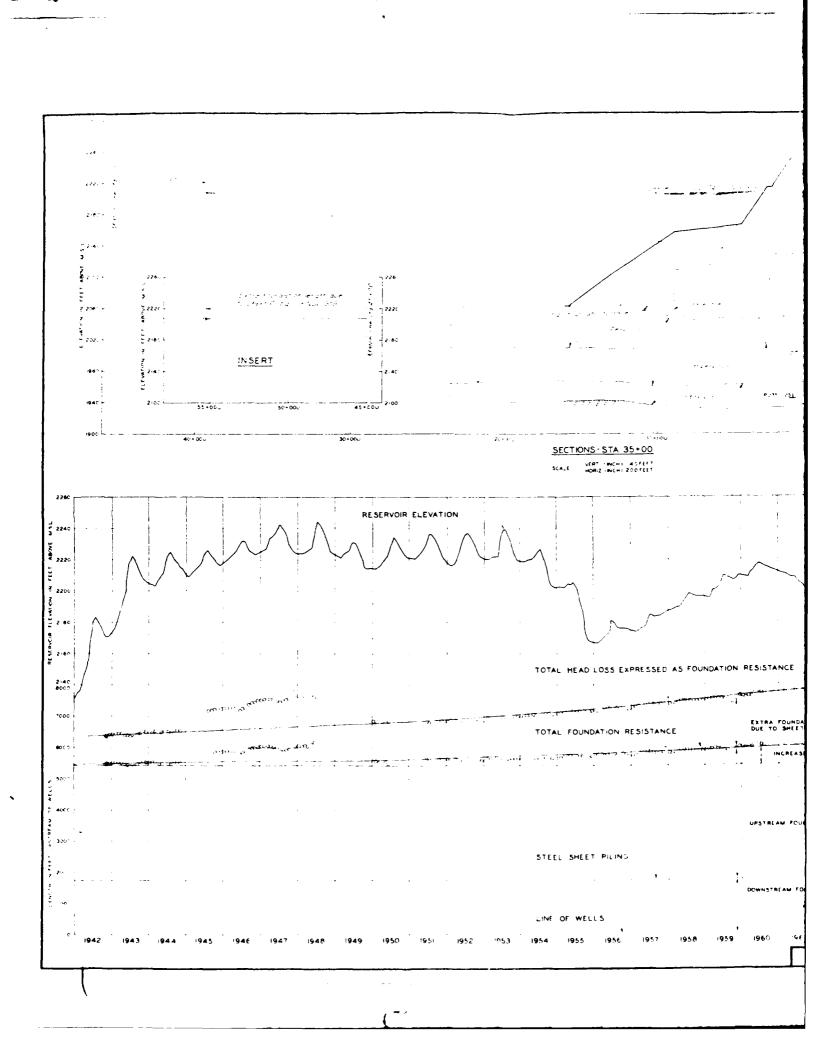


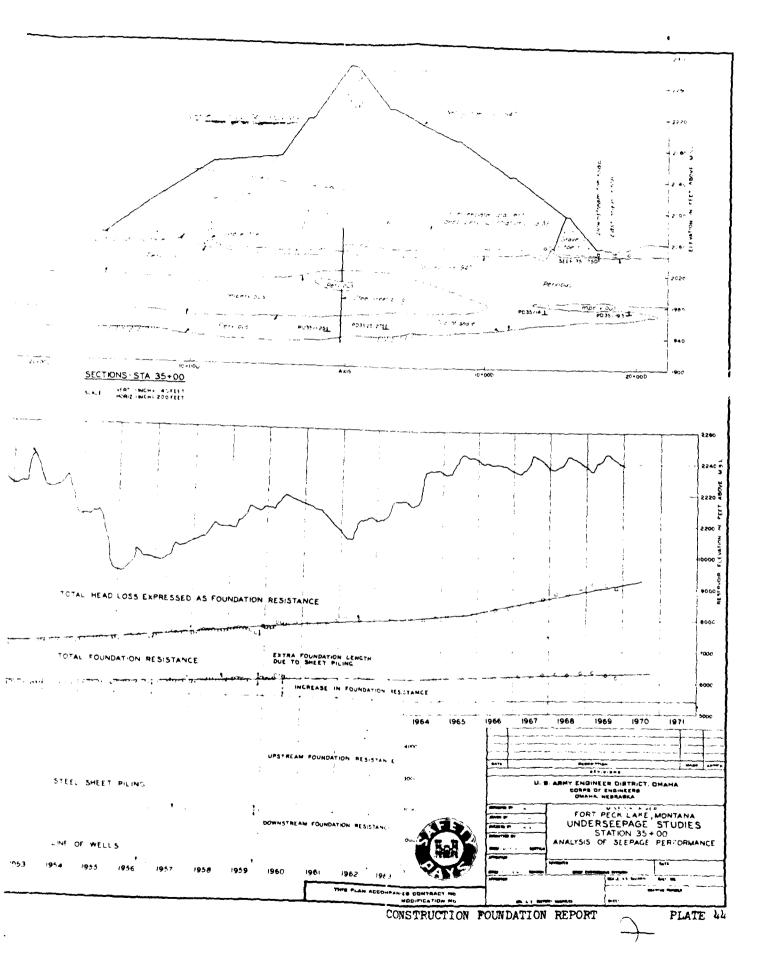
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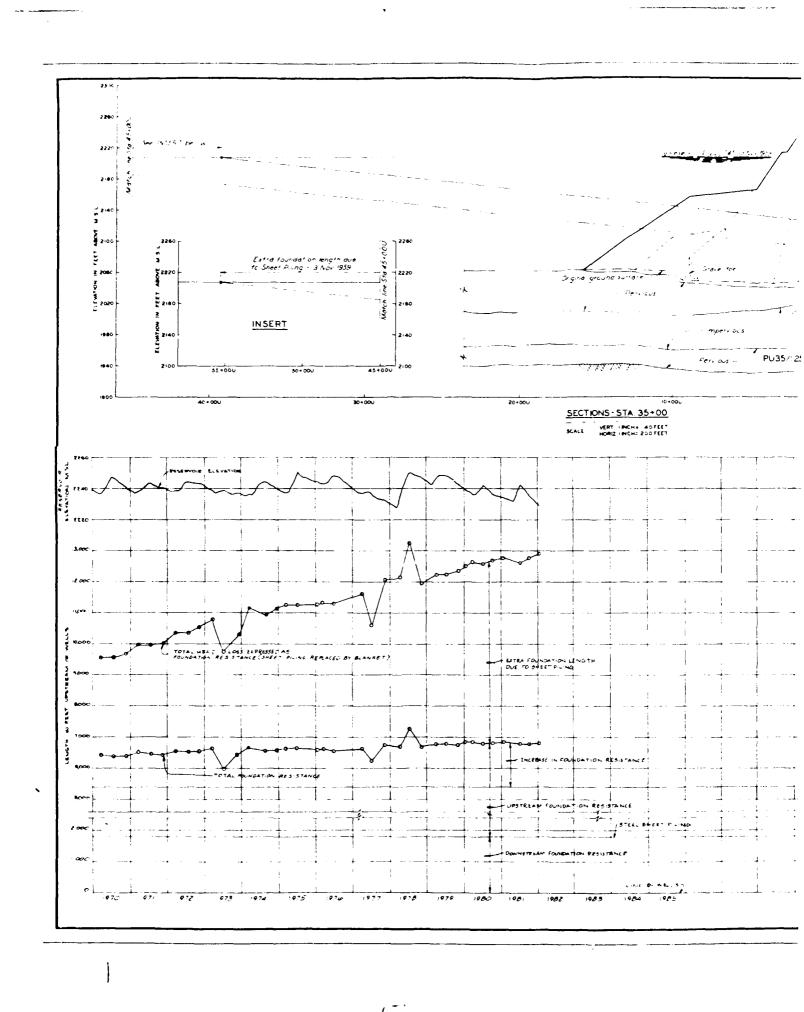


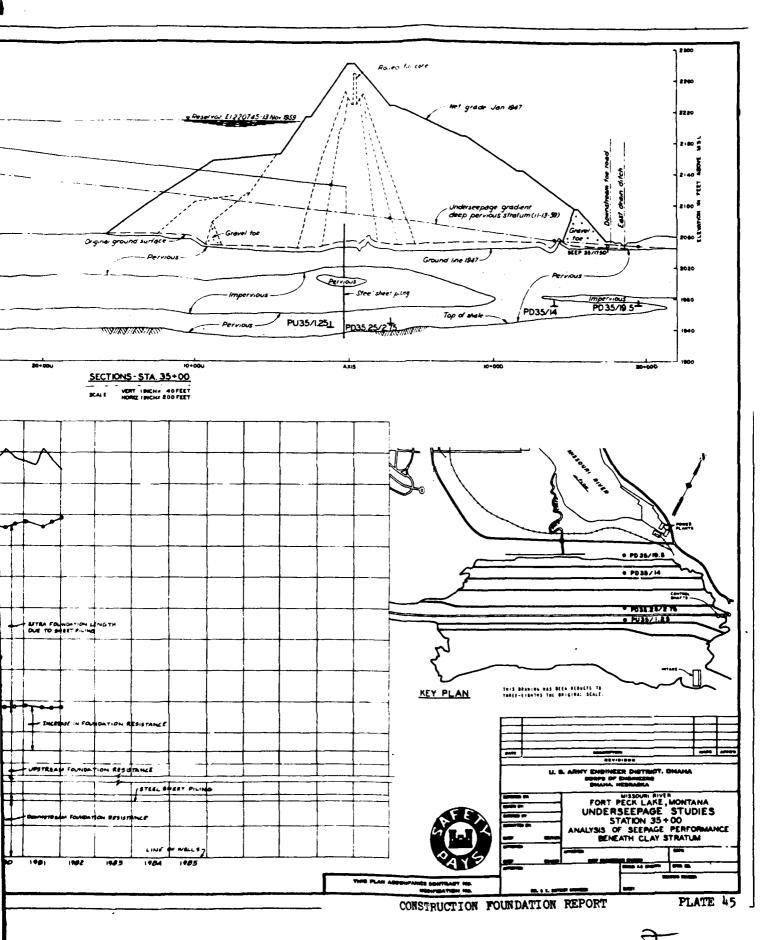


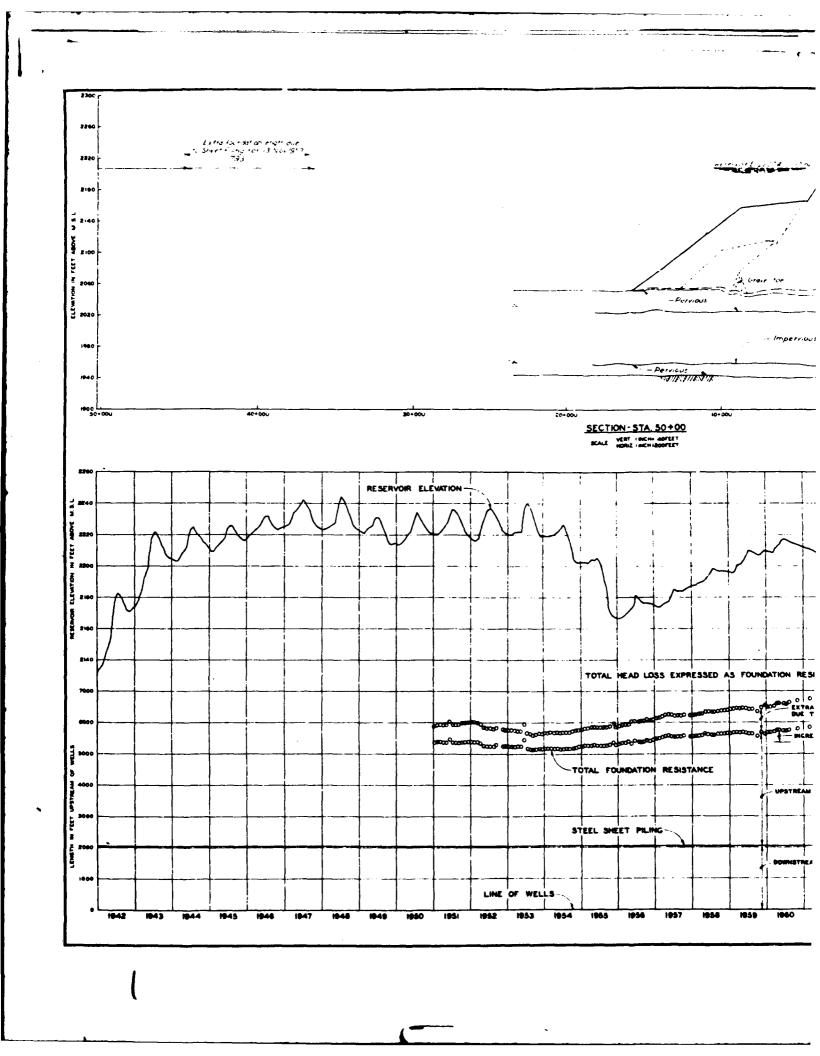


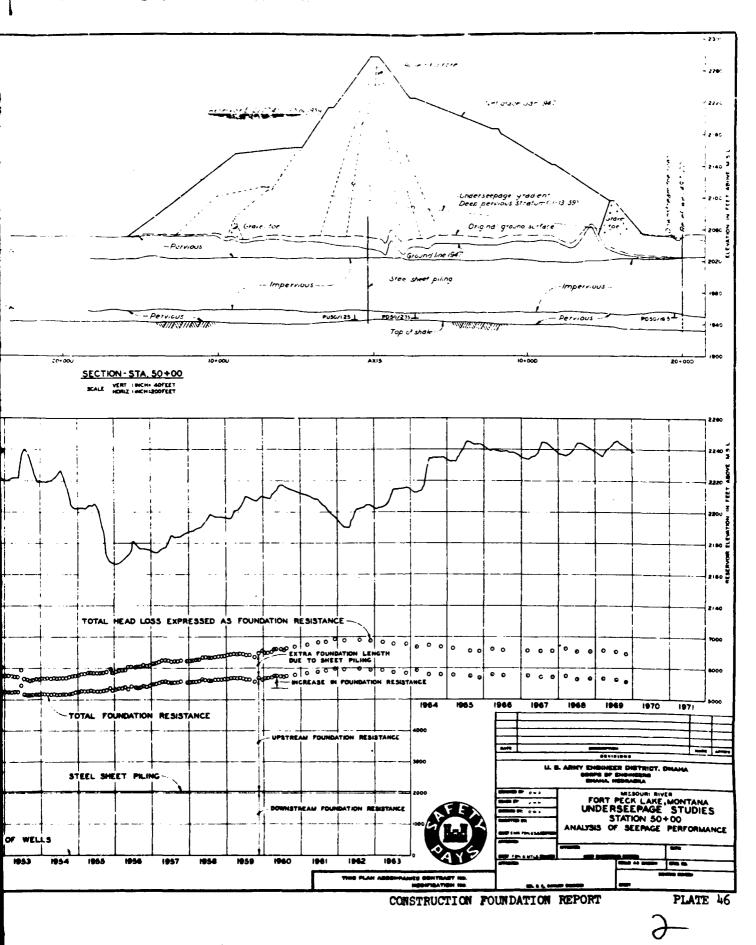


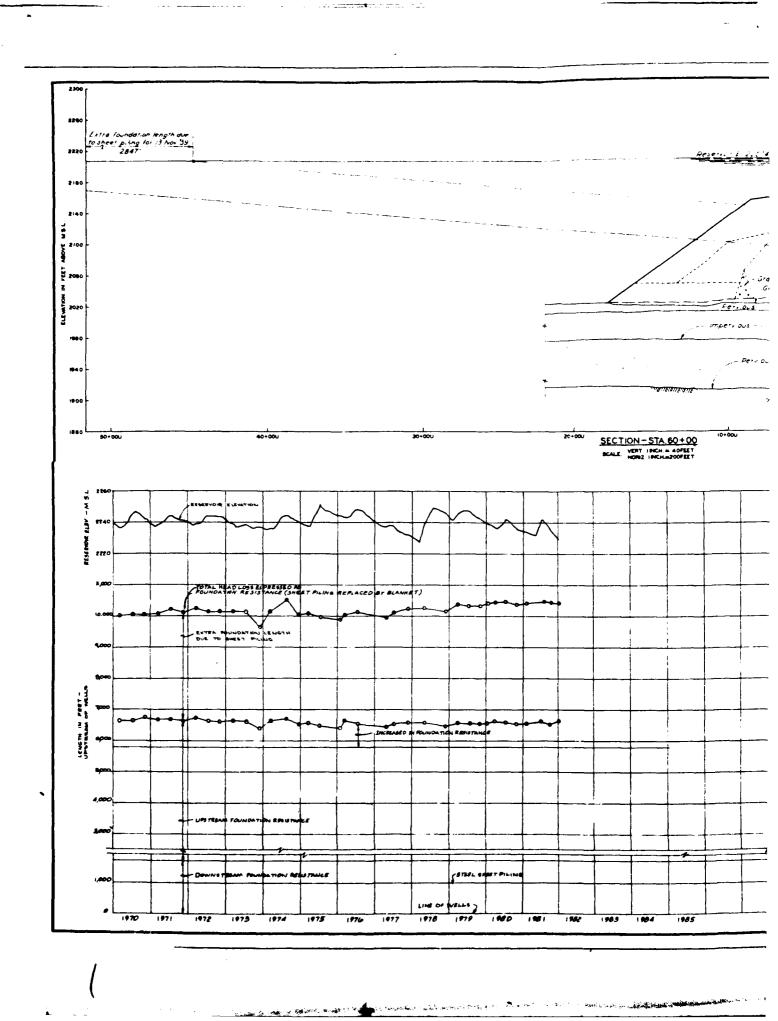
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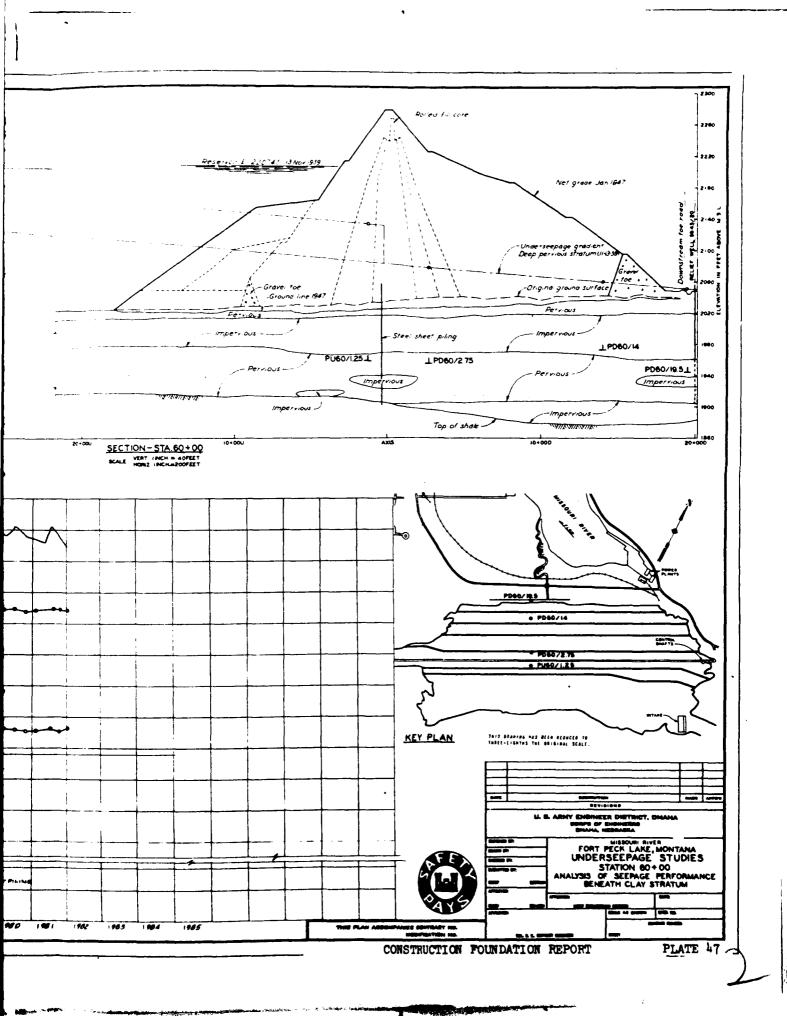




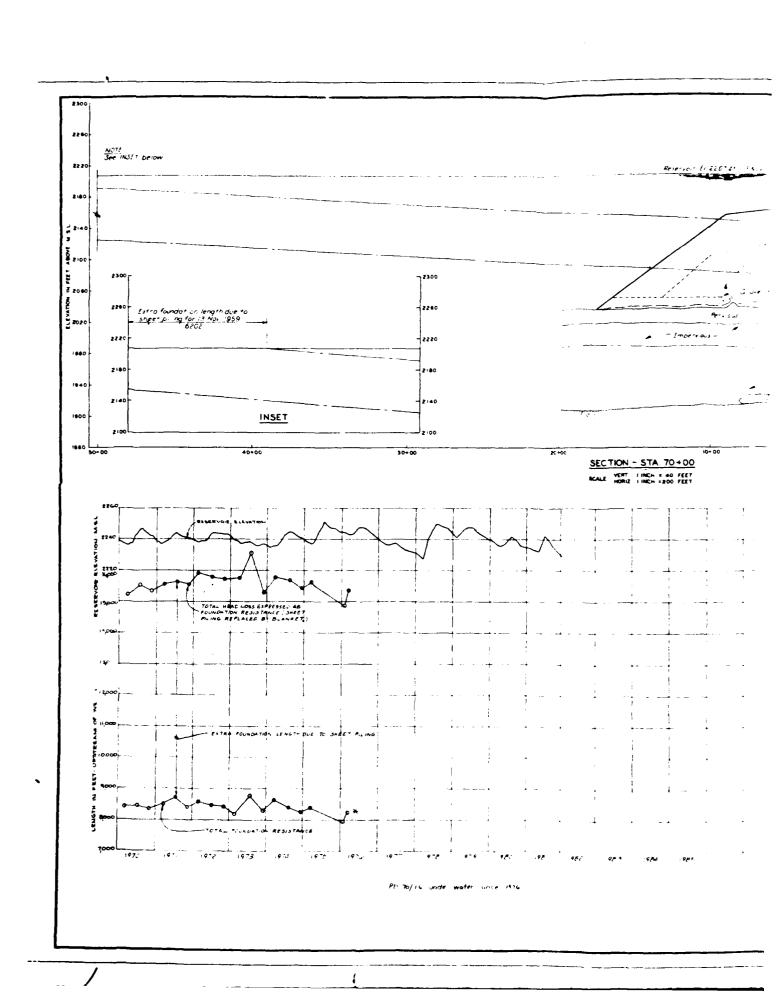


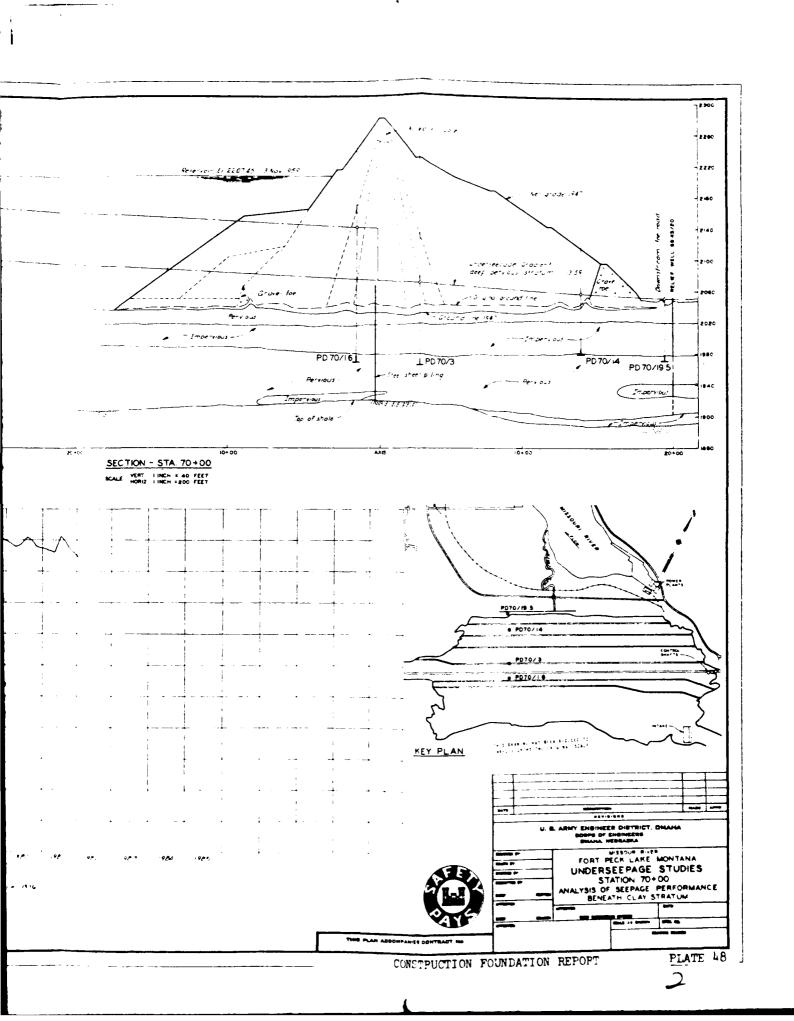


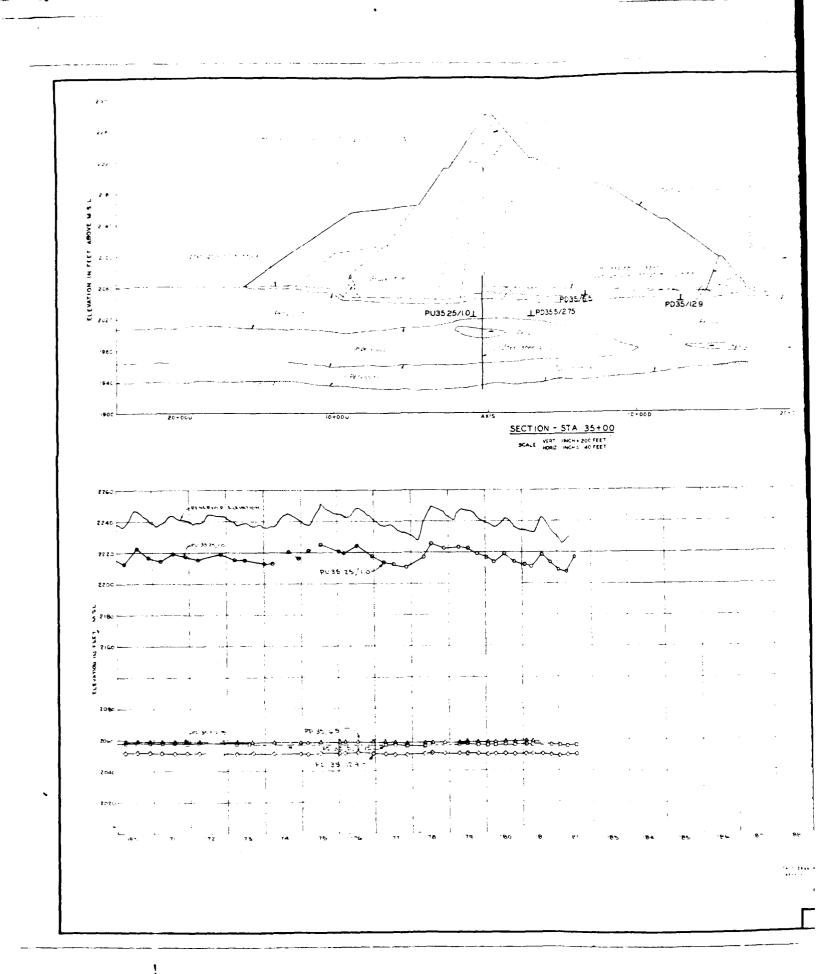


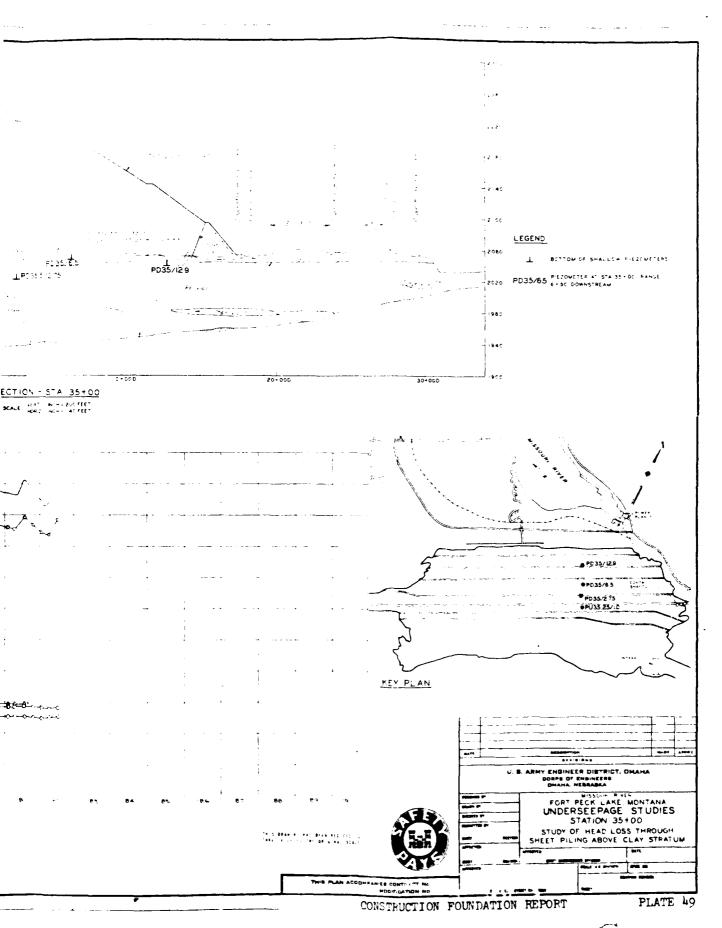


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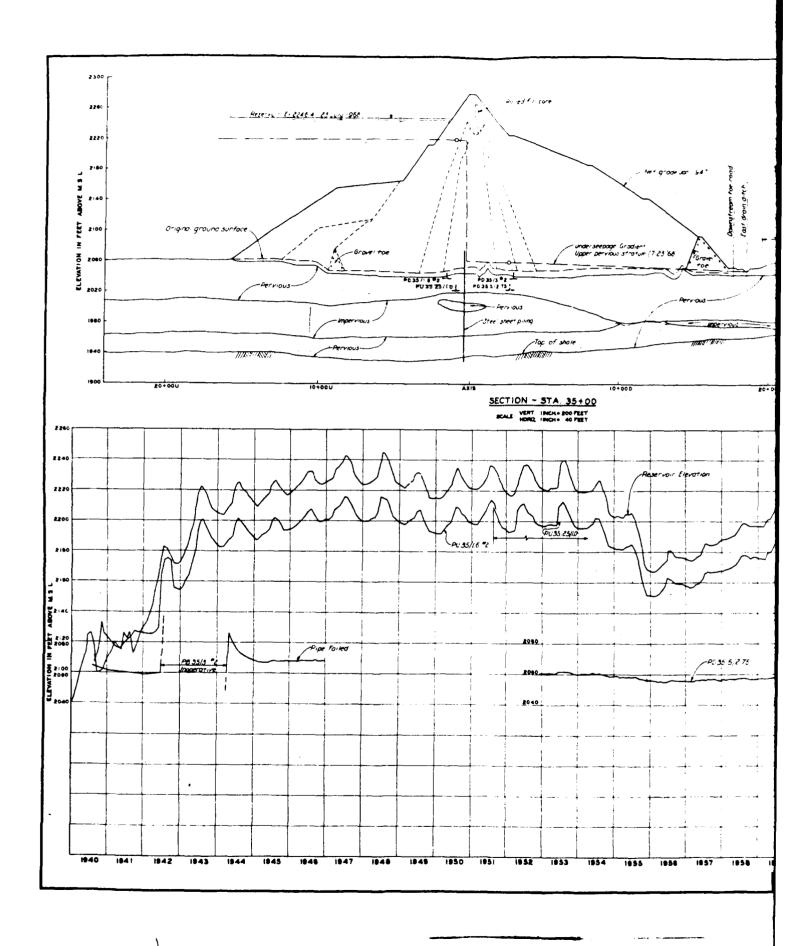


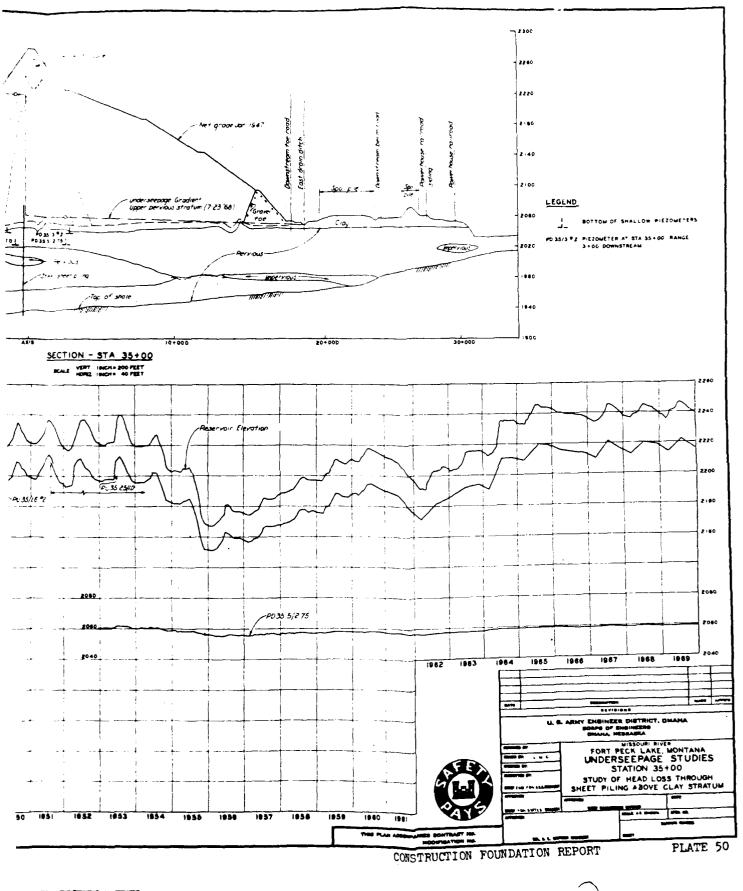


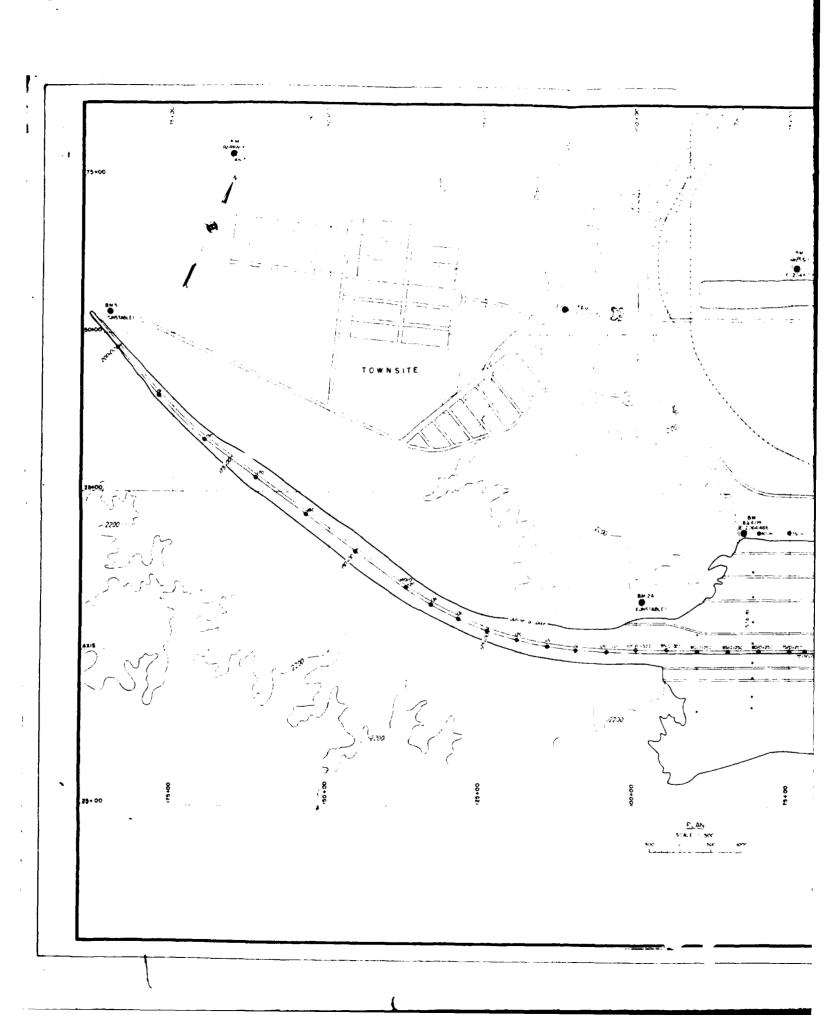


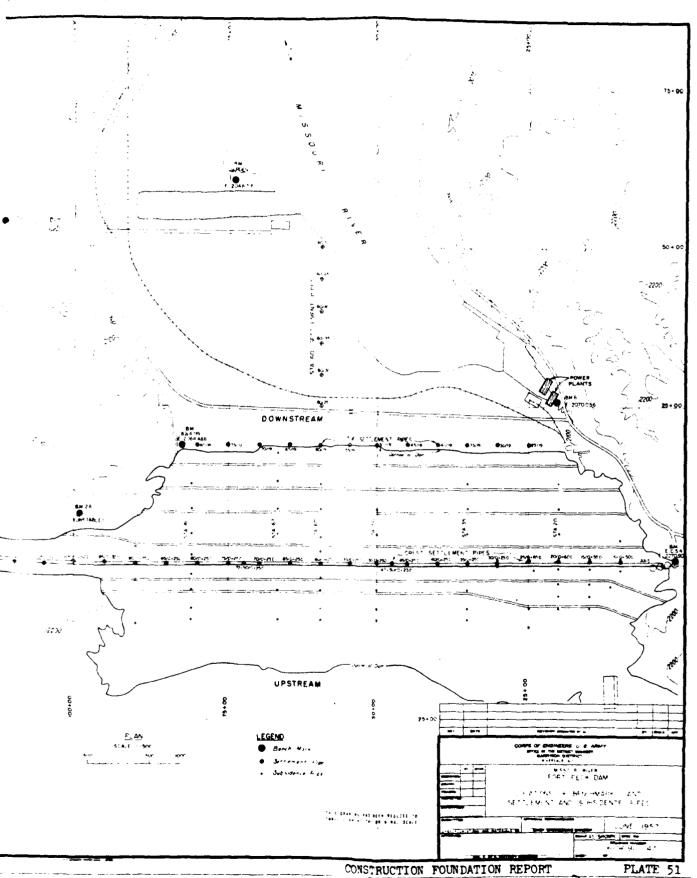


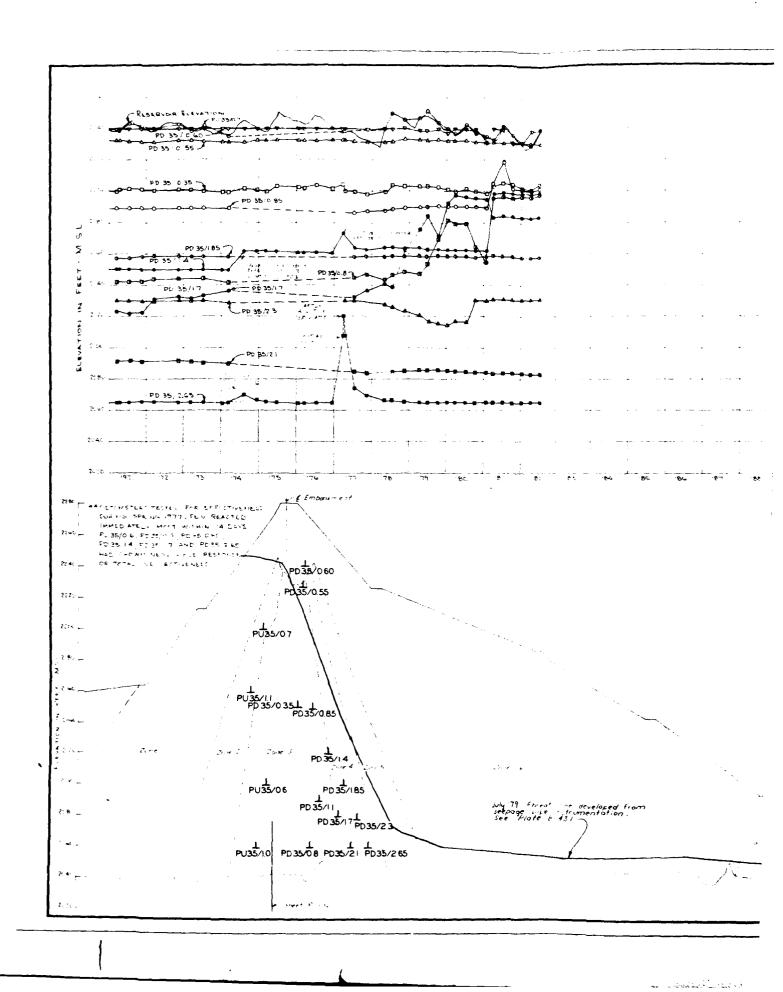
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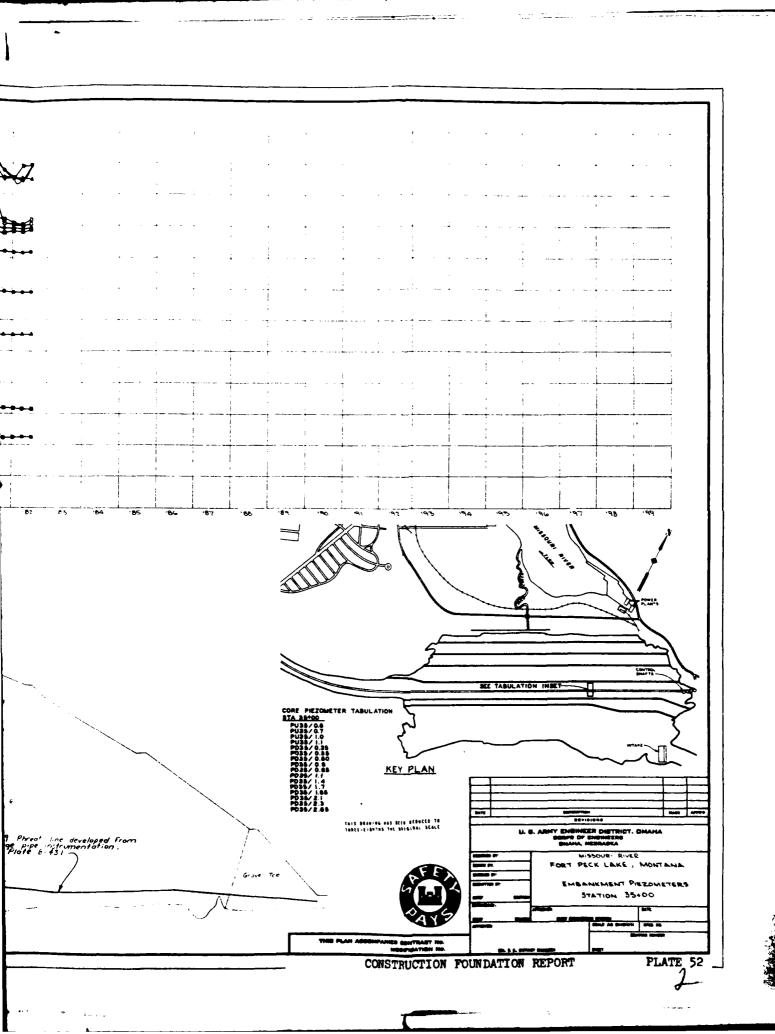


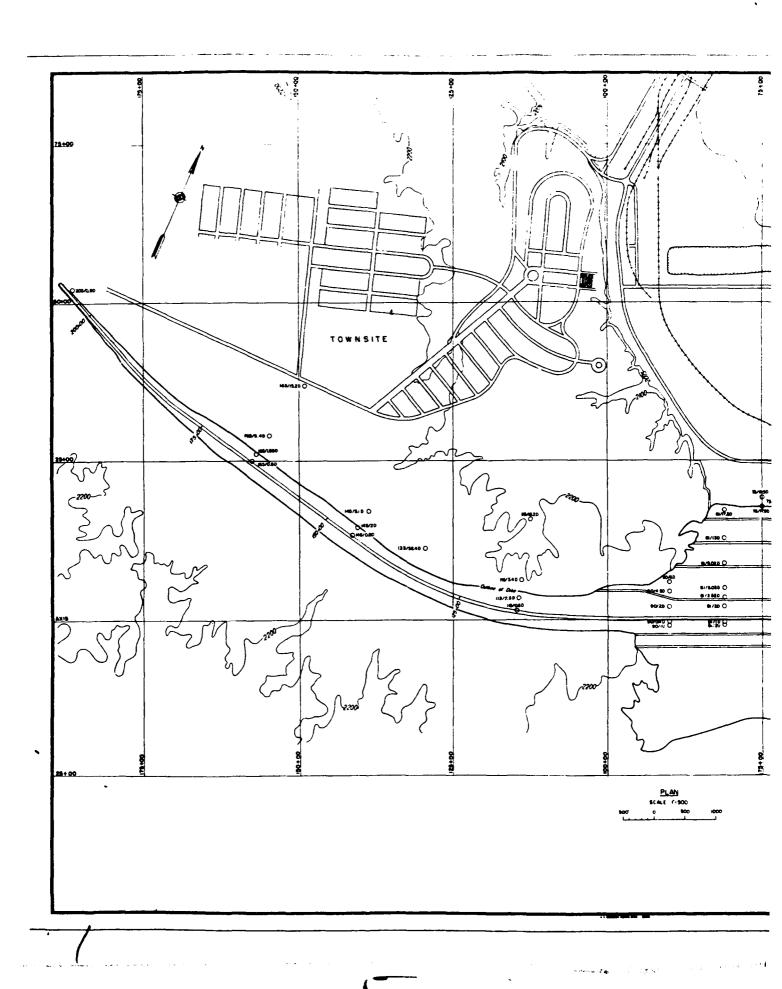


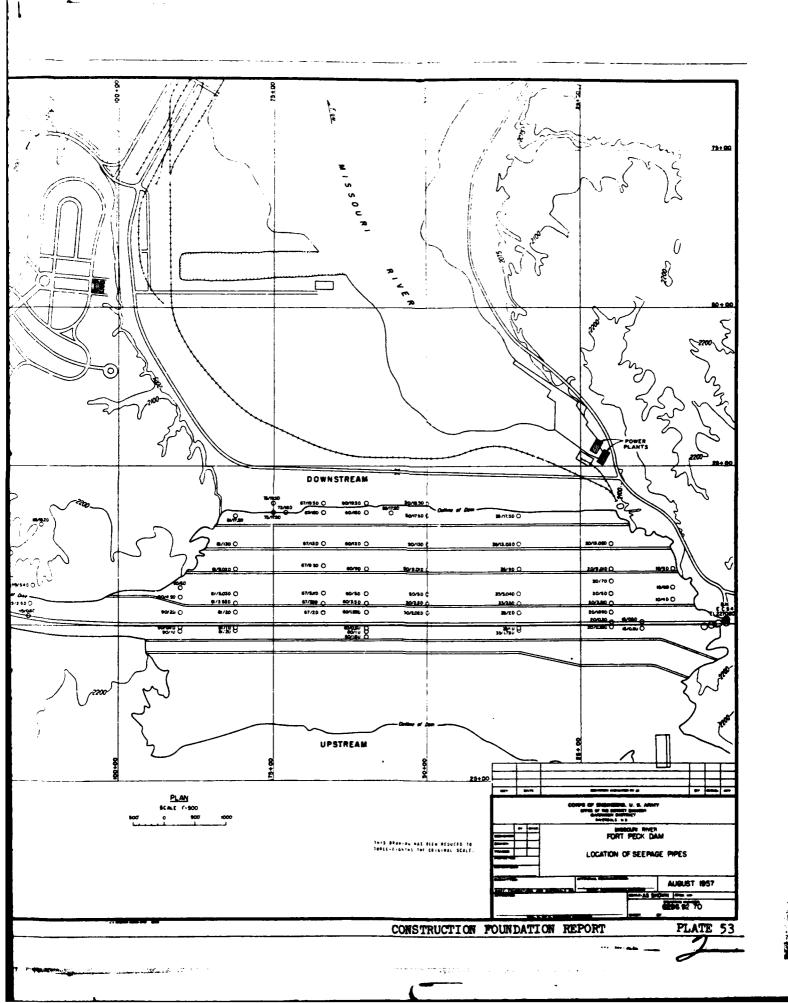


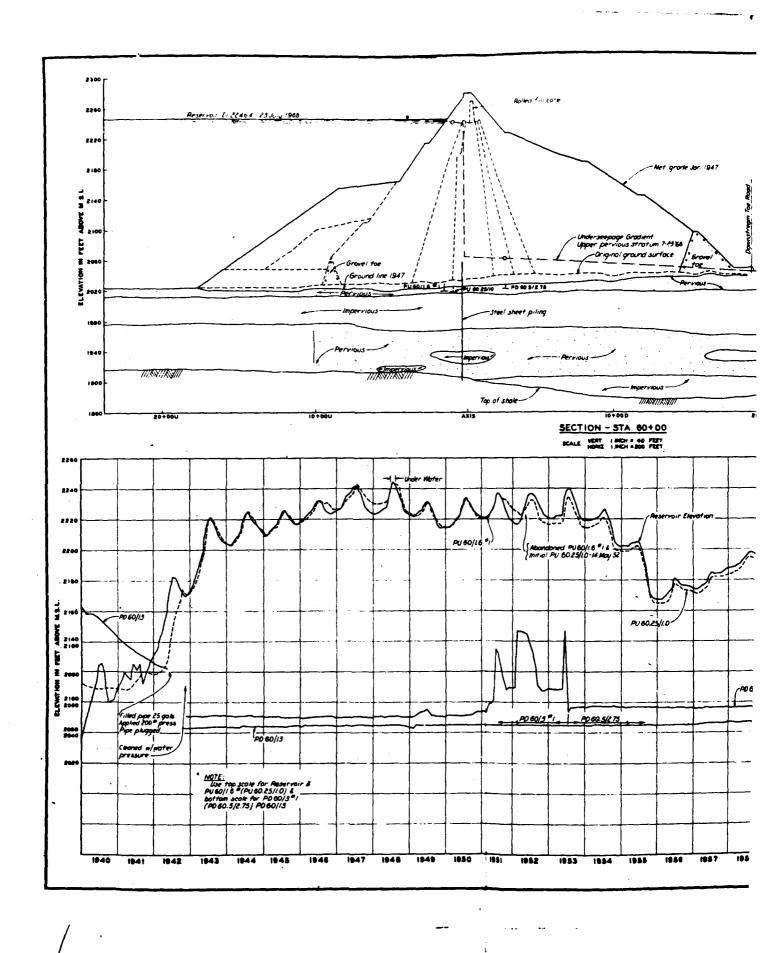


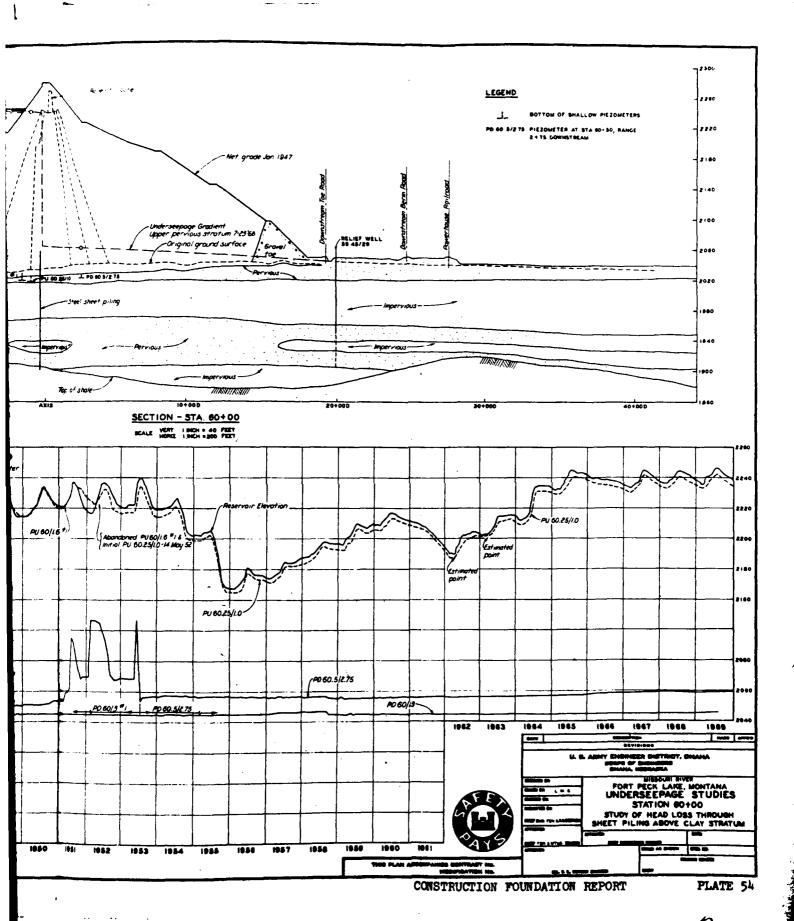




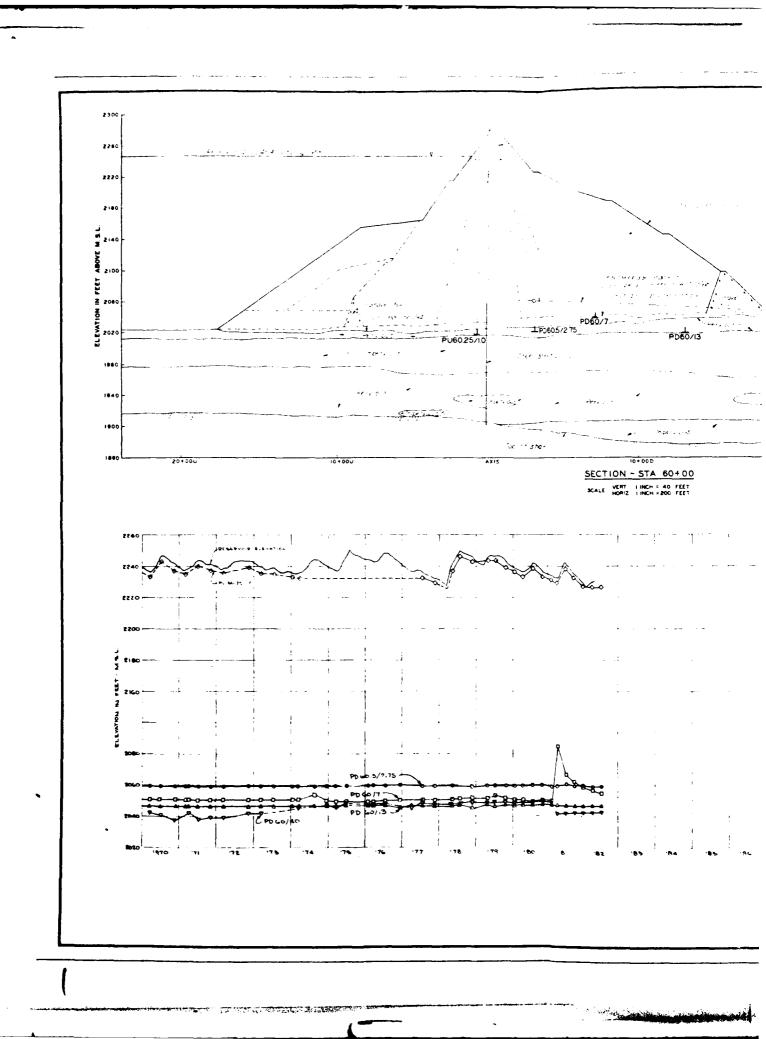


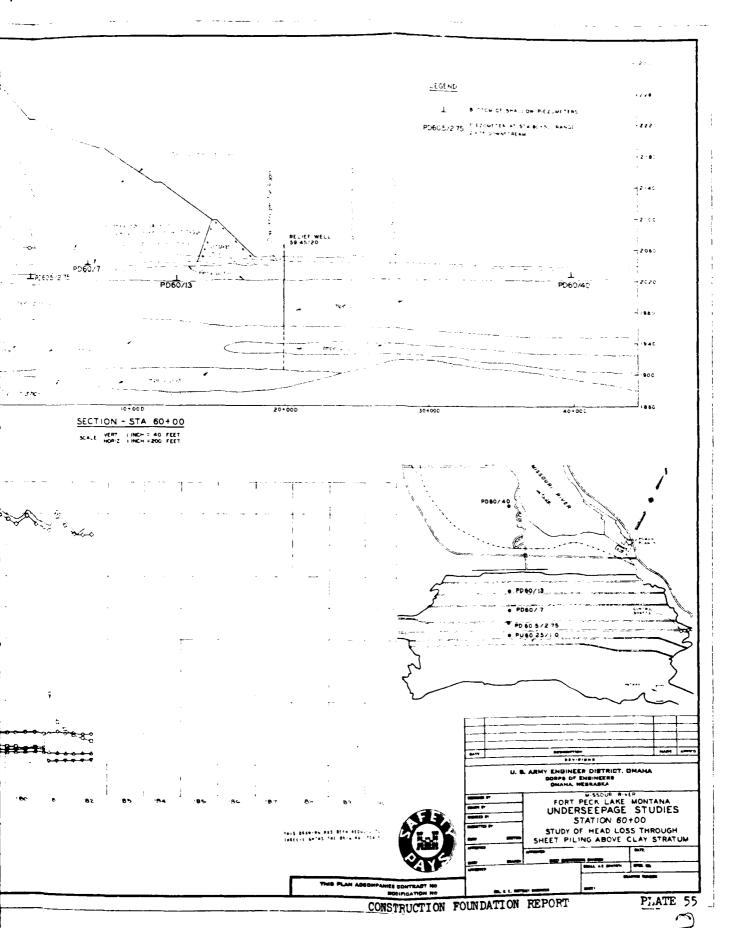


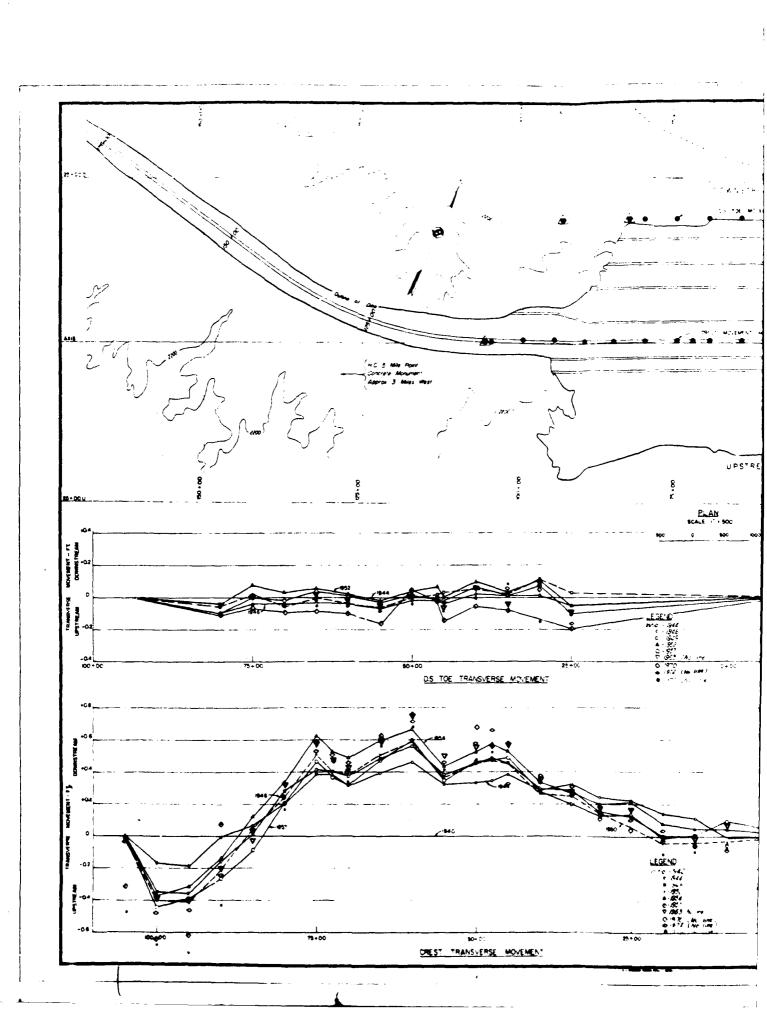


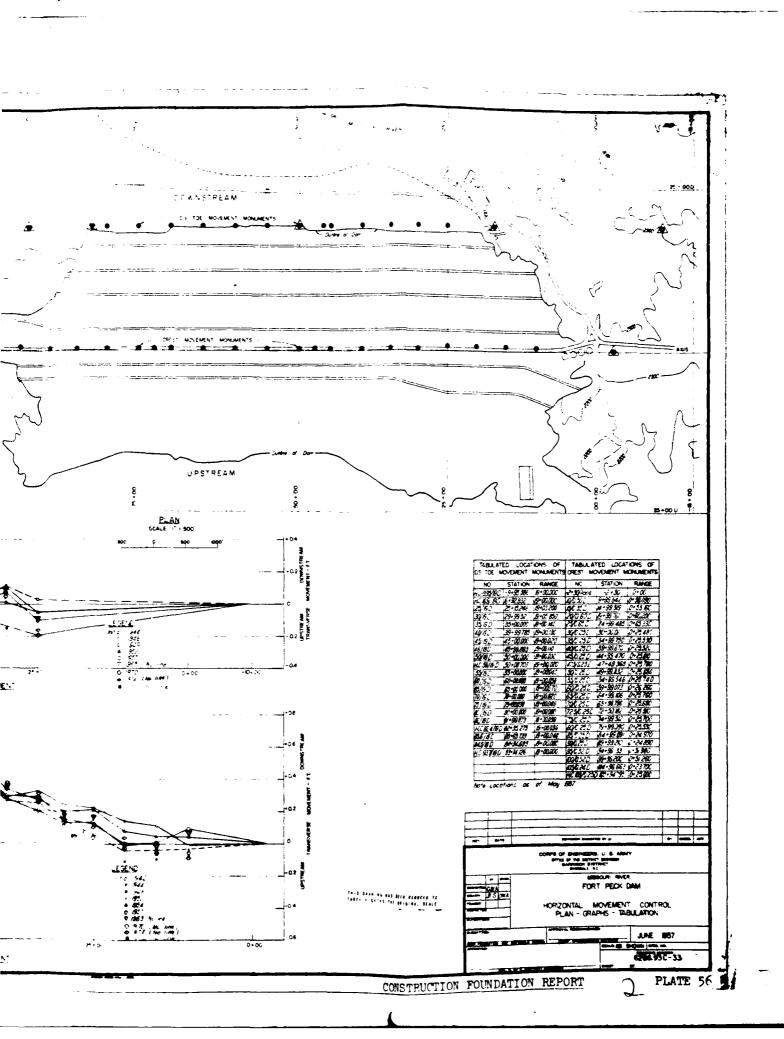


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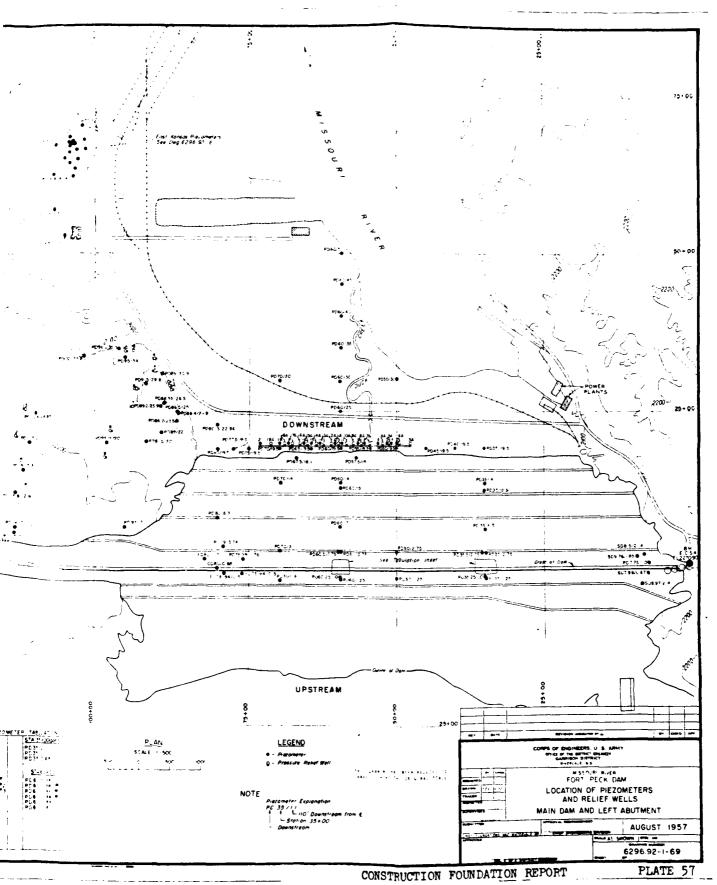




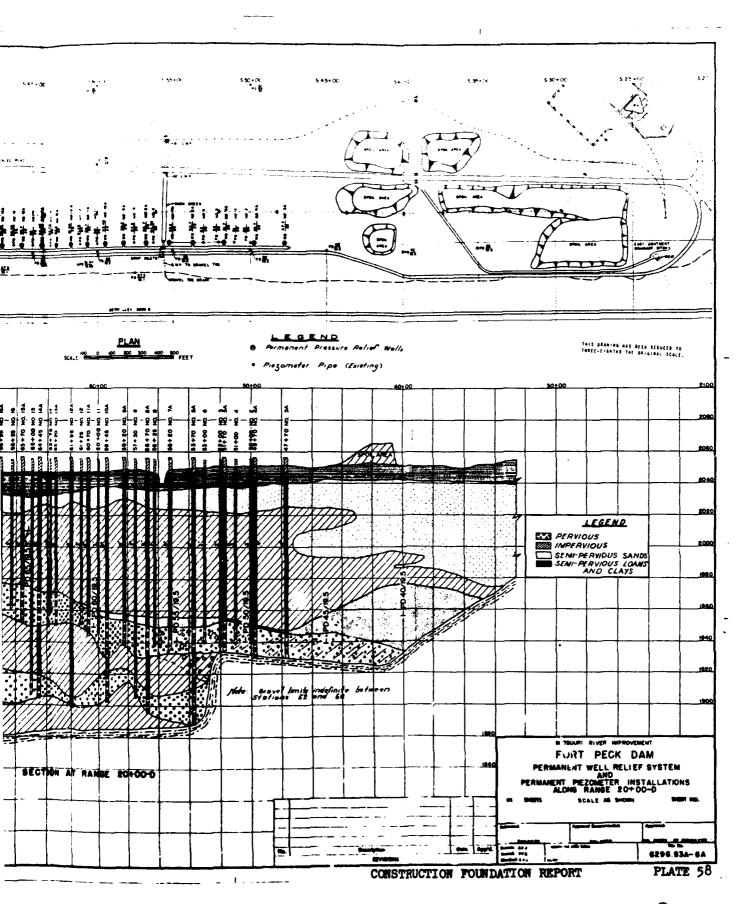


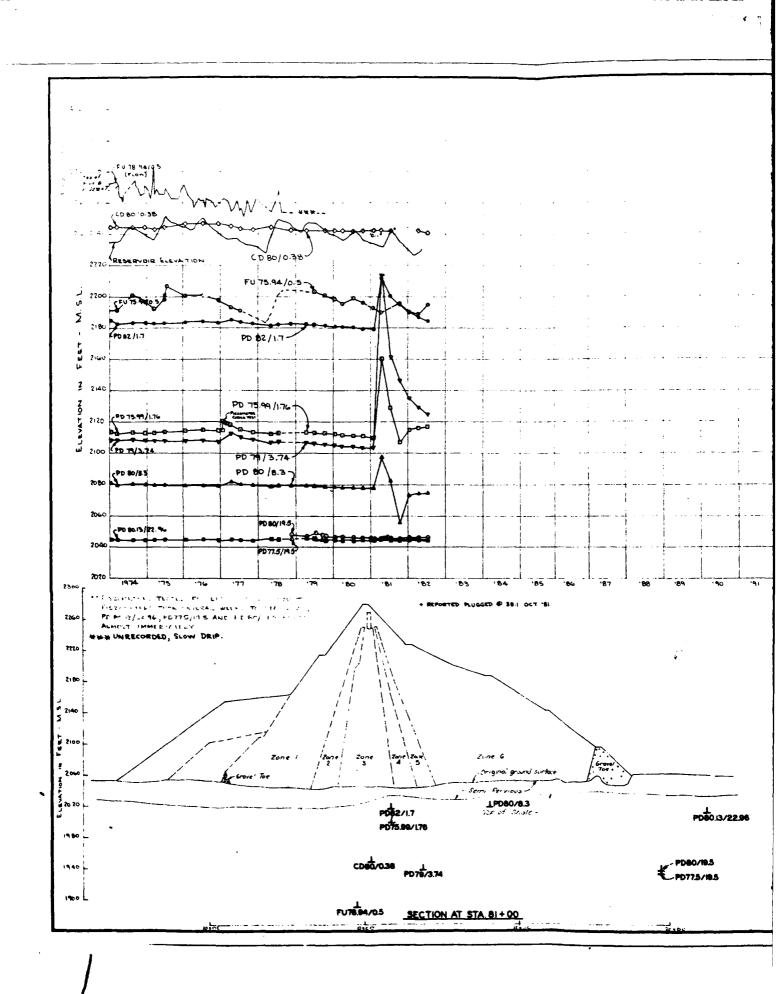


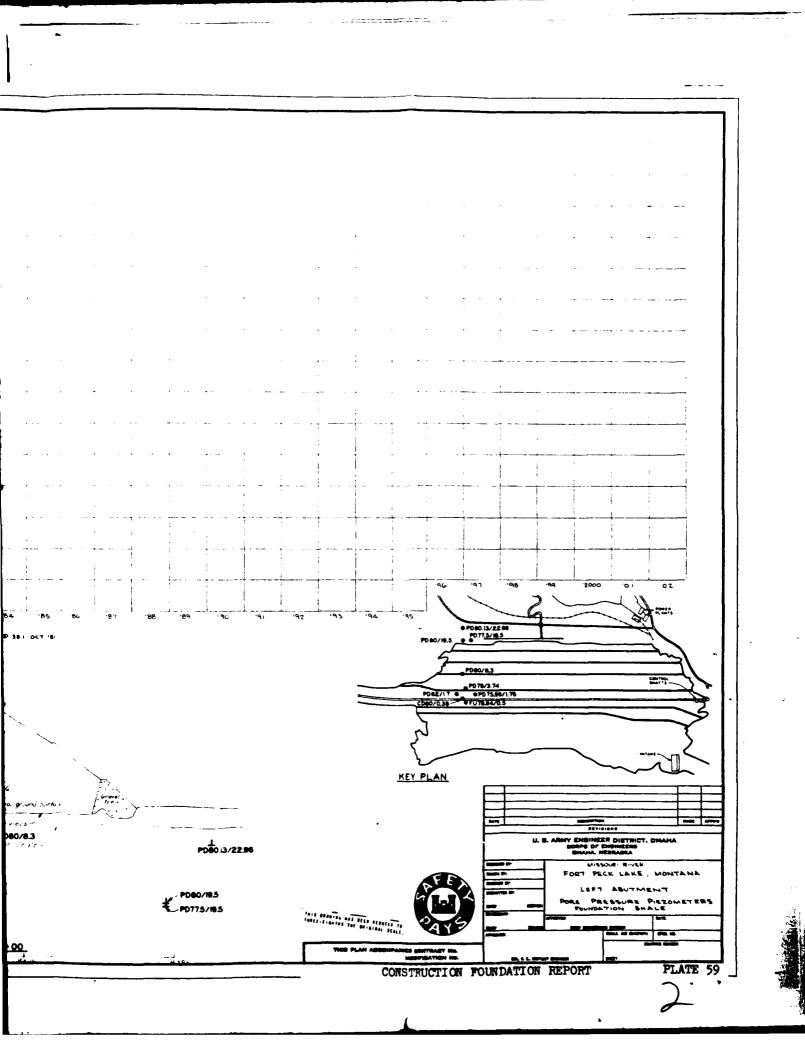
* **** y = \frac{\xi}{\xi} Einer Romeau Gerunner See Einig E296 St. -हें संदेशका 2200

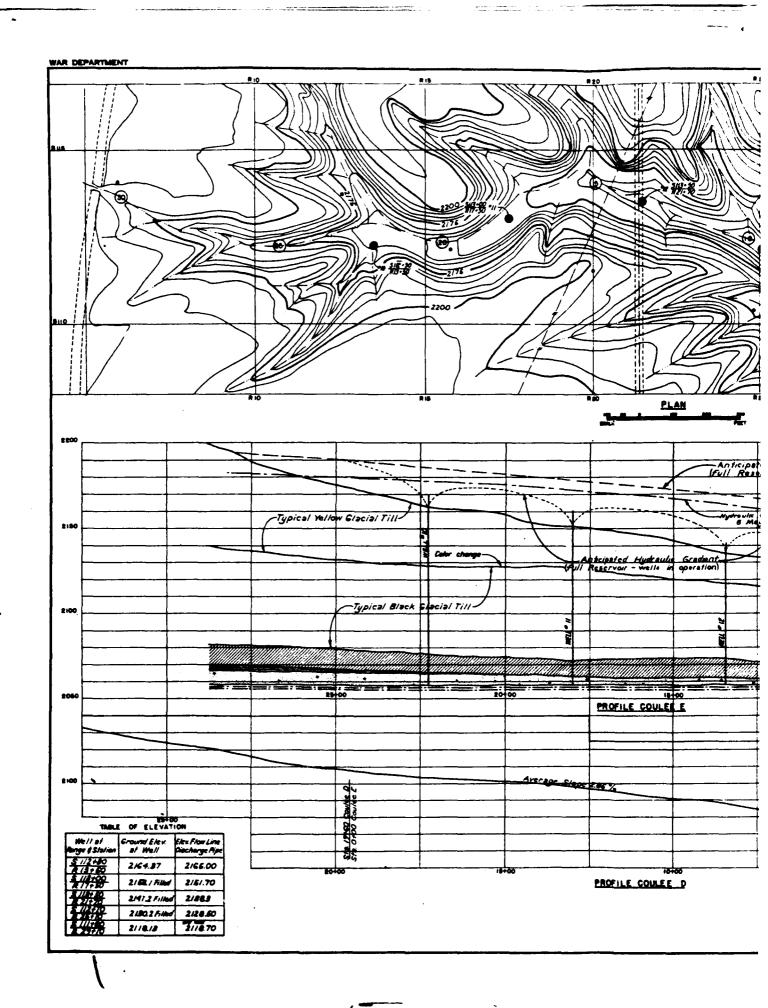


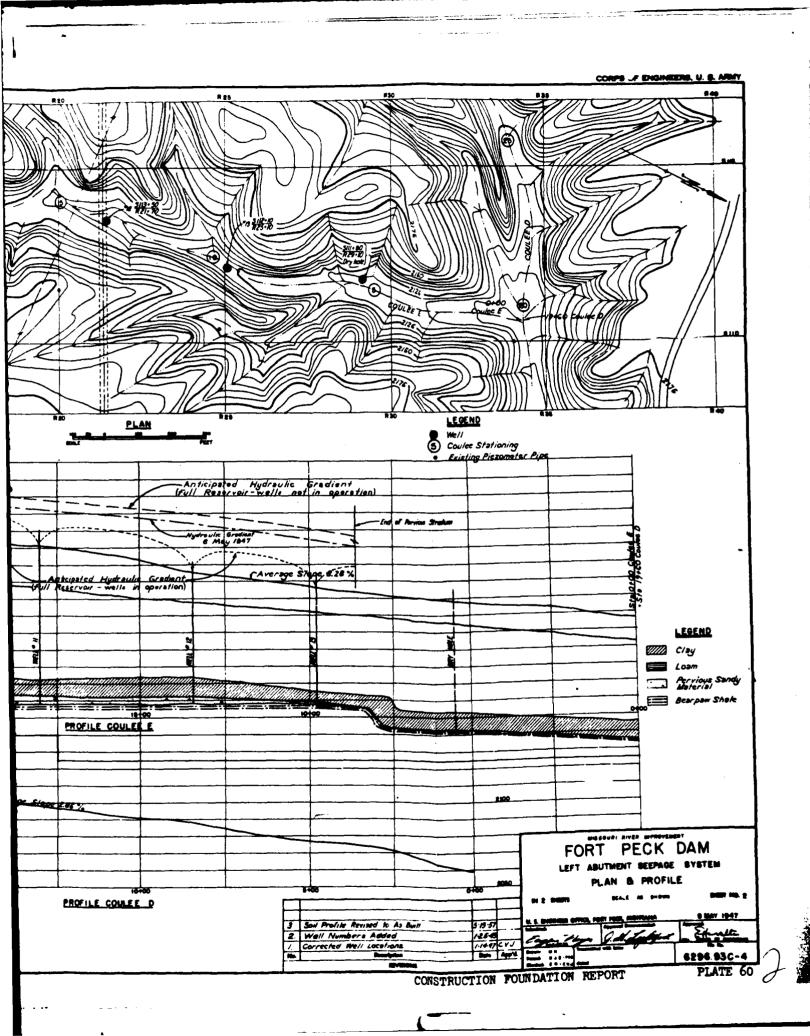
5 55+00 560 • ° ′ -- **5** 5.70+00 = 4 5 75+00 \$80+OU ٠. # 25 + 00-D #20+00-P R6+00-0 PLAN ¥. LEGEND Ground Line
Sefuration Line
Shale Line
Shale Line
Wood Pipe
Wood Pipe SECTION AT NAME 201-00-0 _1

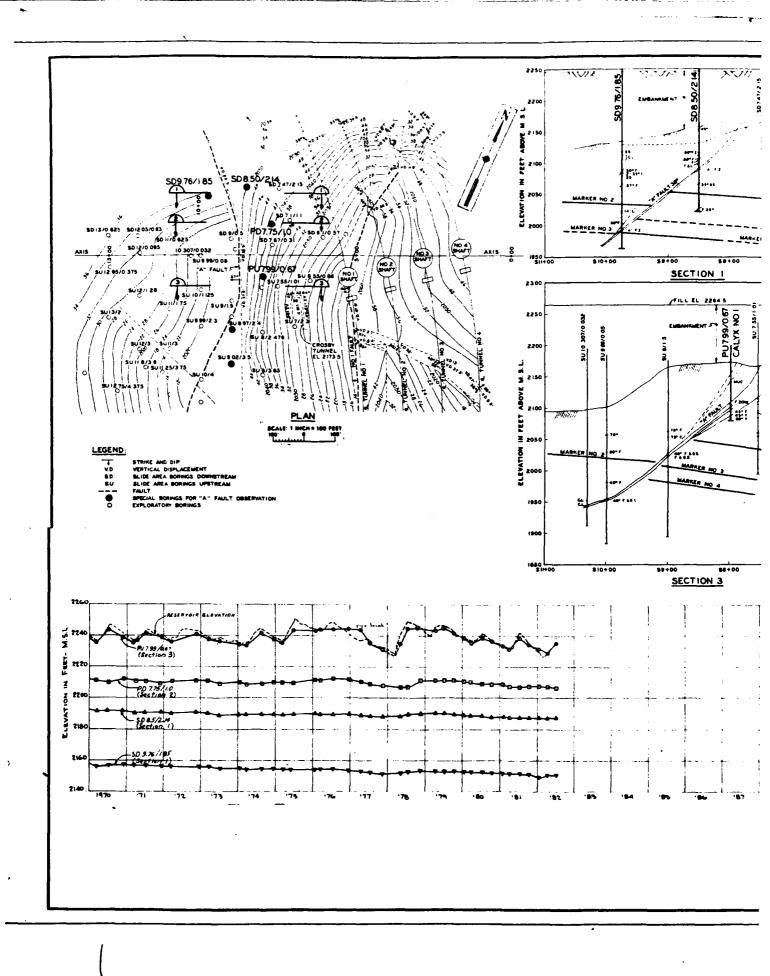


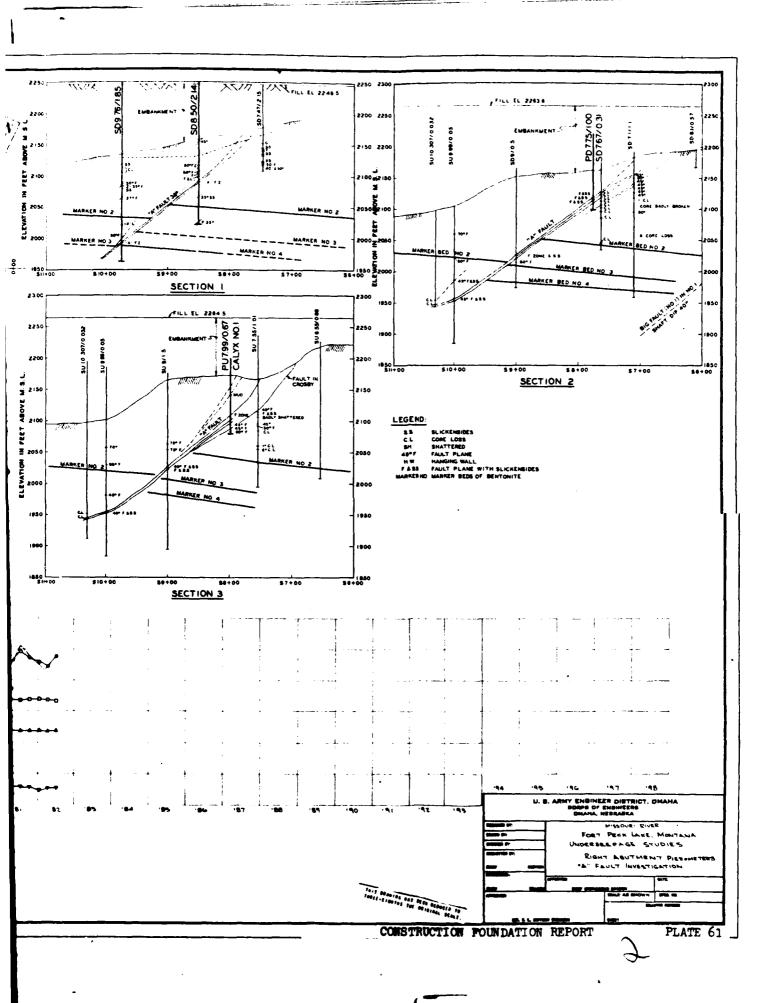








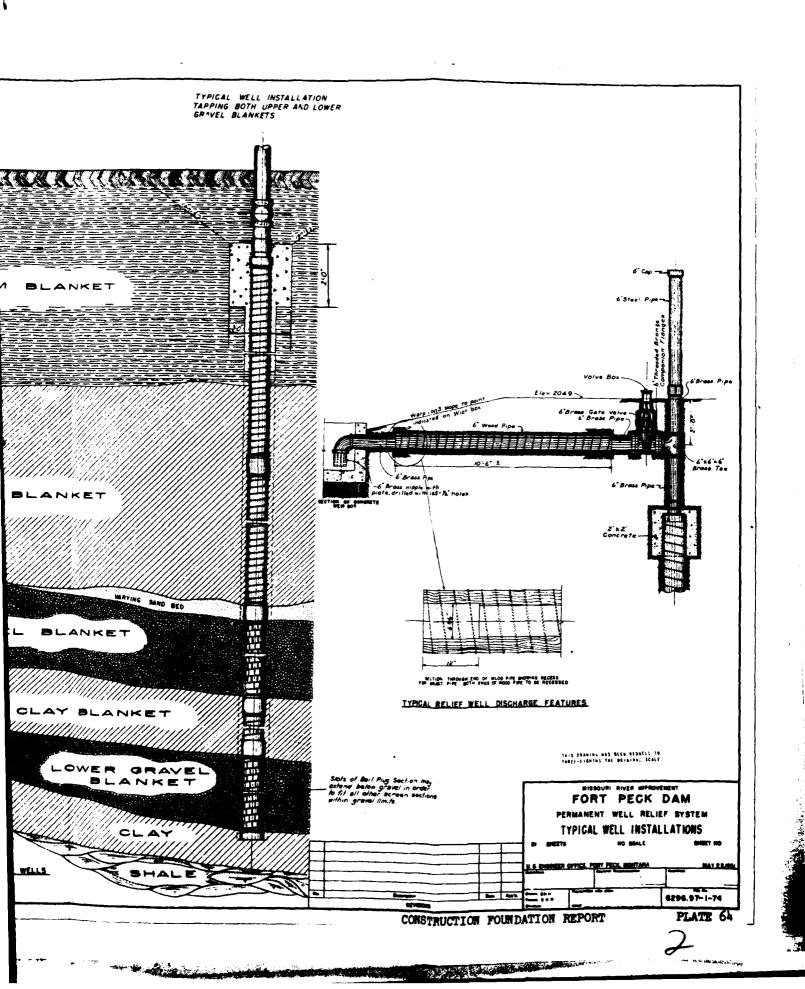


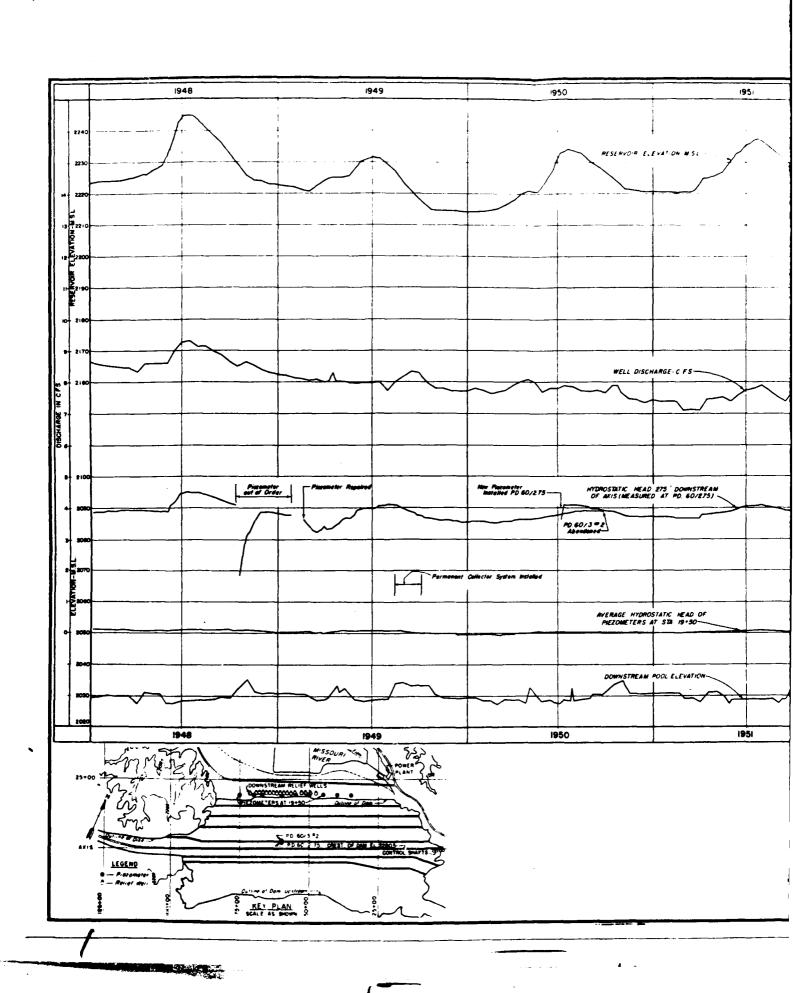


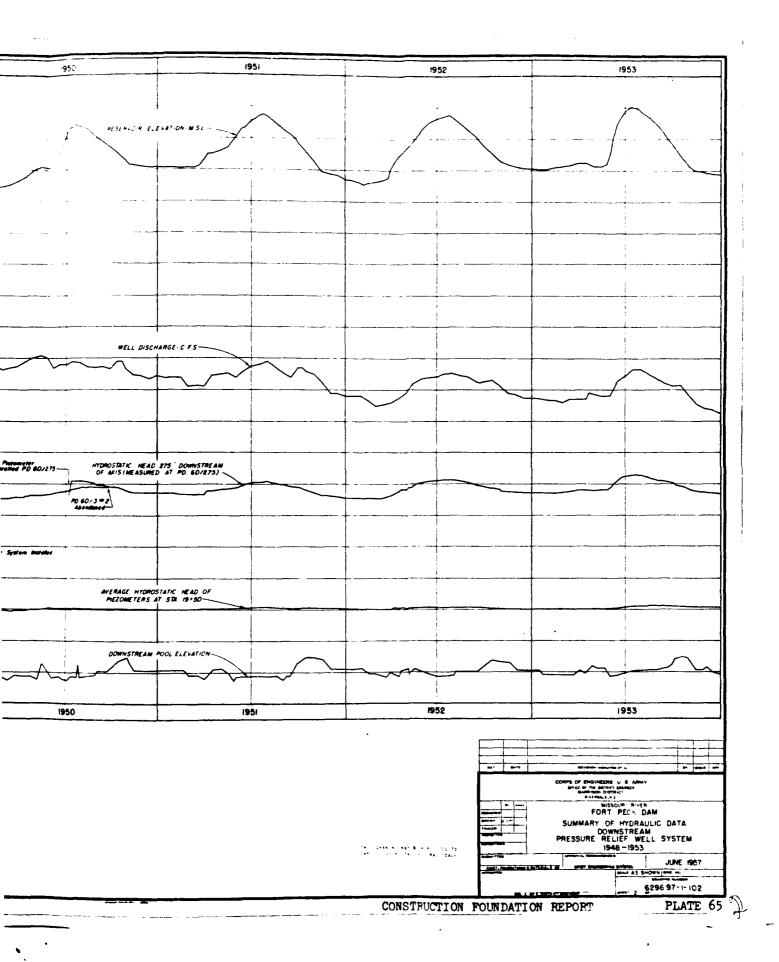
TYPICAL WELL INSTAL TAPPING BOTH UPPER I GRAVEL BLANKETS TYPICAL WELL INSTALLATION
TAPPING UPPER GRAVEL BLANKET ONLY. 6" Sleet Riser -FLOW LINE ELEV 2047 0 to edjust outlet to -Elev 20470. Concrete block a LOAM BLANKET 6" Mood Stave pipe. UPPER CLAY BLANKET Staffed wood pipe acreen to fit grave layer. VARYING SAND BED LOWER GRAVEL BLANKET CLAY TYPICAL ELEVATION OF PERMANENT RELIEF WELLS

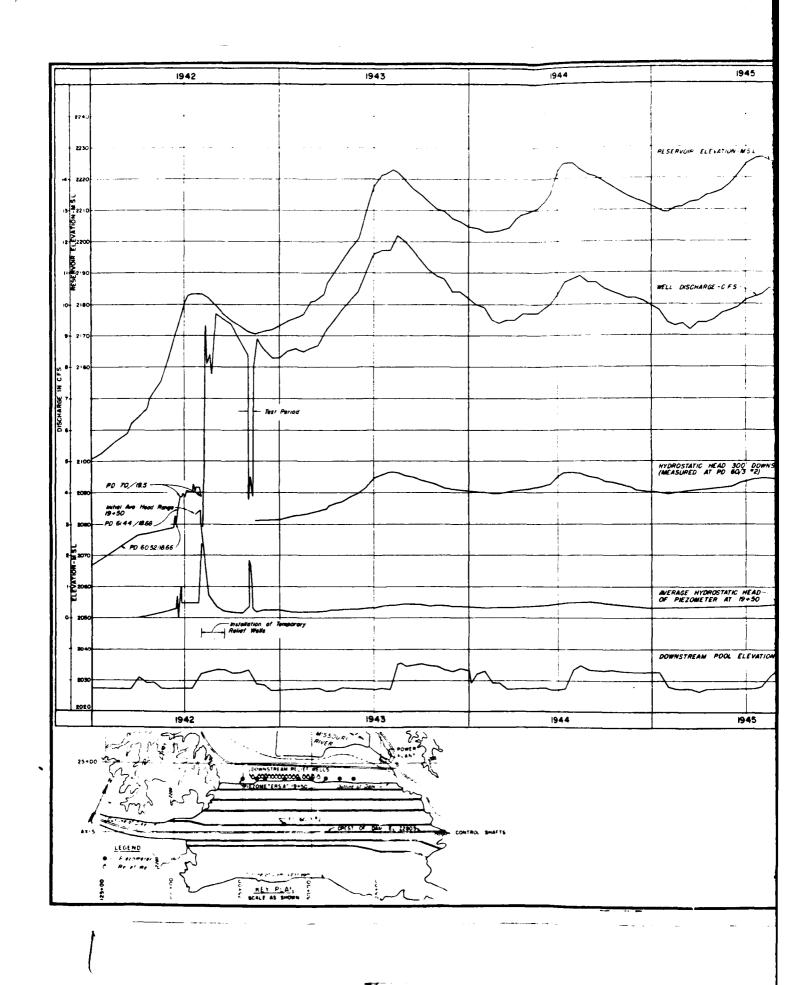
A SECTION OF THE SECT

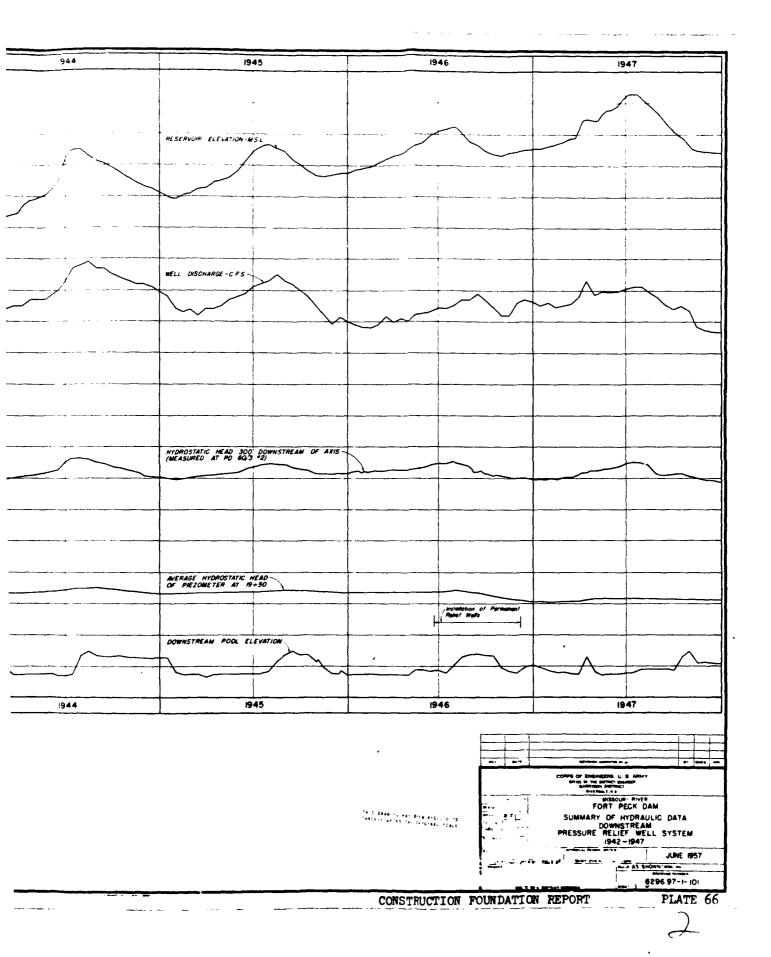
F-14 191



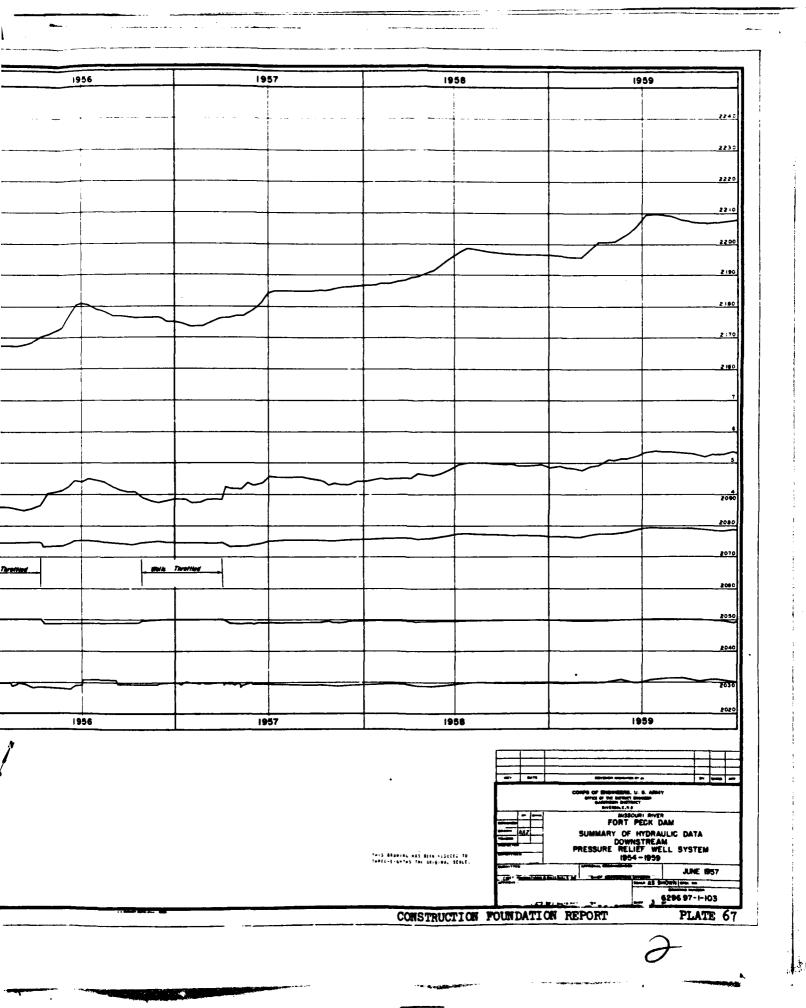


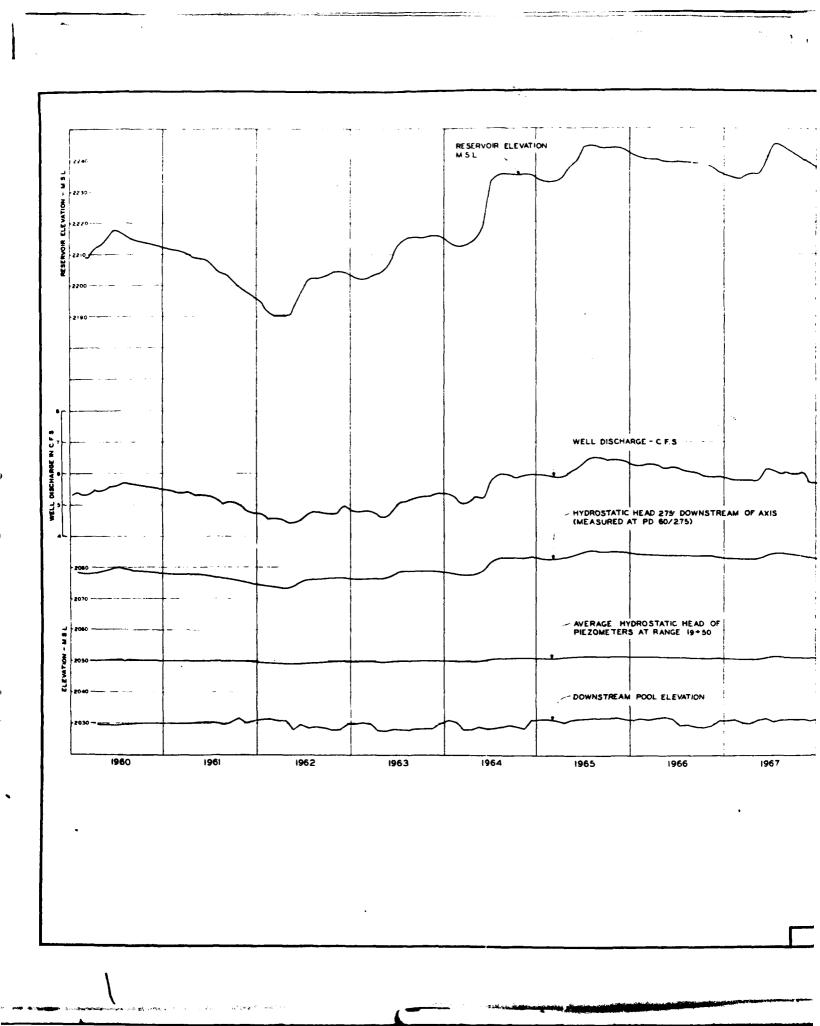


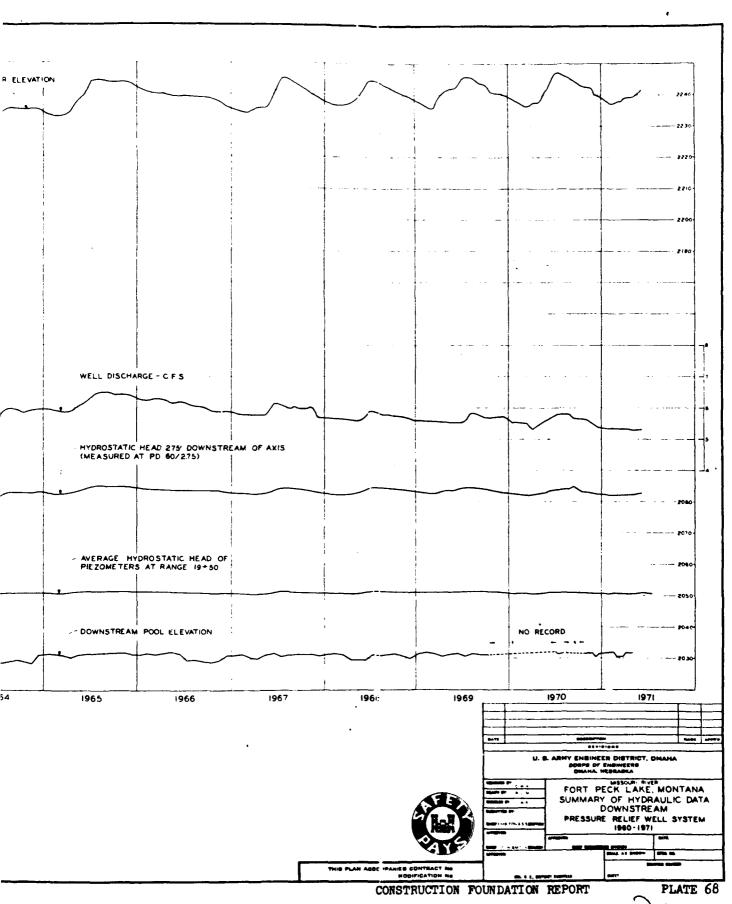


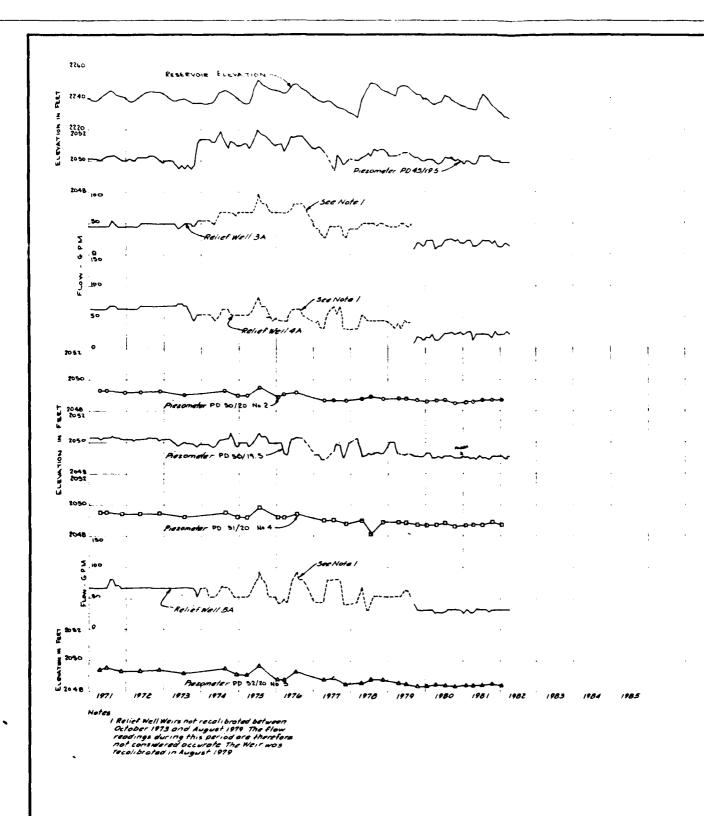


1954 1956 1955 224 RESERVOIR ELEVATION - M.S.L. DISCHARGE IN CFS WELL DISCHARGE C.F.S HYDROSTATIC HEAD 278' DOWNSTREAM OF AXIS MEASURED AT PO 80/278) Threffled AVERAGE HYDROSTATIC HEAD OF PIEZOMETERS AT RANGE 19+30 - DOWNSTREAM POOL ELEVATION 1956 1955 1954 2437 G DOWNSTIR AN RELIEF WELLS 1000 LEGEND SCALE AS SHOWN 2

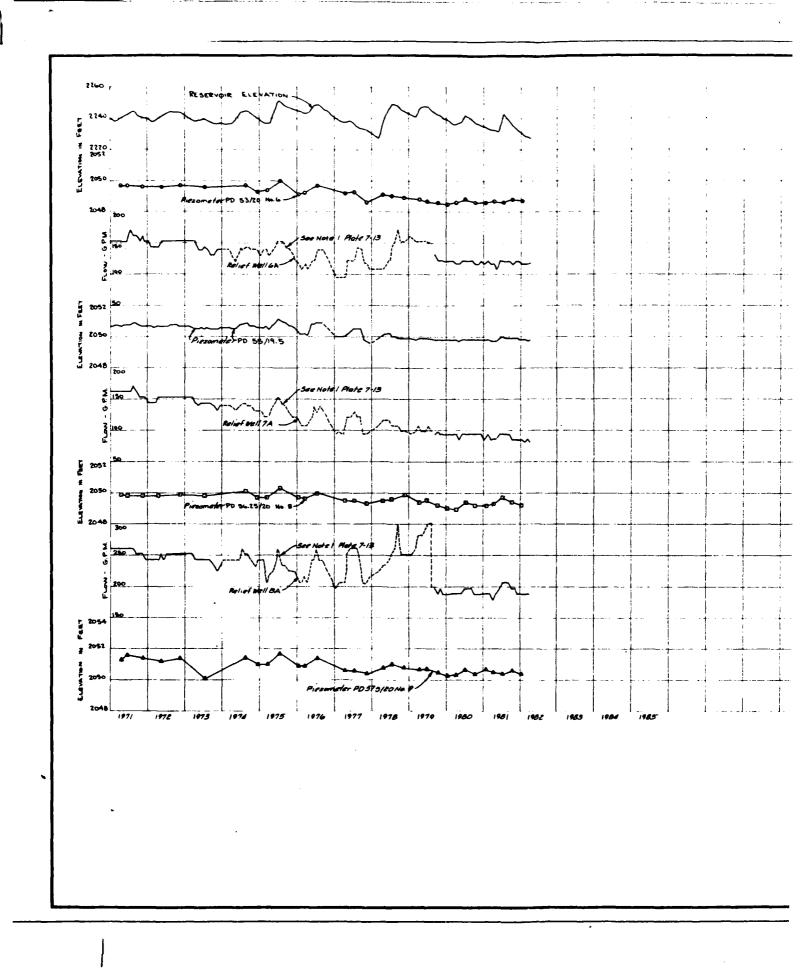




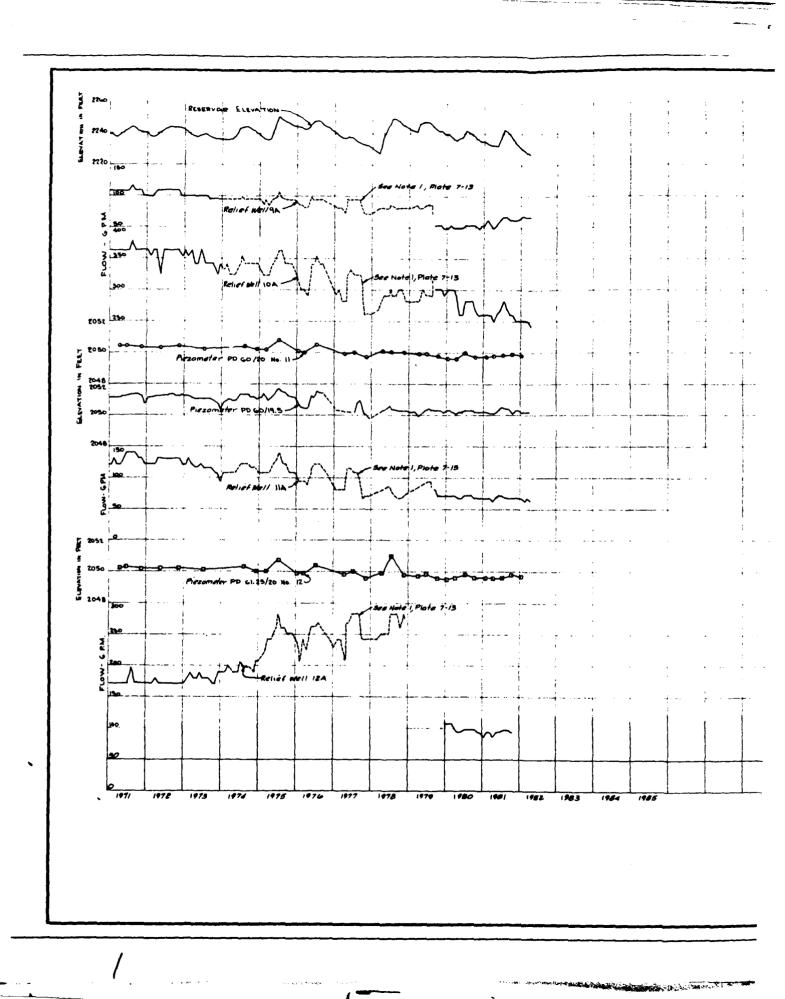




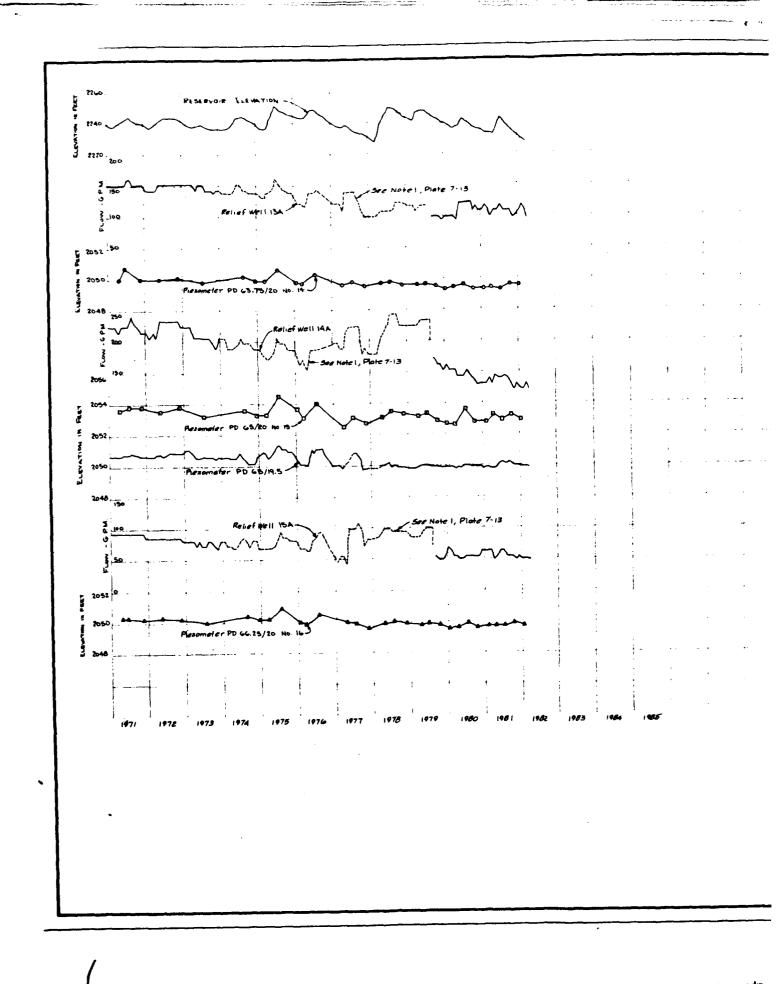
U. B. ARMY EMBINEER DISTRICT. DMAMA
DORRED OF EMBINEERS
OMAMA, NEBRABAS
MISSOURI RIVER
FORT PECK LAKE MONTANA
SUMMARY OF HYDRAULIC DATA FOR
DOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 151A, 46+00 - 52+00 PLATE 69 CONSTRUCTION FOUNDATION REPORT



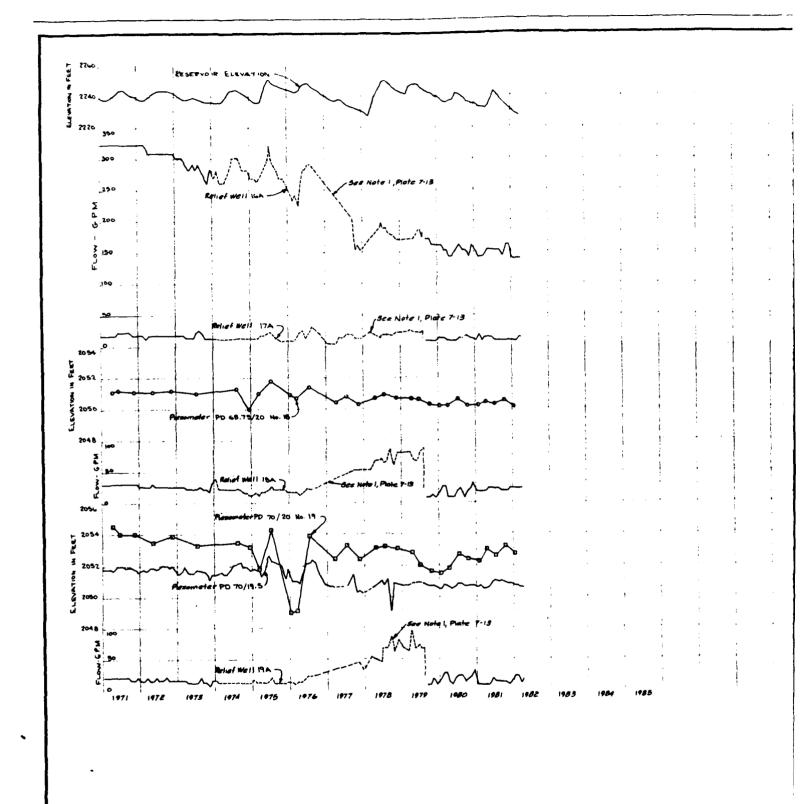
THIS DRAWING MAS BEEN REDUCED TO THREE-EIGHTHS THE BRIGIDAL SCALE. MISSOURI RIVER
FOUT PECK LAKE MONTANA
SUMMARY OF HYDRAULIC DATA FOR
BOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 CONSTRUCTION FOUNDATION REPORT PLATE 70



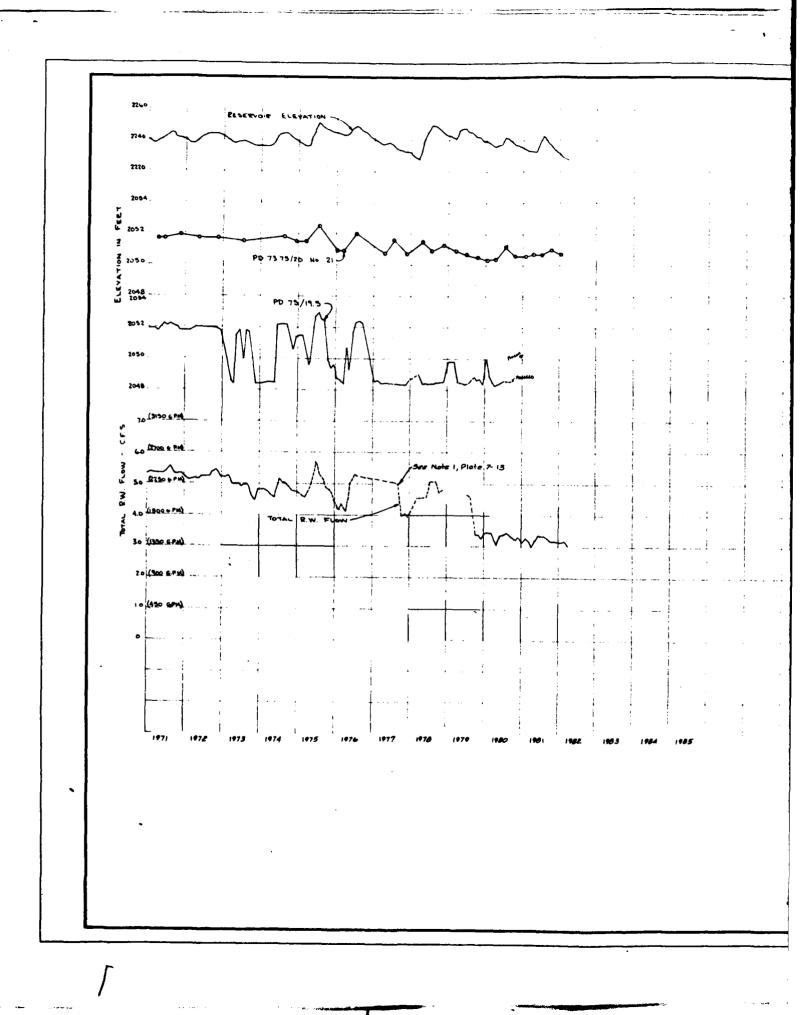
1982 1983 1984 1985 MISSOURI RIVER
FORT PECK LAKE MONTAMA
SUMMARY OF HYDRAULIC DATA FOR
BOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 CONSTRUCTION FOUNDATION REPORT PLATE 71



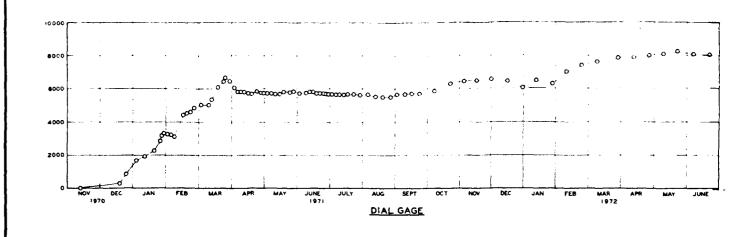
MISSOURI RIVER
PORT PECK LAKE MONTAMA
SUMMARY OF HYDRAULIC DATA FOR
DOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 CONSTRUCTION FOUNDATION REPORT PLATE 72

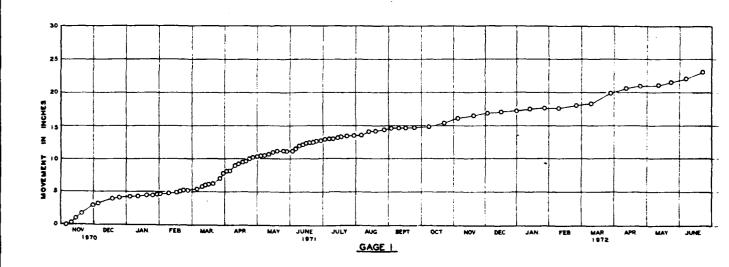


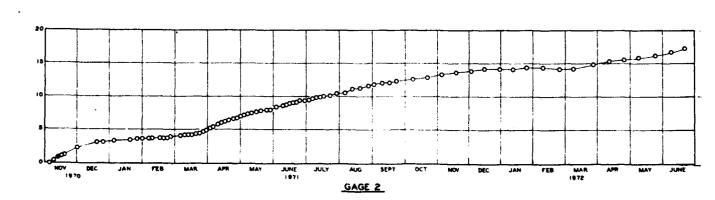
THIS BRANING HAS BEEN REDUCED TO THEREE-E GRESS THE BRISINAL SCALE. MISSOURI RIVER
PORT PECK LAKE MONTANA
SUMMARY OF HYDRAULIC DATA FOR
BOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 CONSTRUCTION FOUNDATION REPORT PLATE 73.



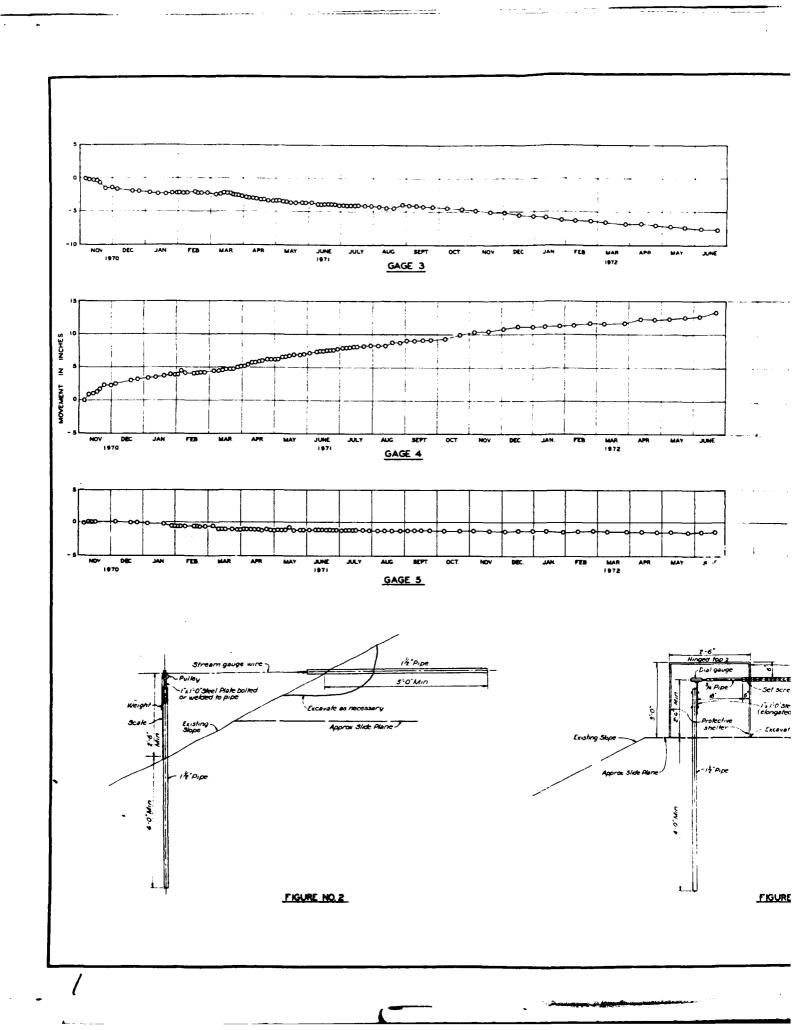
THIS DRAWING HAS DEED REDUCED TO THREE-EIGHTHS THE DRIGINAL SCALE. MISSOURI RIVER
FORT PECK LAKE MONTANA
SUMMARY OF HYDRAULIC DATA FOR
BOWNSTREAM PRESSURE RELIEF WELL SYSTEM, 1971 - 1982 15TA, 72+00 - 74+00 CONSTRUCTION FOUNDATION REPORT PLATE 74

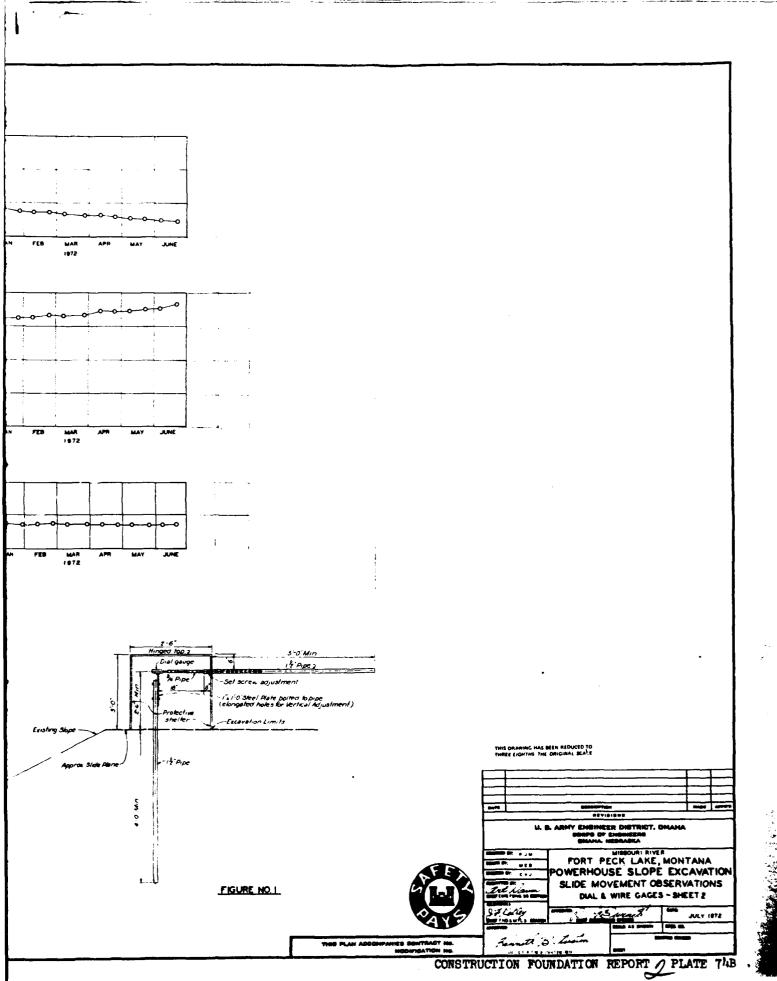


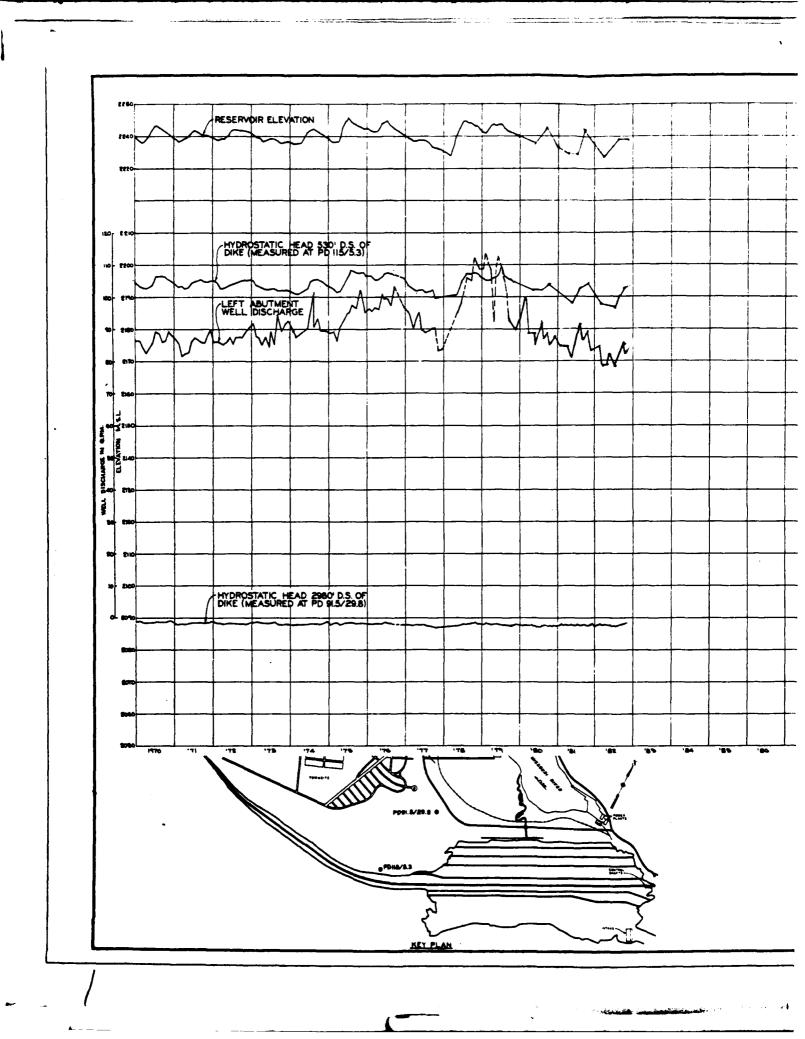


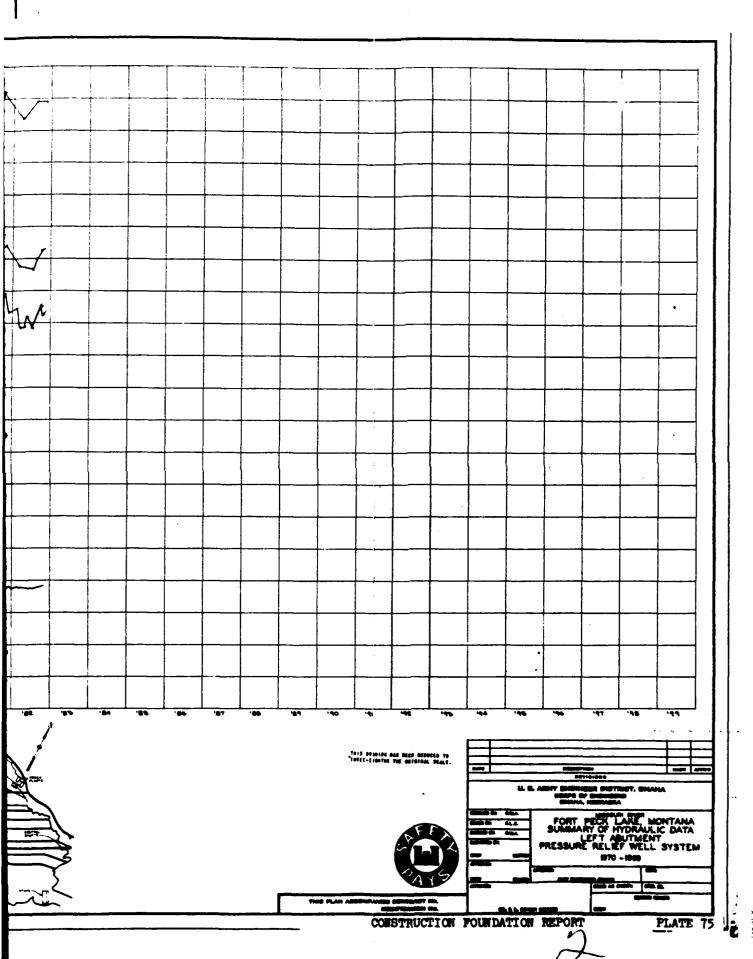


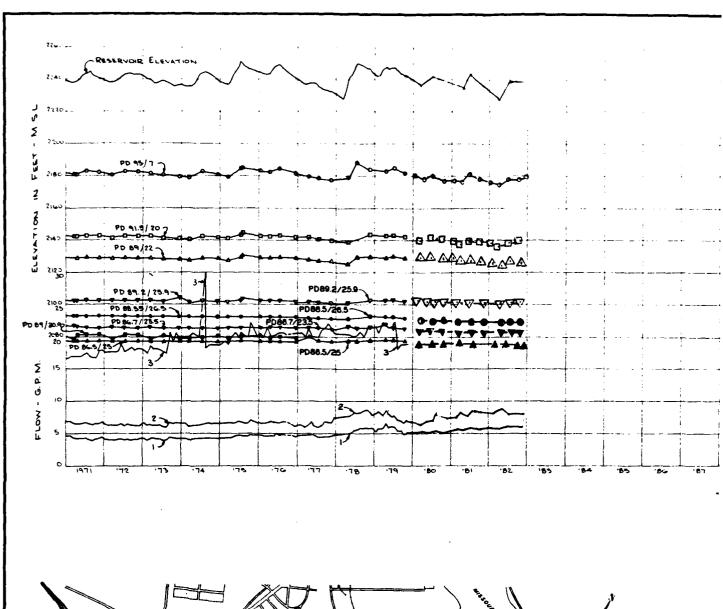
MAR 1972 JAN JUNE THIS DRAWING HAS BEEN REDUCED TO THREE EIGHTHS THE ORIGINAL SCALE U. S. ARMY ENSINEER DISTRICT, OMAMA COMPS OF ENSINEERS SMAMA, NESSASKA MAR 1972 FEB MISSOURI RIVER
FORT FECK LAKE, MONTANA
POWERHOWSE SLOPE EXCAMATION
SLIDE MOVEMENT OBSERVATIONS
DIAL & WIRE GAGES - SHEET I m 66 u g a 97 Glia 12 was JULY 1972 France Si leater PLATE 74A CONSTRUCTION FOUNDATION REPORT

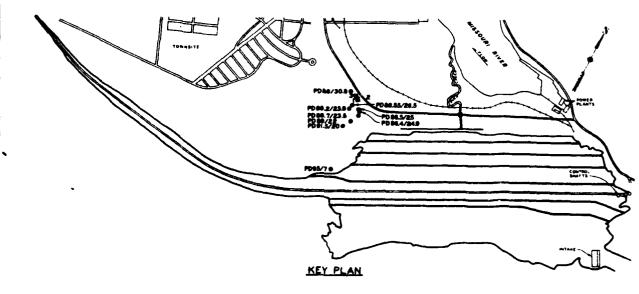




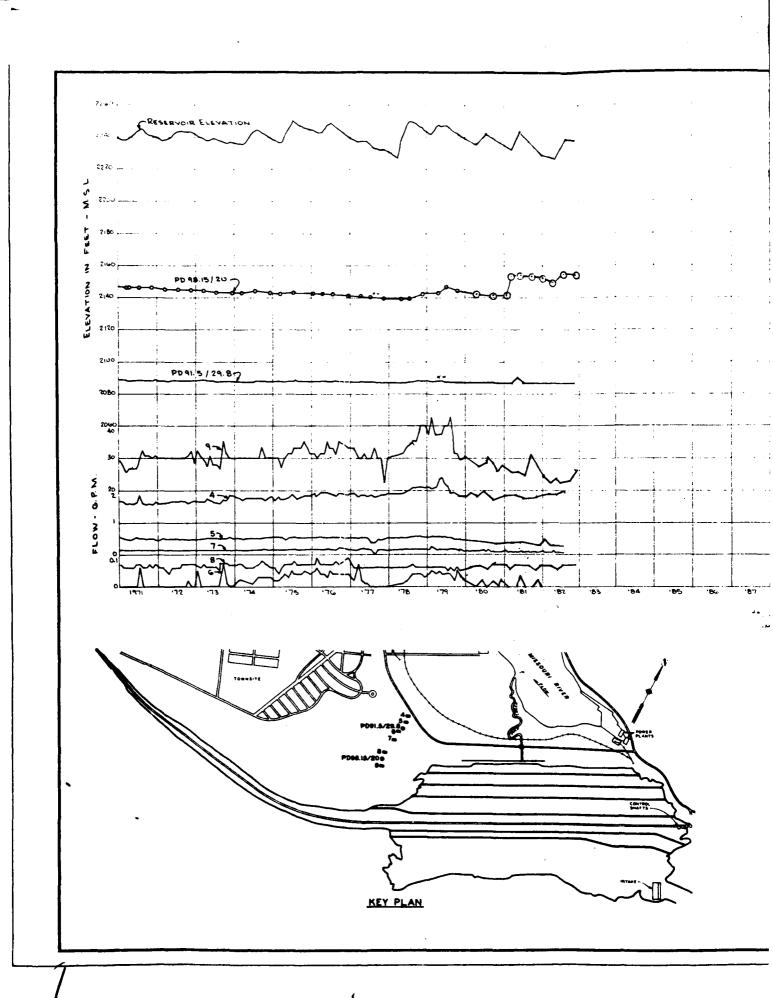




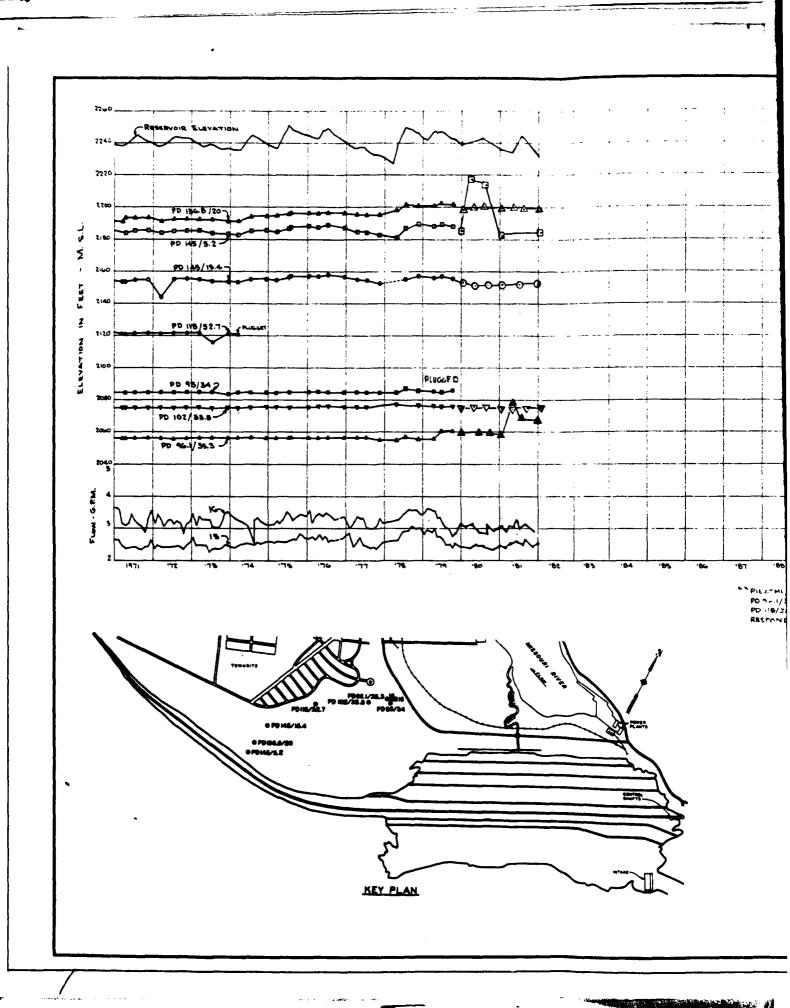


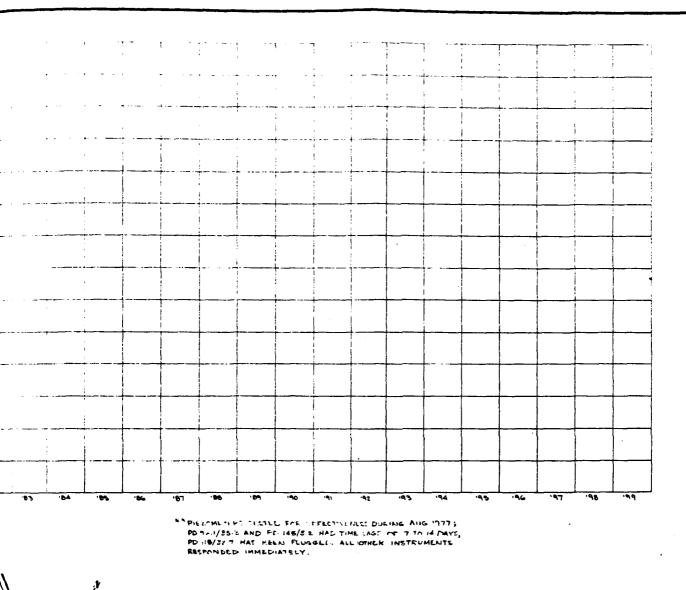


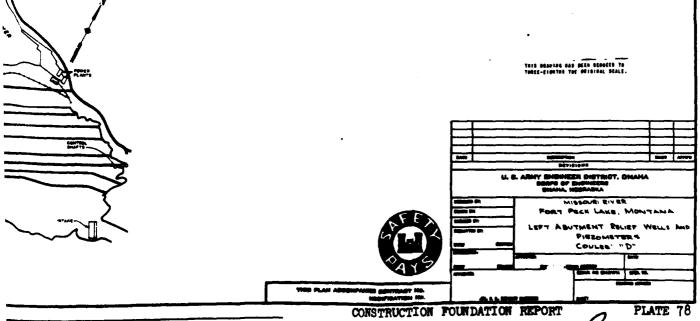
3-043 e.2△A ~\$v\$₹₹?. ć8' .82 88 AND IN THE PERSON OF THE PERSO u. B. Army endincer district, dimama compo of endincers ghama, nebrabia LEPT ABUT MENT RELIEF WELLS & Conres. "B" PLATE 76 CONSTRUCTION FOUNDATION REPORT

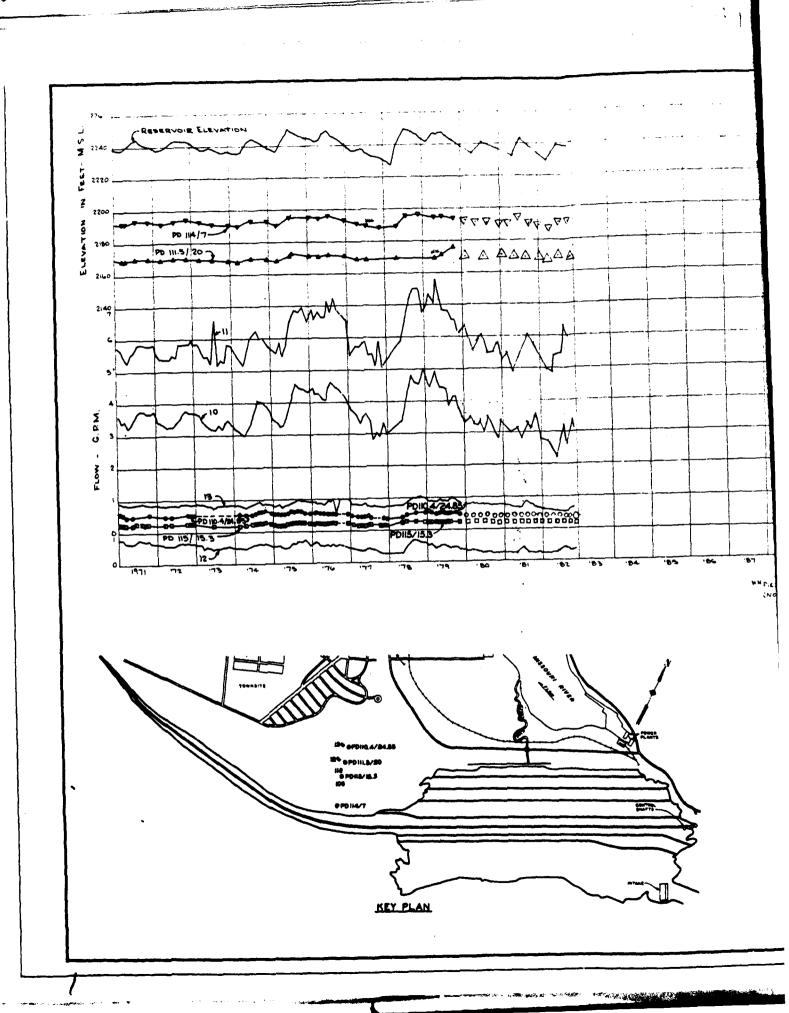


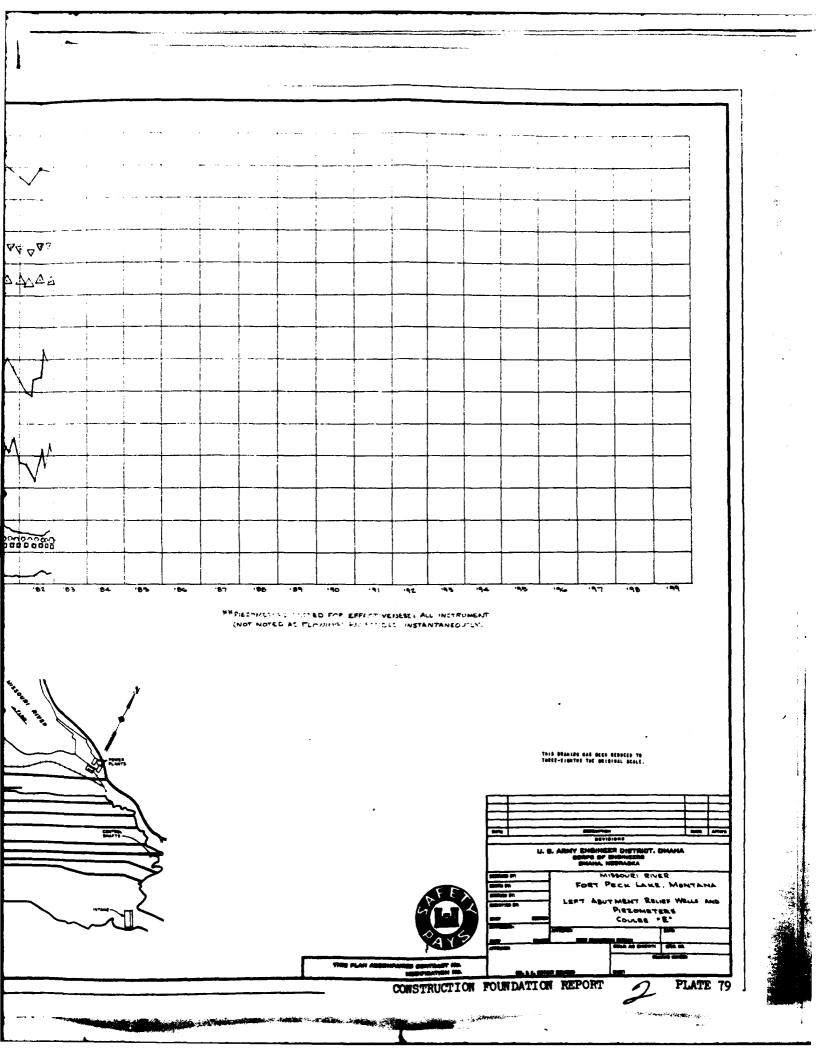
.95 ۲۵۰ .43 94 .00 THE THE THE PERSON AND ALL SECTIONS THE TANK LAG. THIS BRANING HAS BEEN REPUCED TO THREE-EIGHTHS THE BRIGINAL SCALE. CONSTRUCTION FOUNDATION REPORT PLATE 77

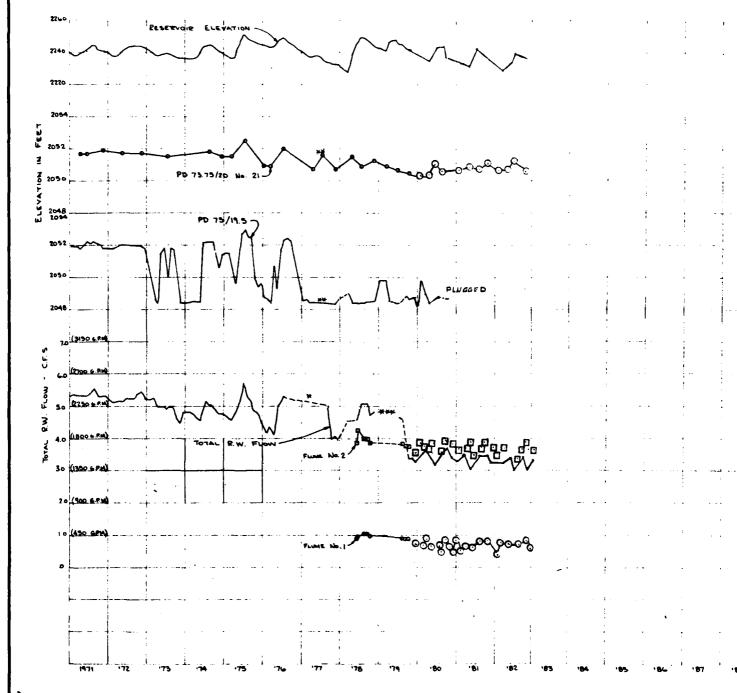




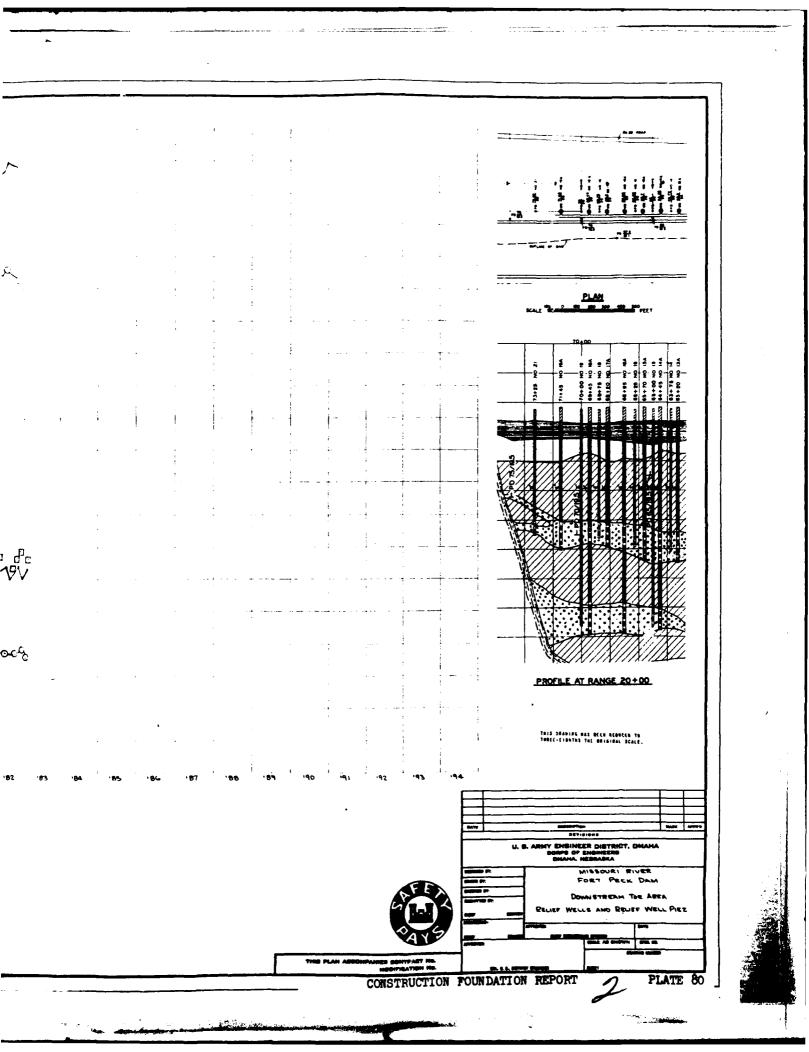


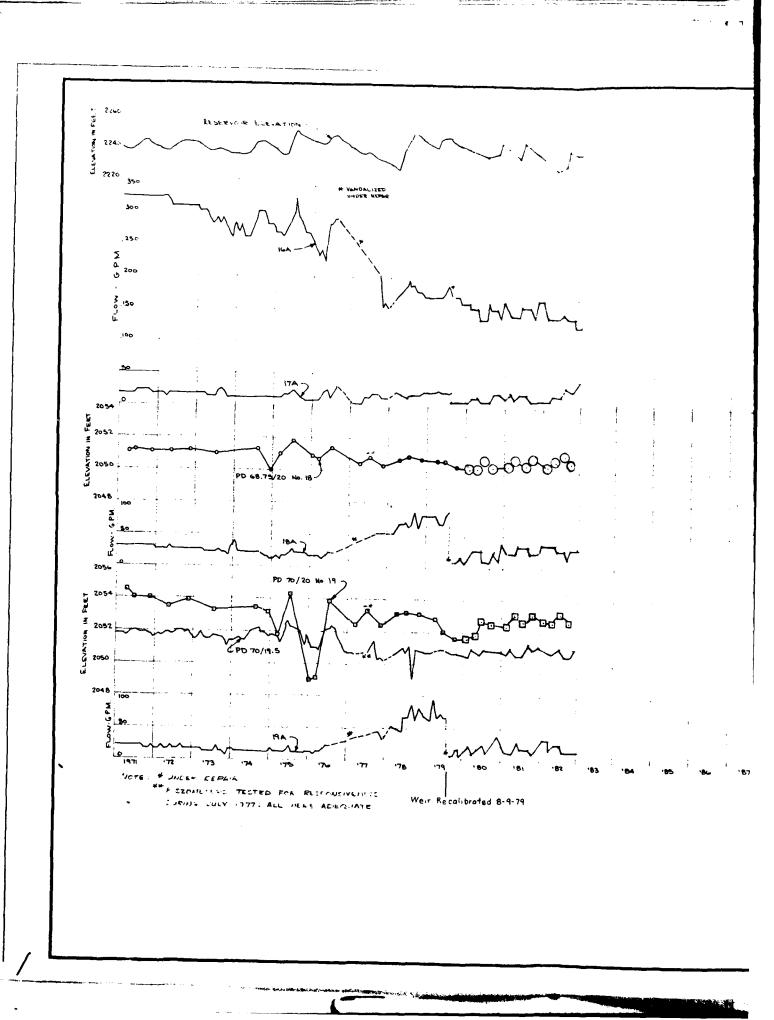


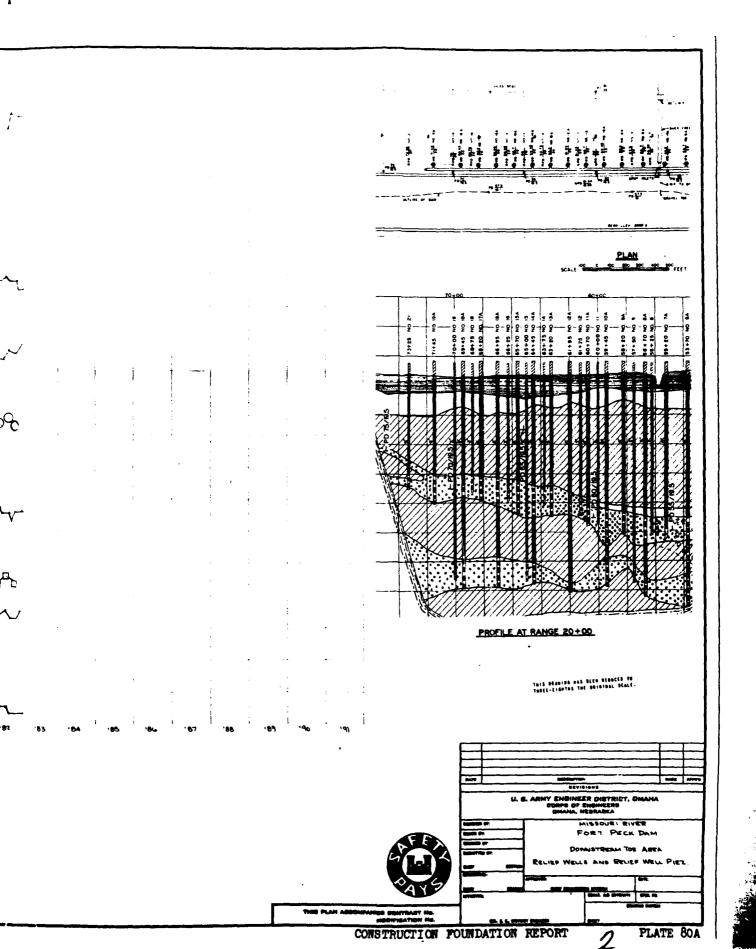




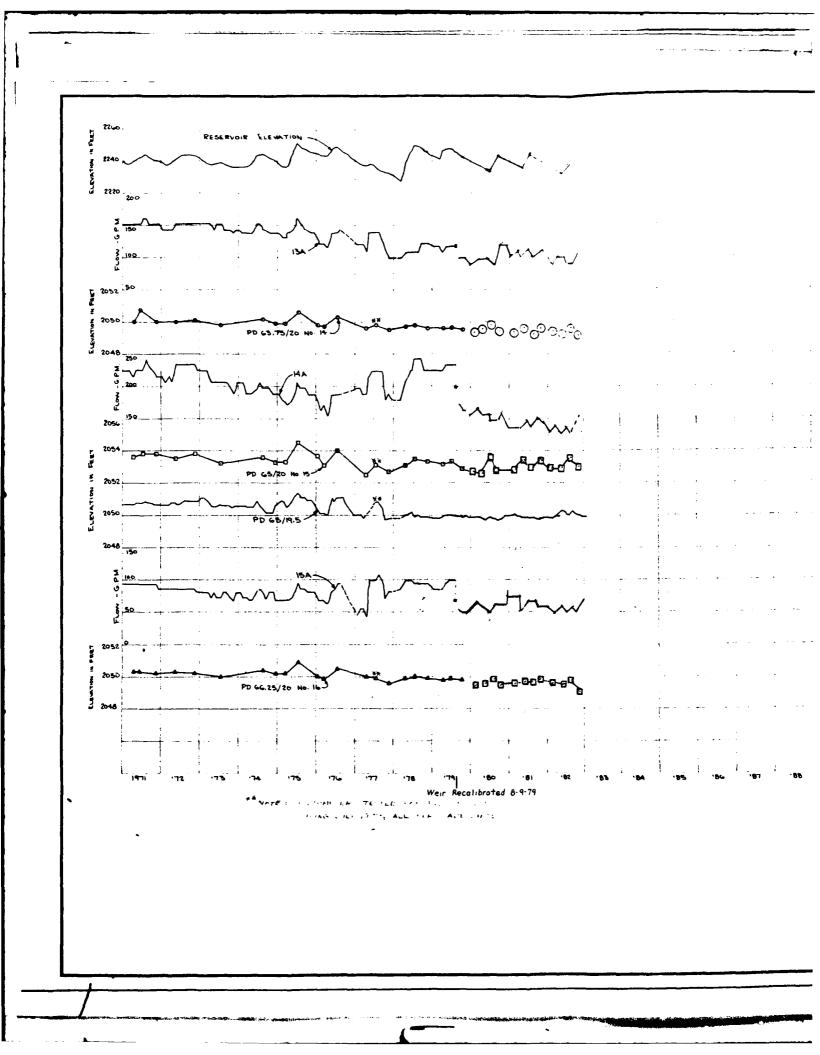
NOTE. TOTAL RELIEF WALL FLOW IS SUMMATION OF INDIVIDUAL R.W. FLOWS. THE SUM OF FLOME NO.1 AND FRIME NO. E SHOULD APPRISHMATE THE TOTAL R.W. FLOWS.
WELLS, IGA, IBA AND IBA UNDER REPAIR.
BY STATES FROM THE TOTAL FOR A PARTIE OF THE TOTAL PROPERTY OF THE TOTAL PROPER

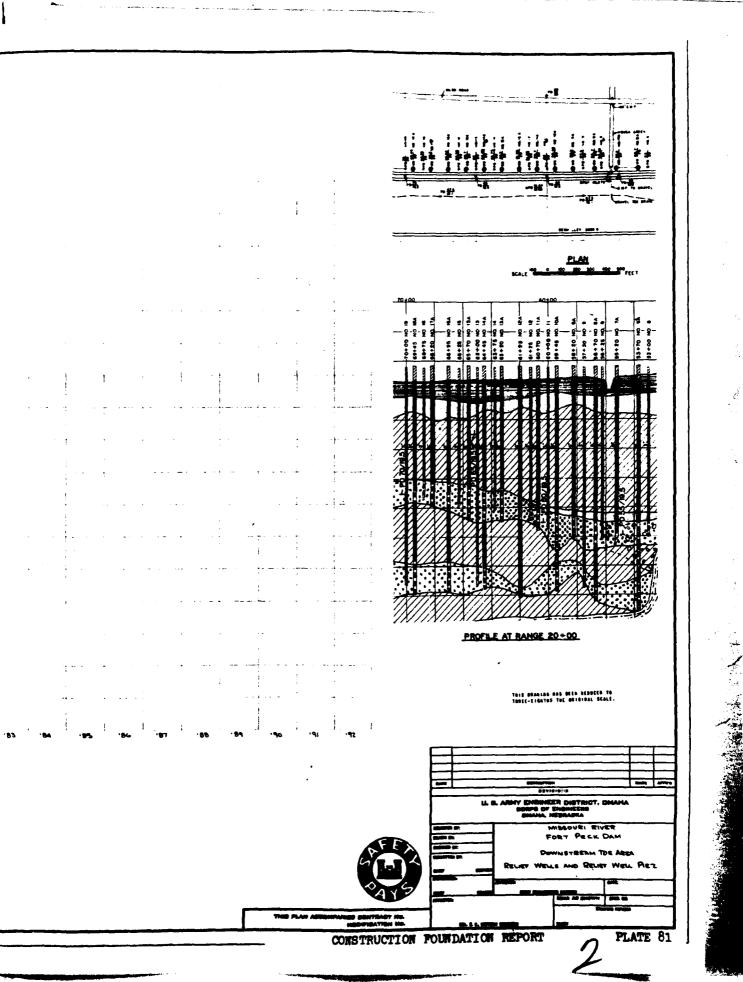






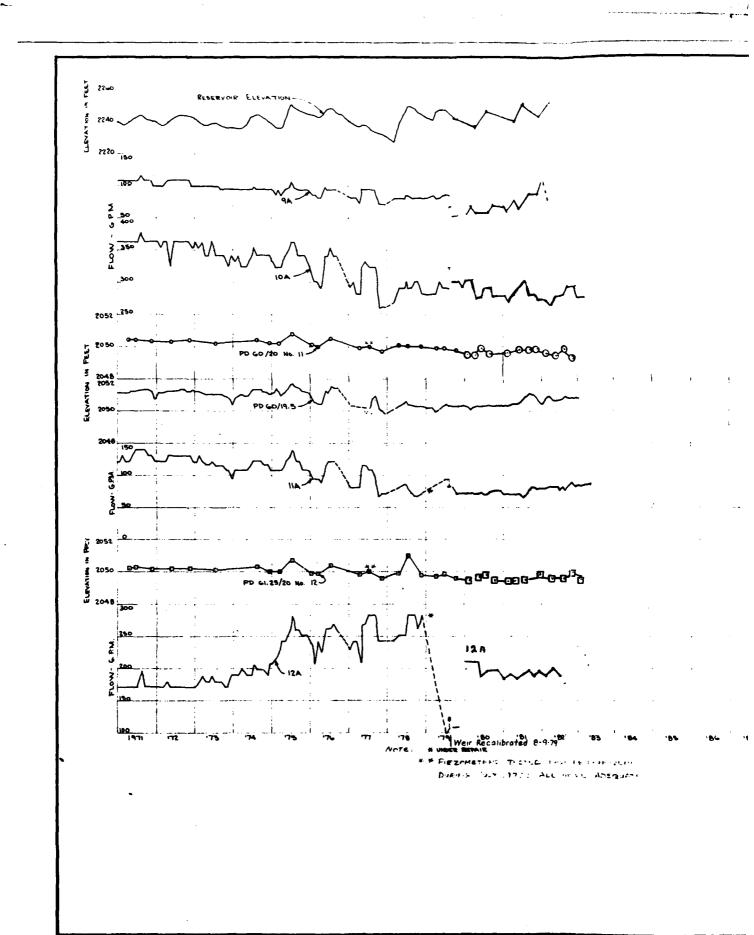
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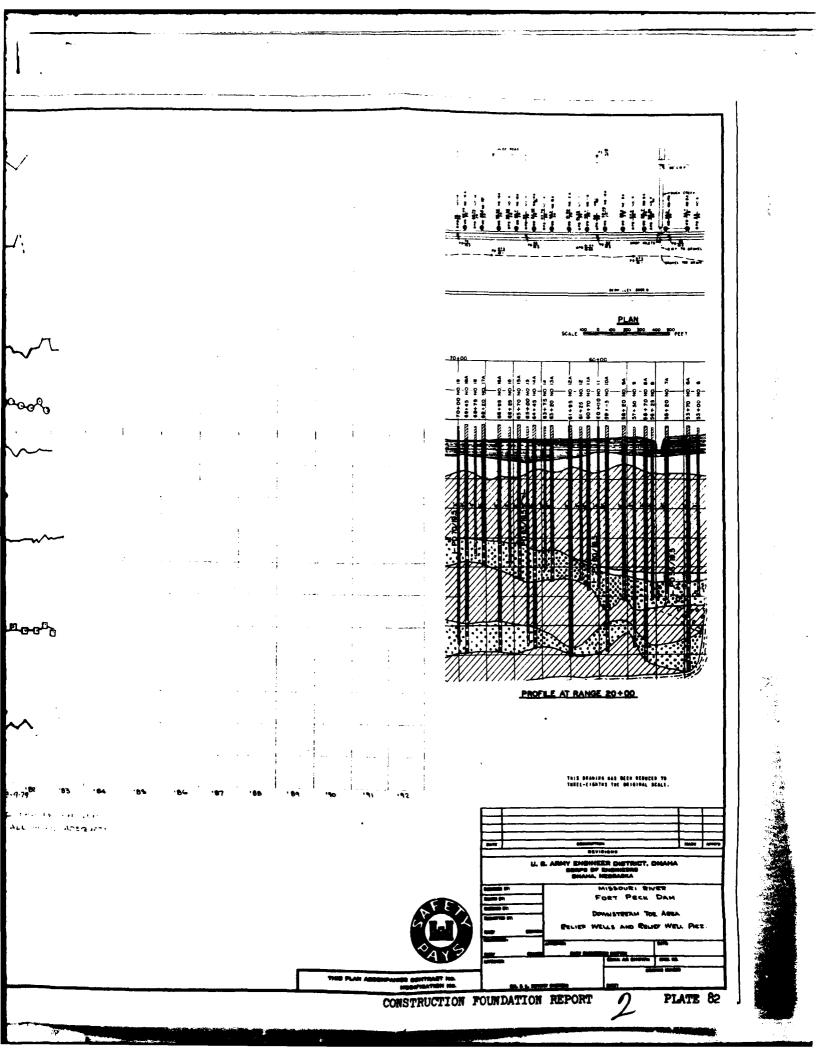


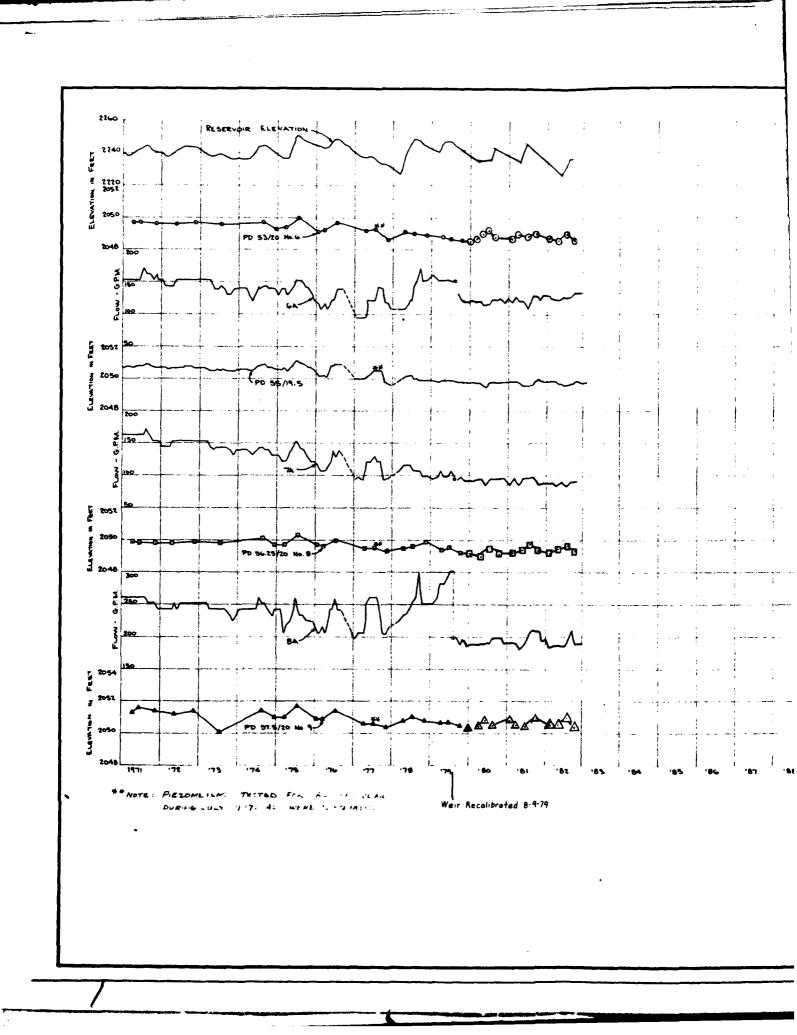
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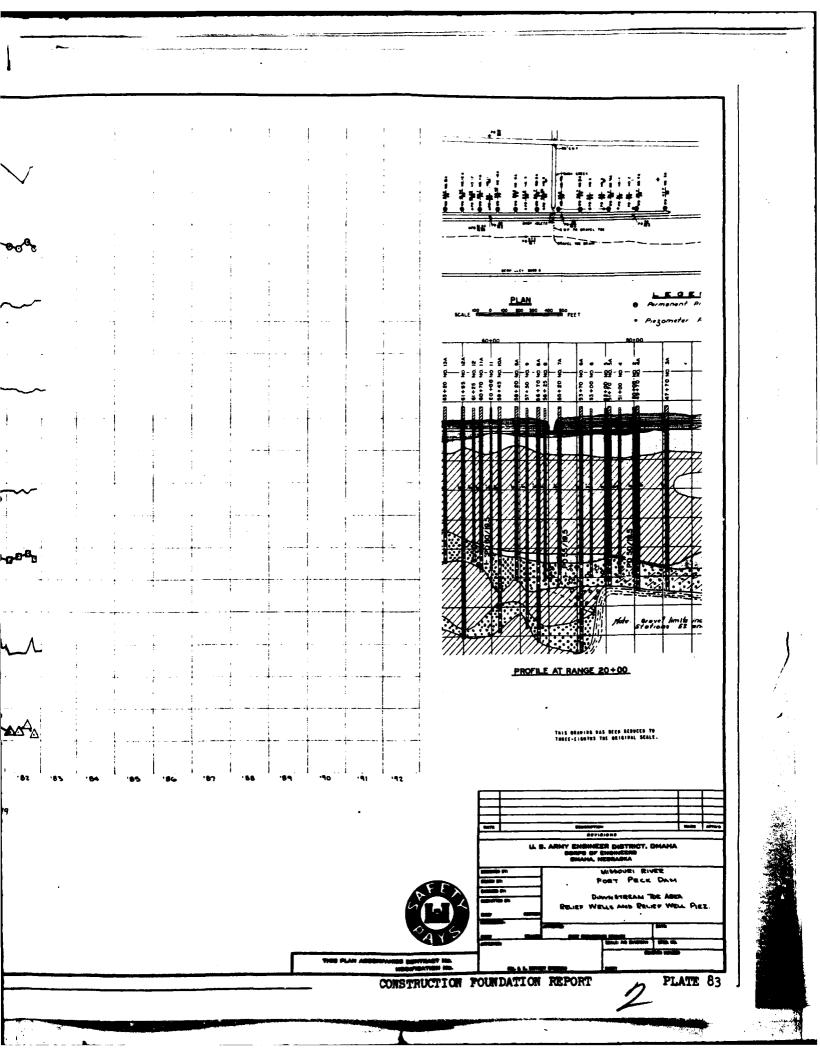
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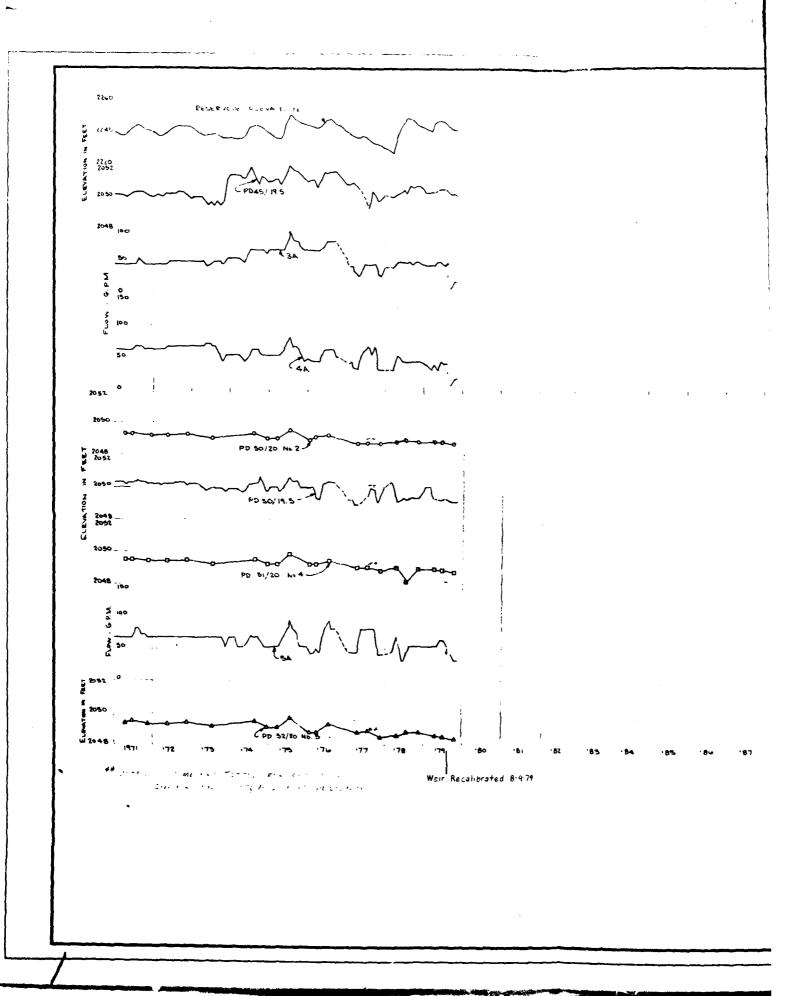


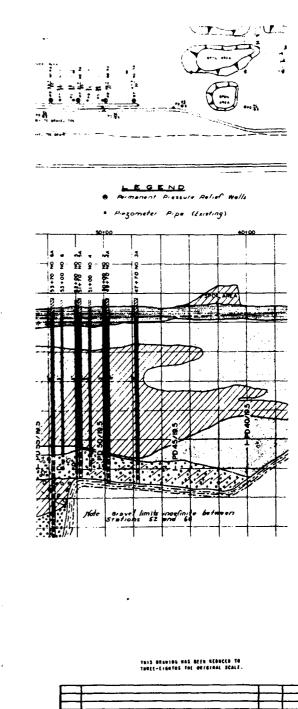
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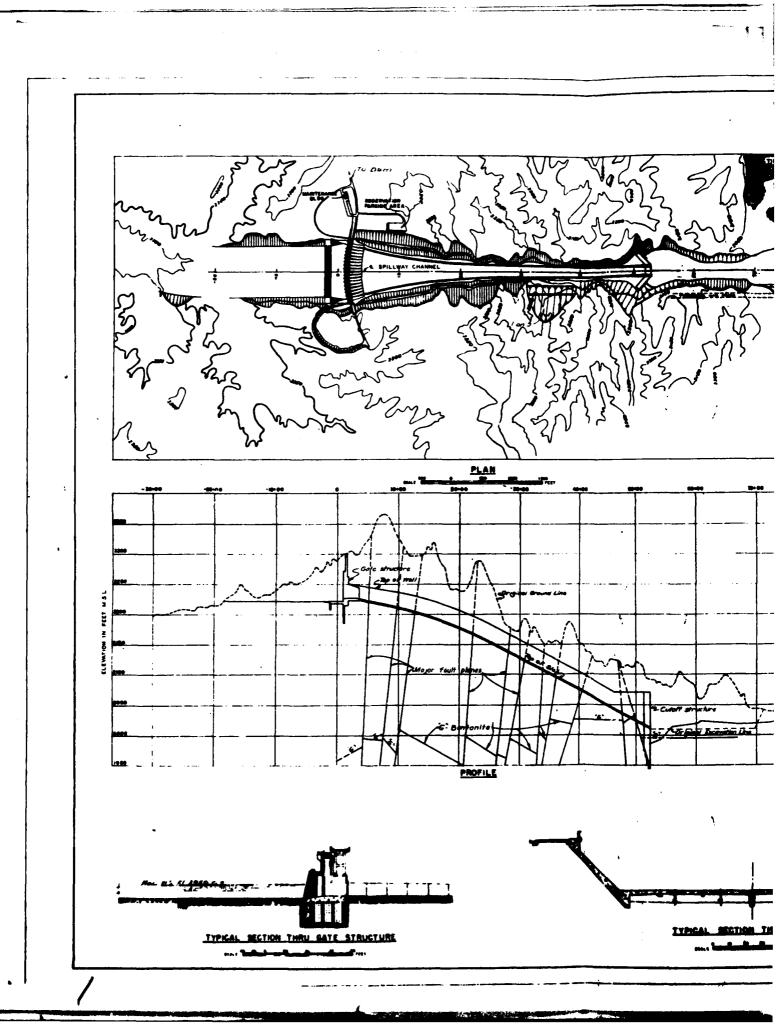


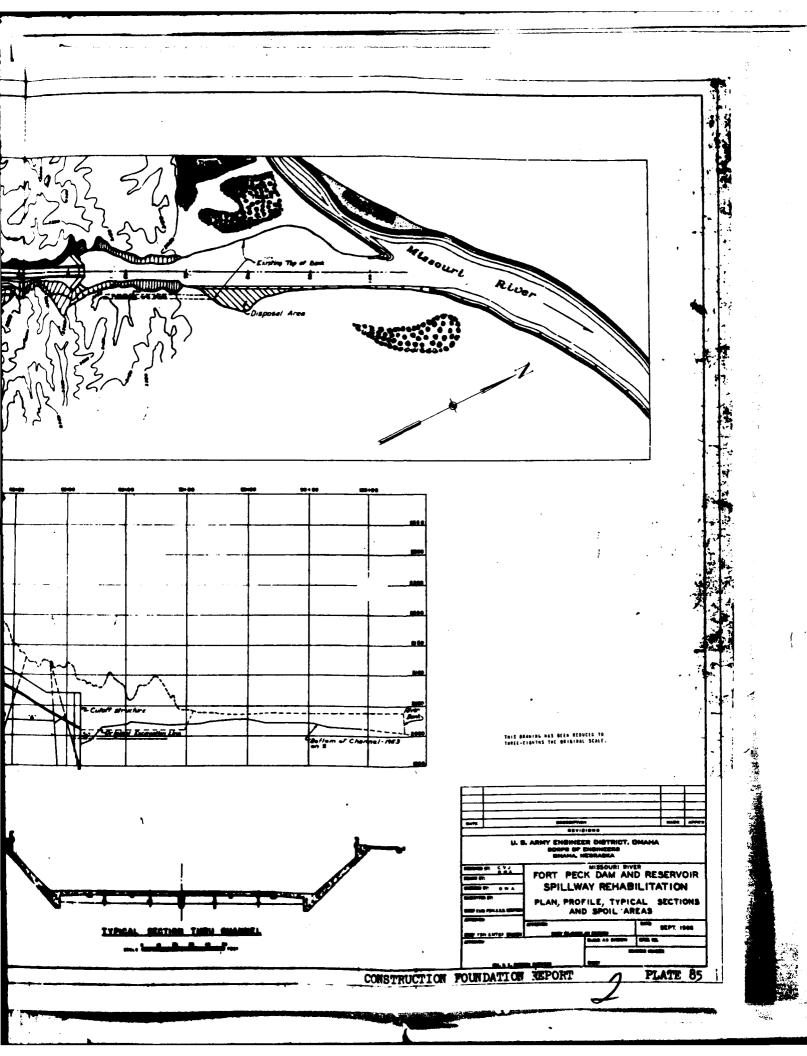






CONSTRUCTION FOUNDATION REPORT PLATE 84

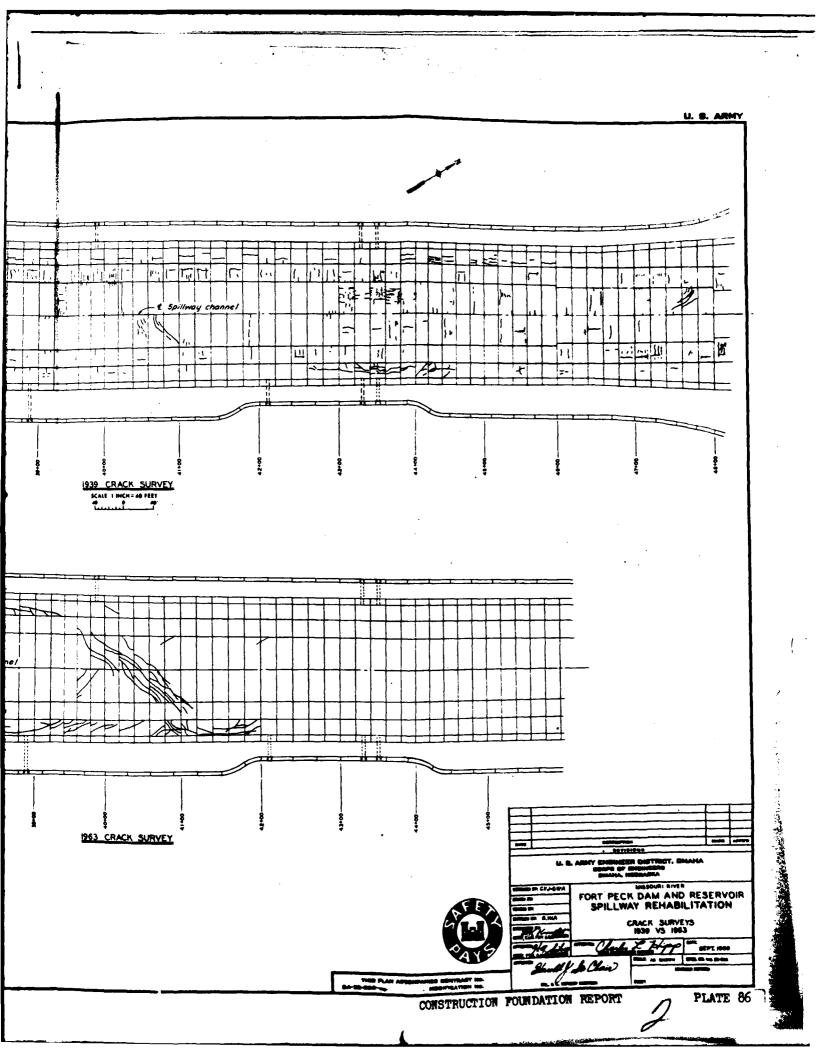


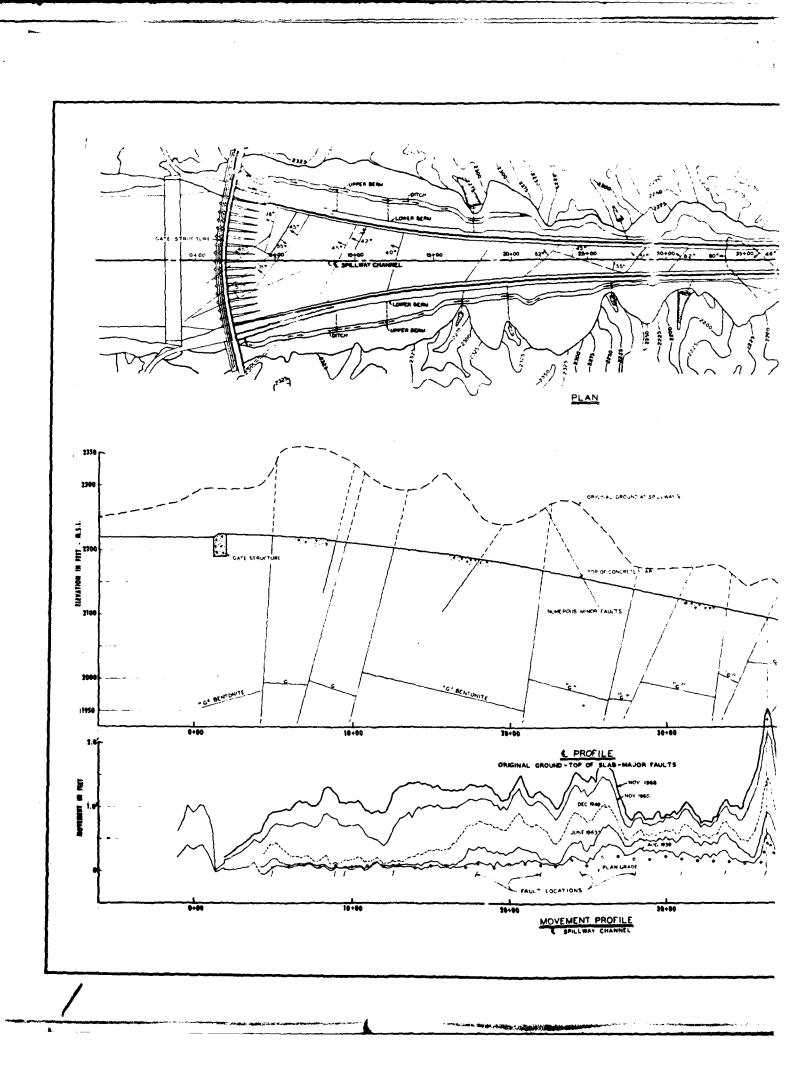


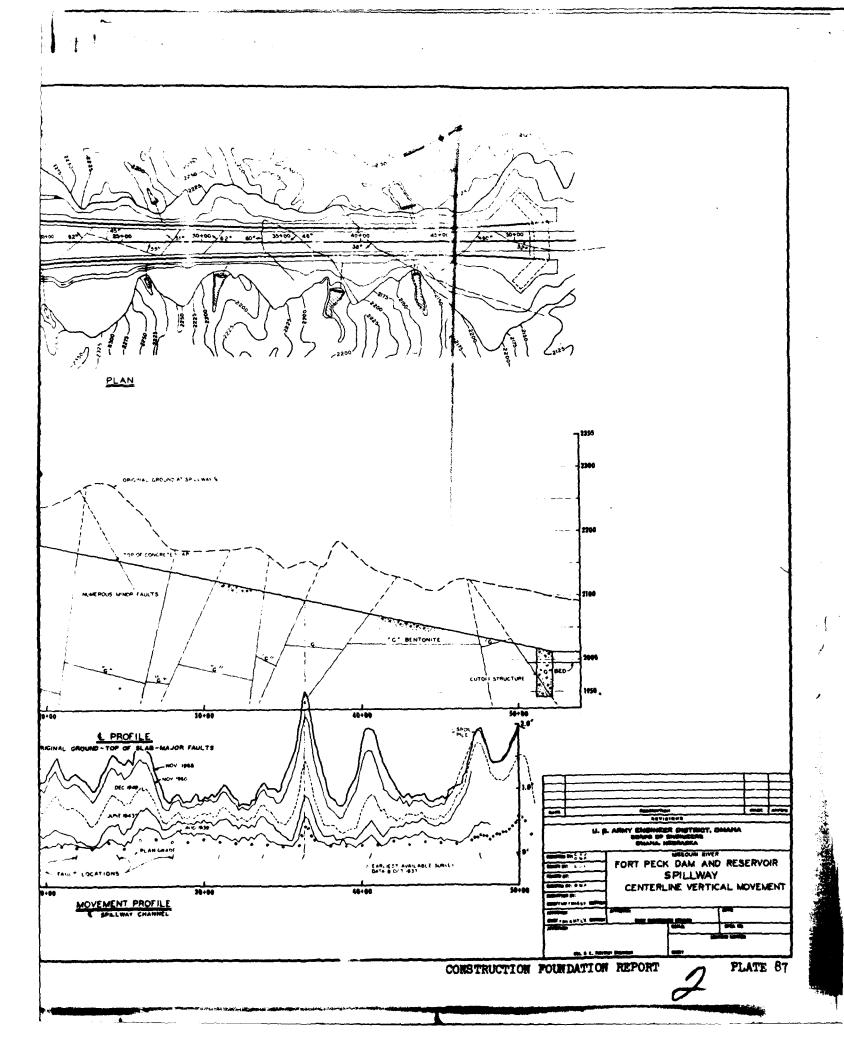
CONSTRUCTION FOUNDATION REPORT MISSOURI RIVER FORT PECK 3/4 MONTANA VOLUME 2 DRAWINGS(U) ARMY ENGINEER DISTRICT OMAHA NE JAN 83 AD A134 914 F/G 13/13 UNCLASSIFIED NI

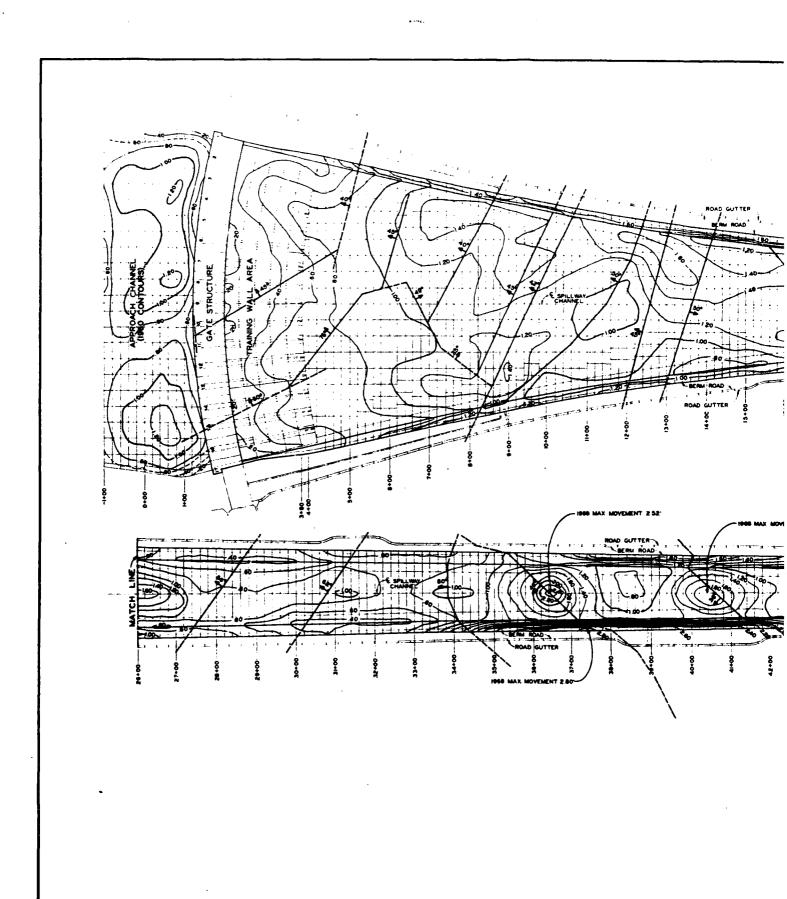


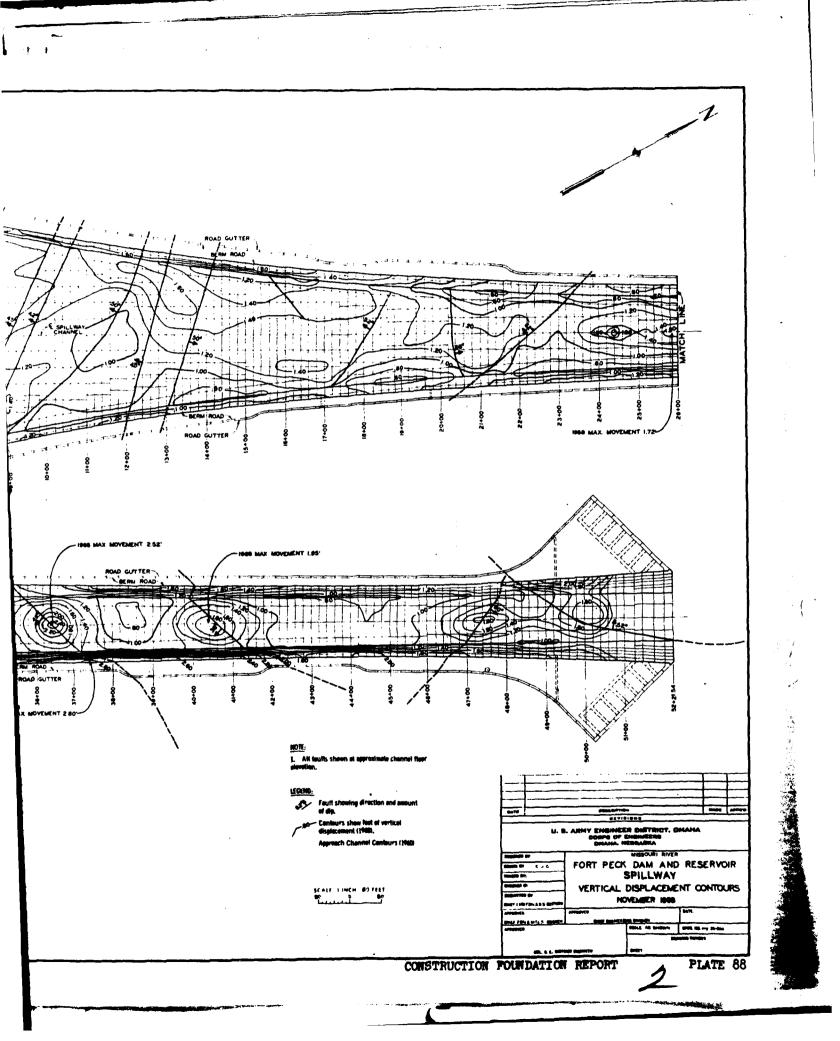
MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS - 1963 - A

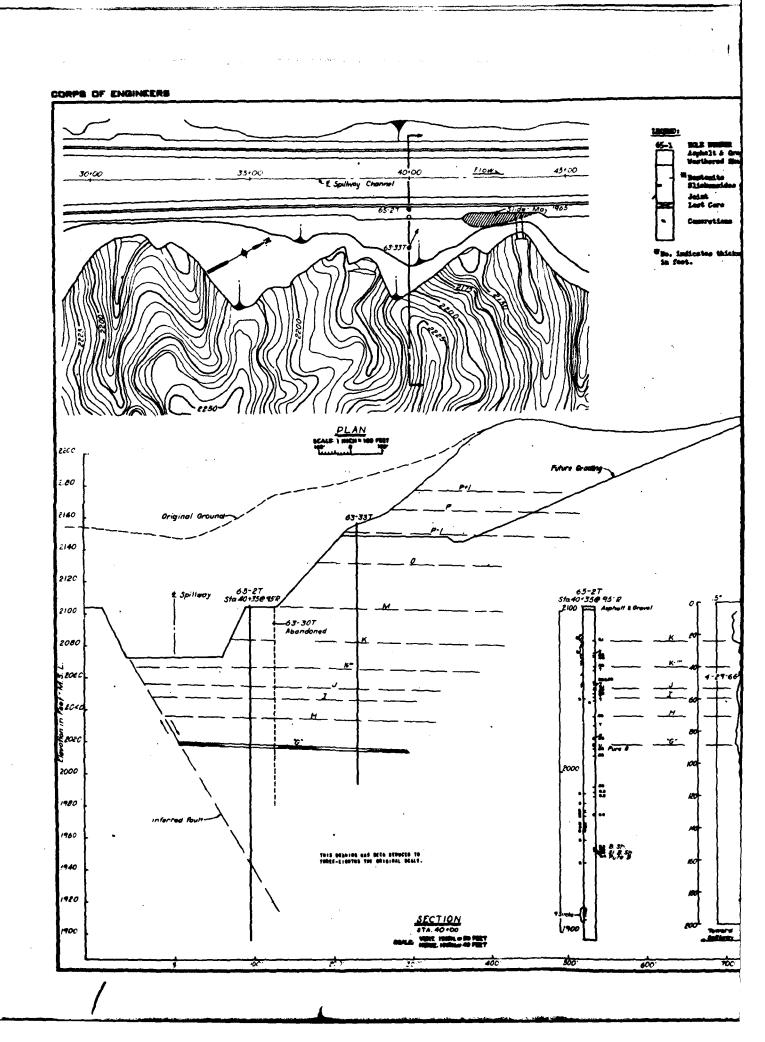


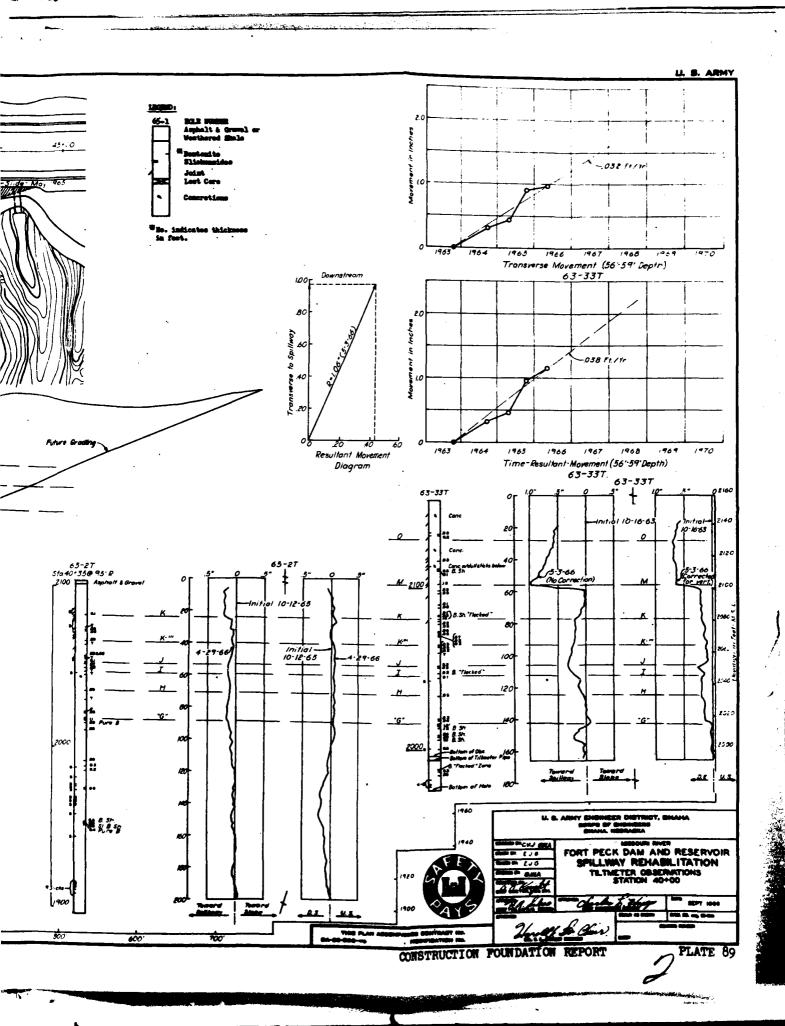




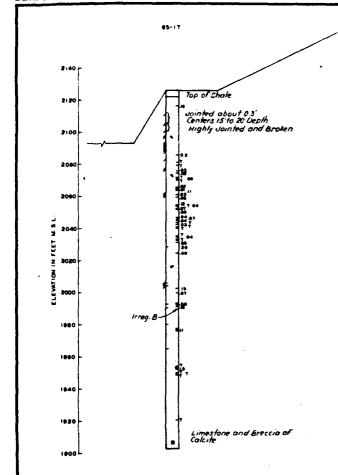


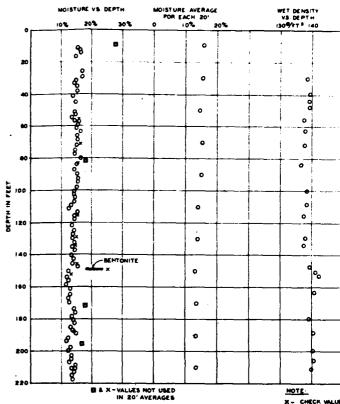




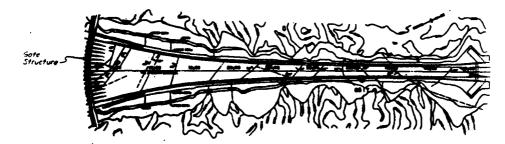








X - CHECK VALUE LABORATORY DURING TES



KEY PLAN

DEPTH		MOISTURE AVERAGE FOR EACH 20'		WET DENSITY VS. DEPTH	DRY DENSITY VS. DEPTH			VOID RATIO				PERCENT SATURATION				
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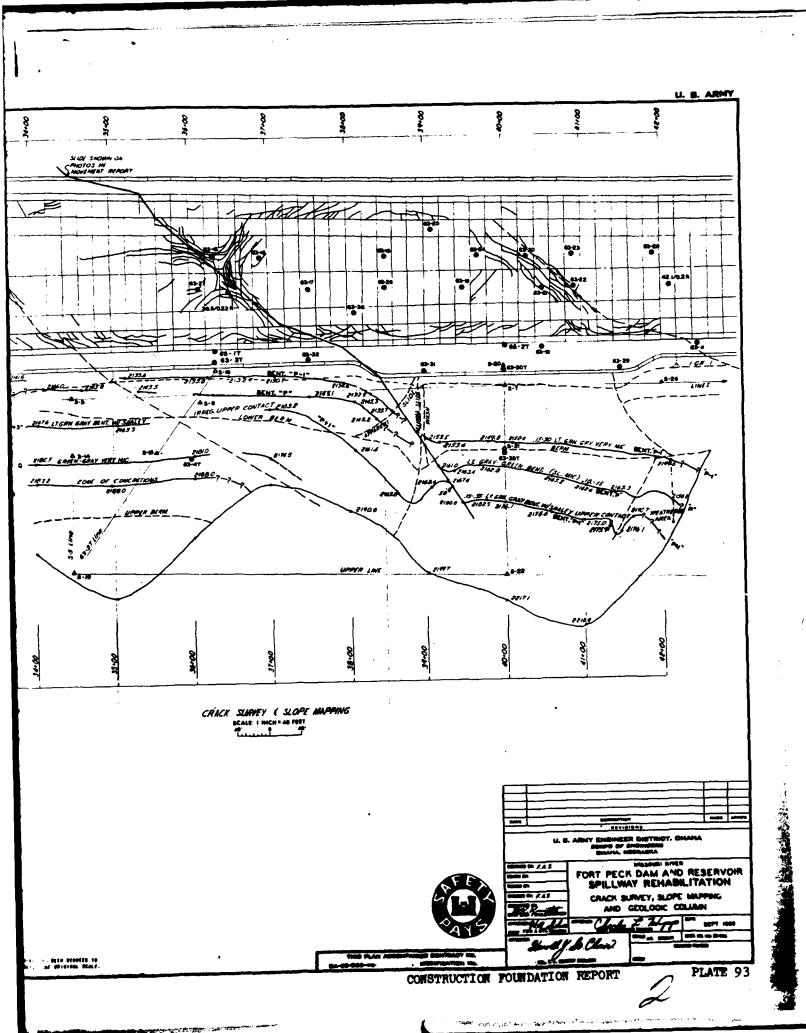
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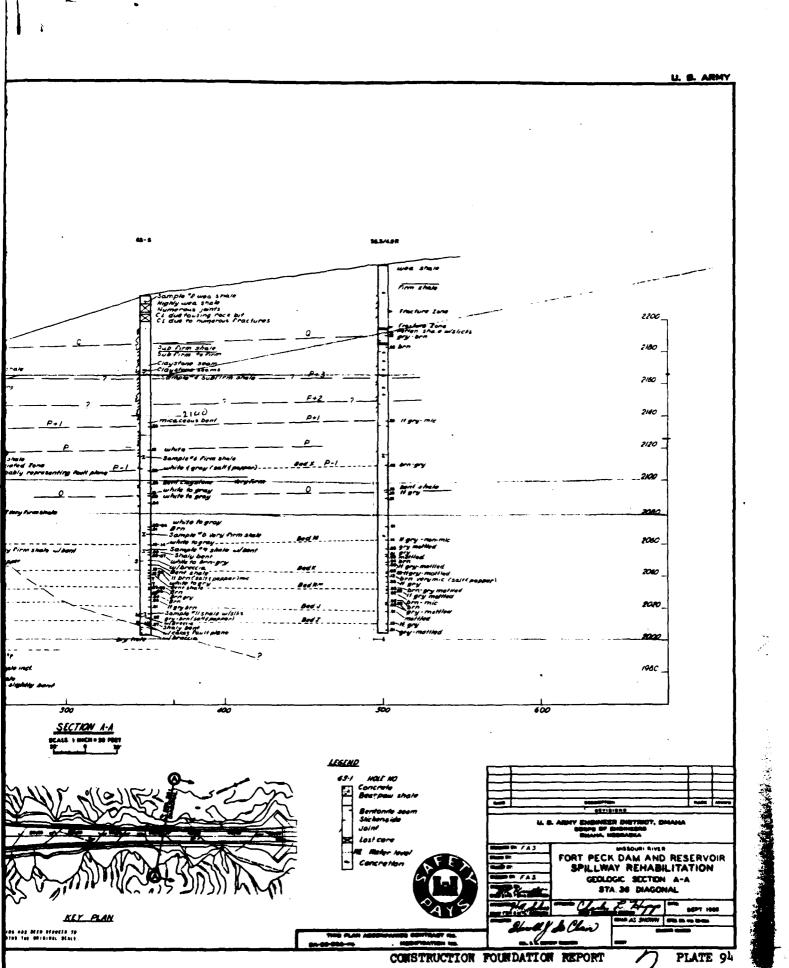
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CONSTRUCTION FOUNDATION REPORT

7 PLATE 91

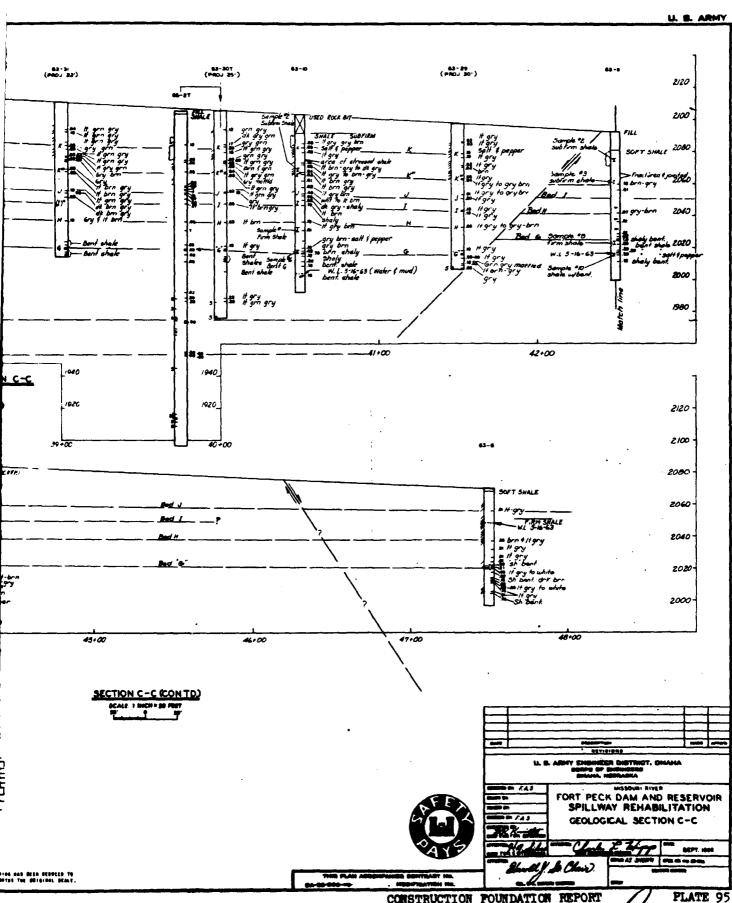
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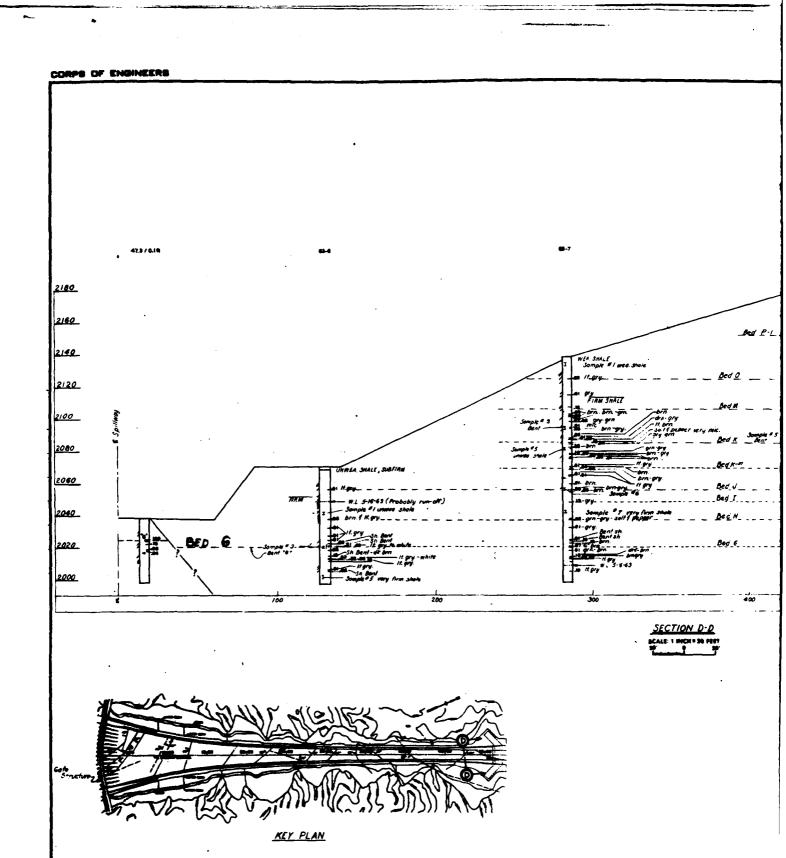


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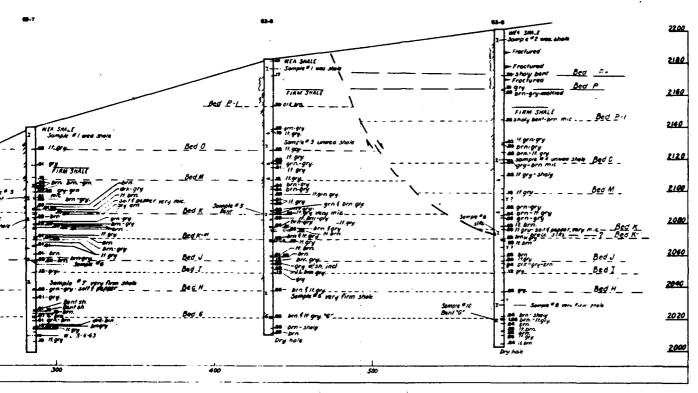


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CONSTRUCTION FOUNDATION REPORT

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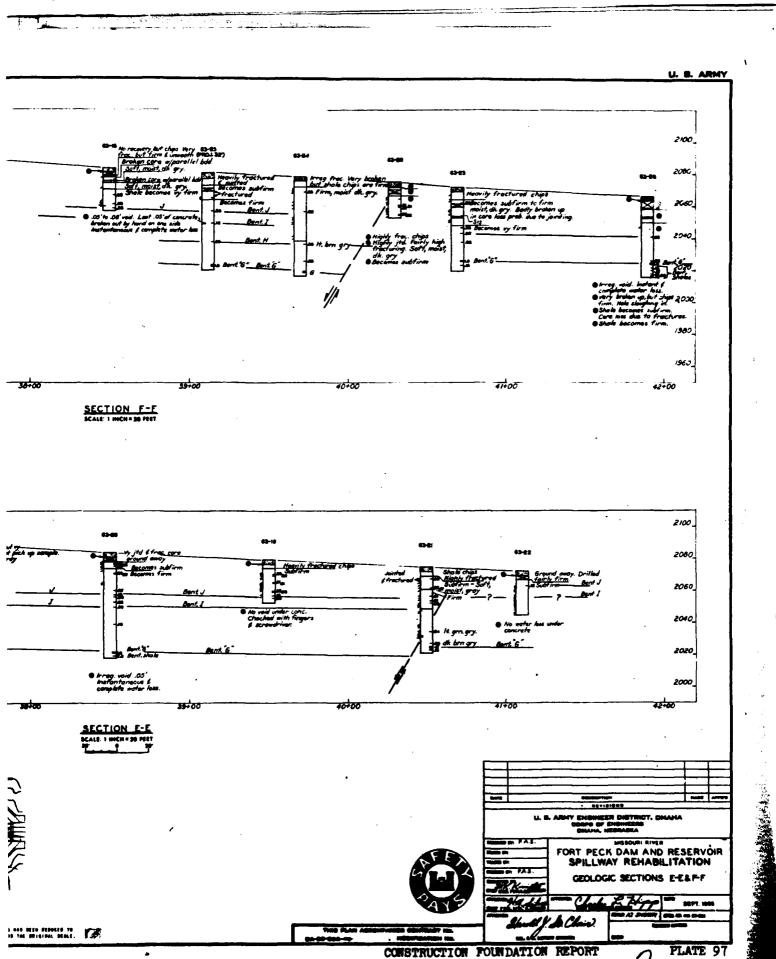


PLATE 97

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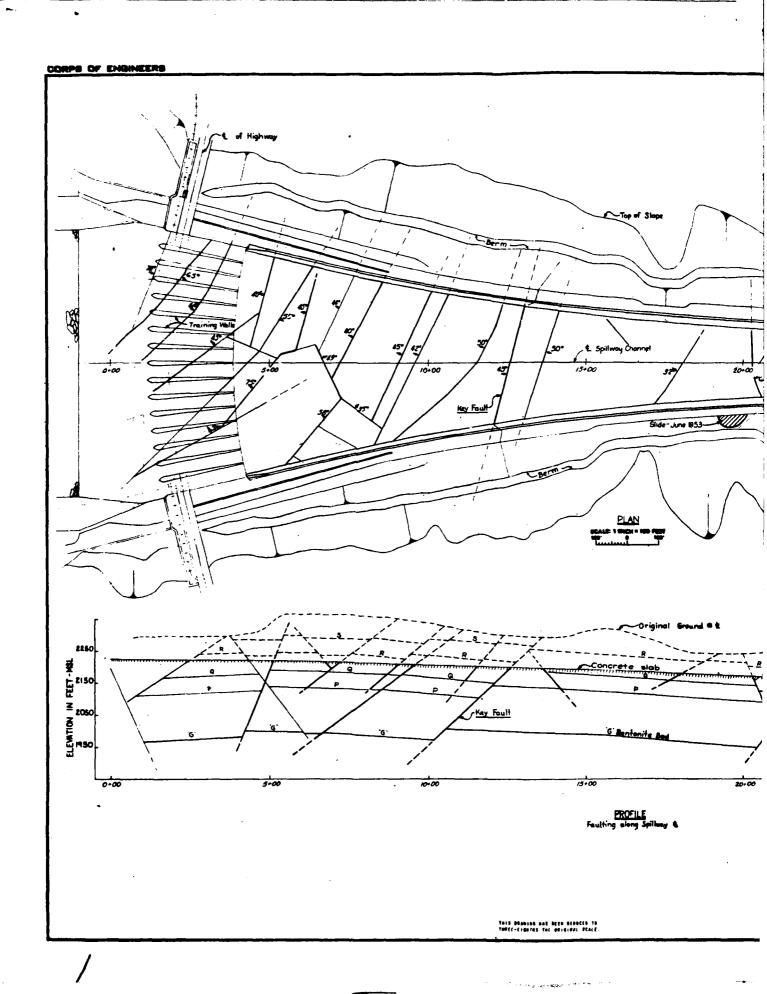
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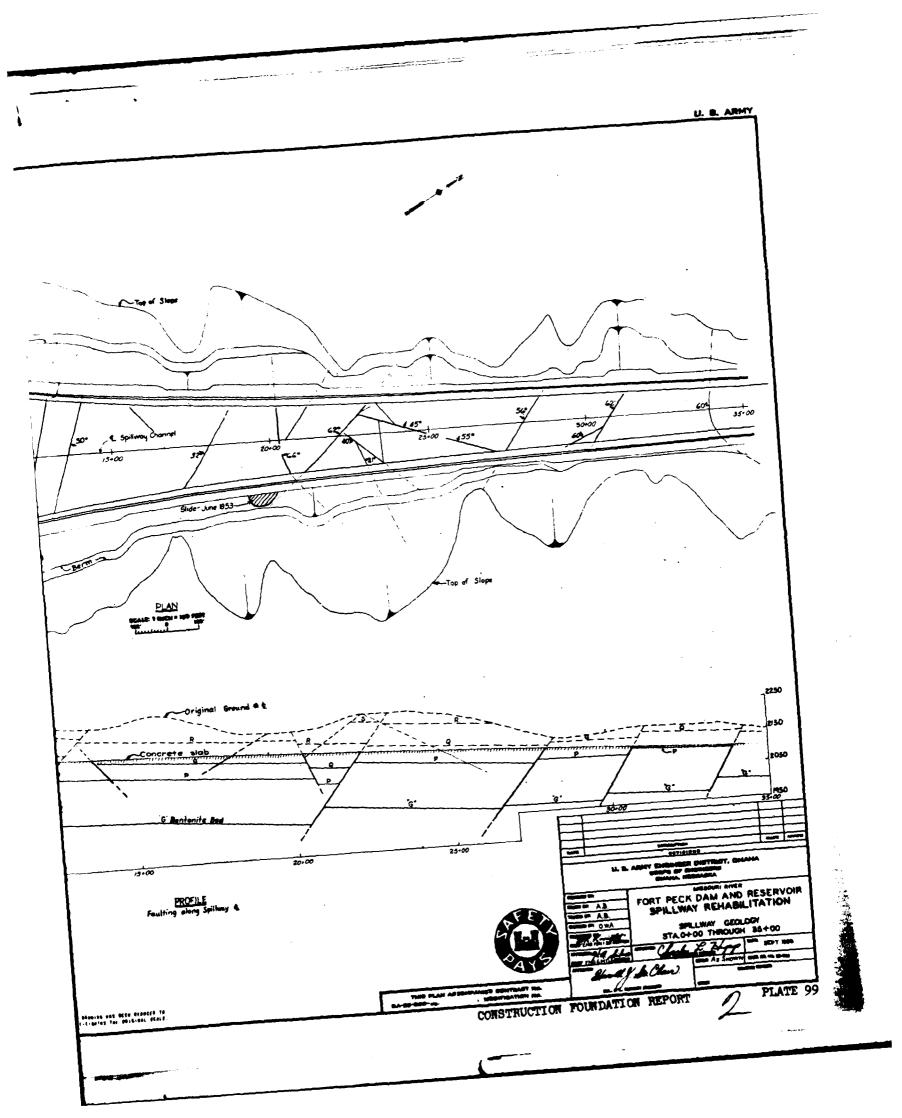
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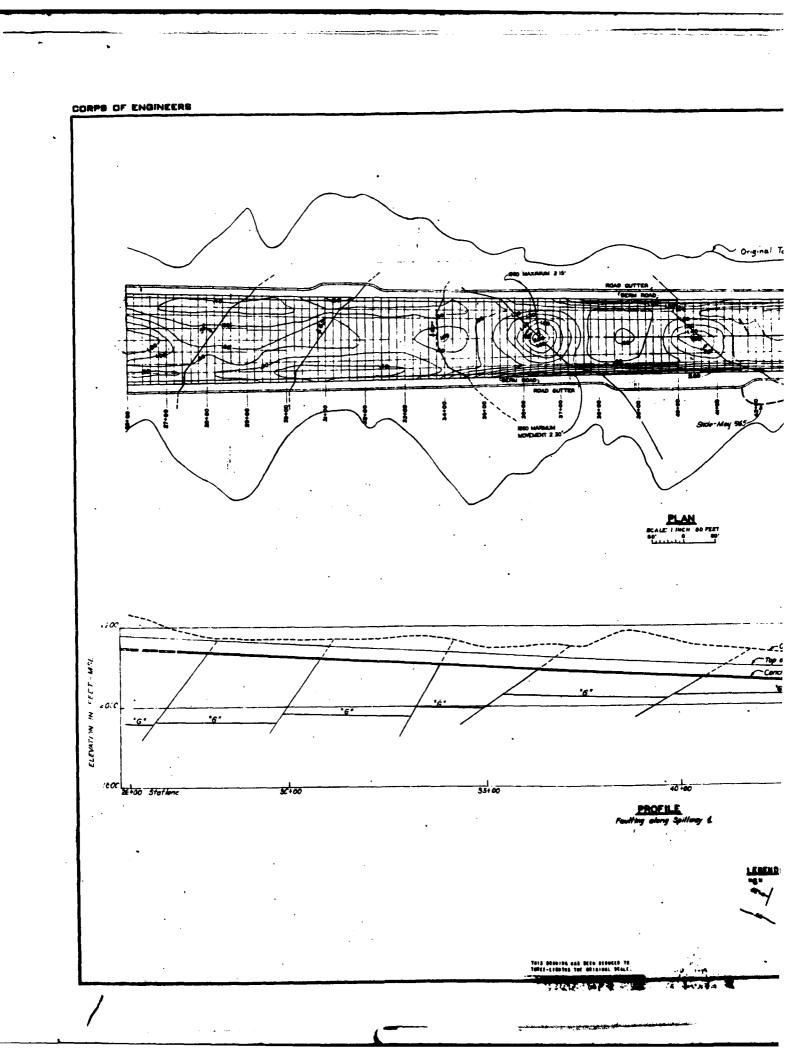
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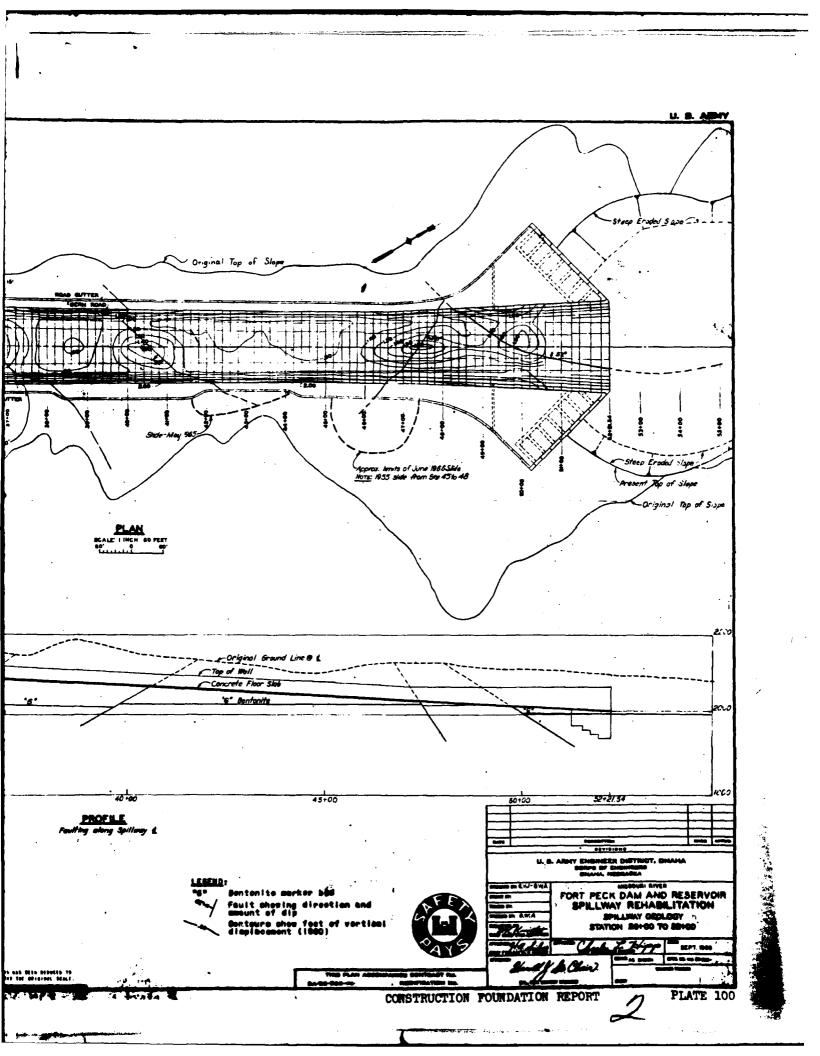
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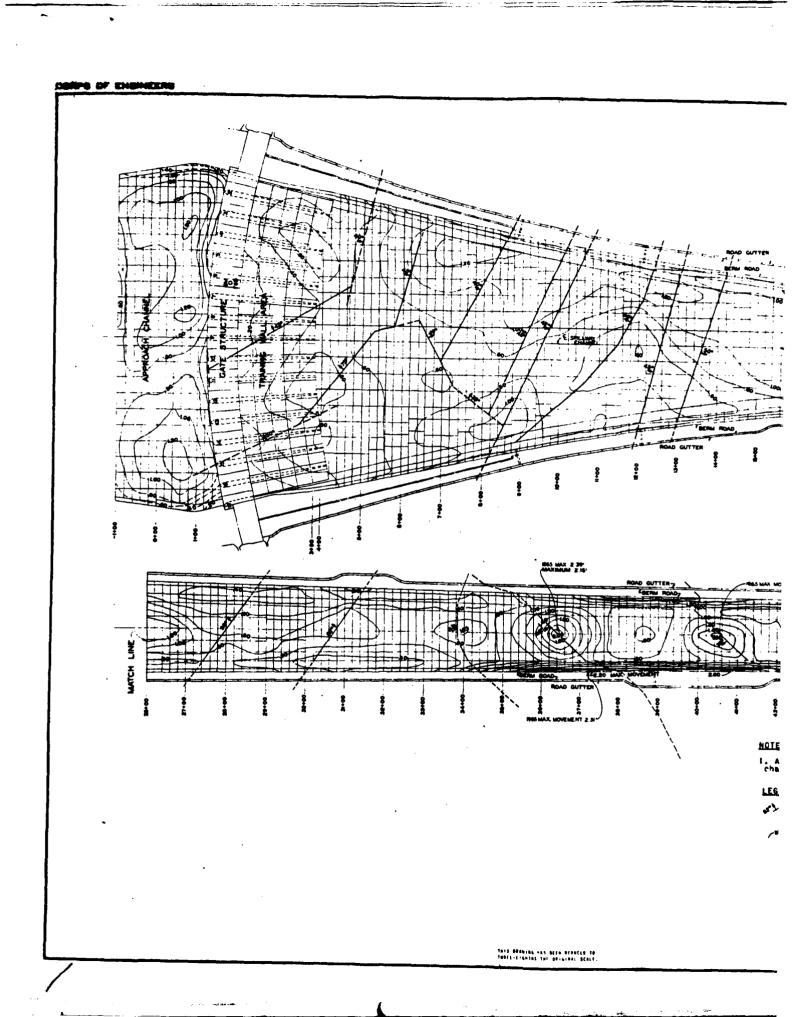
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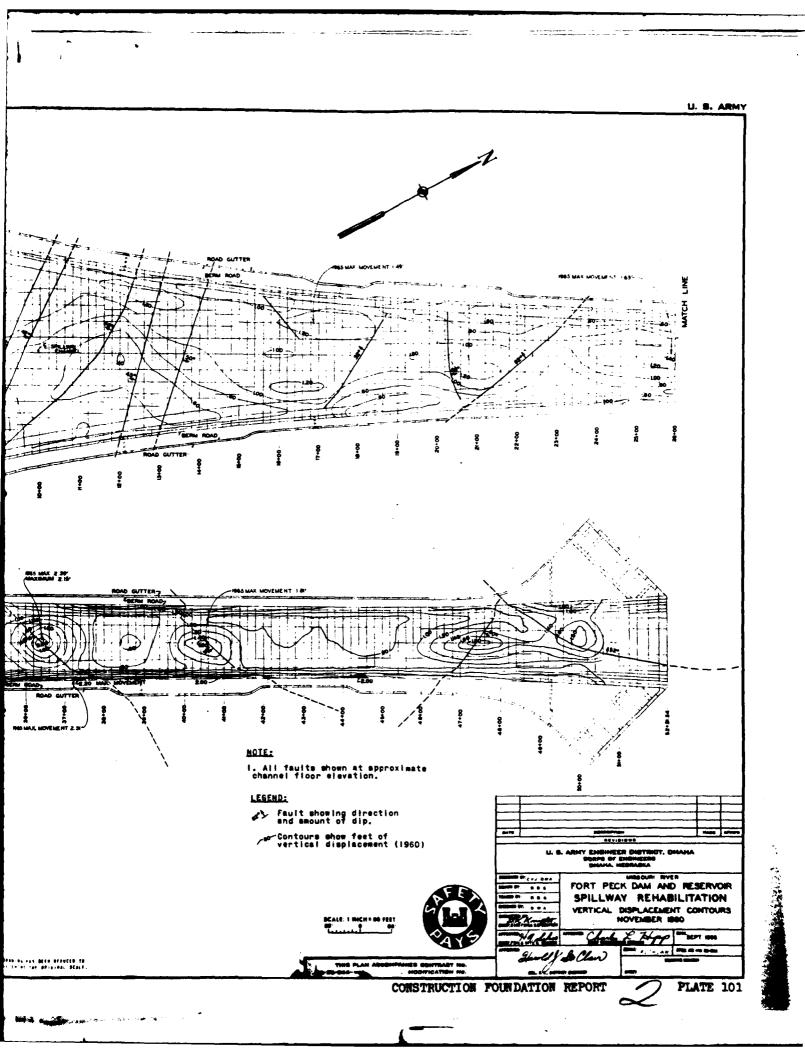


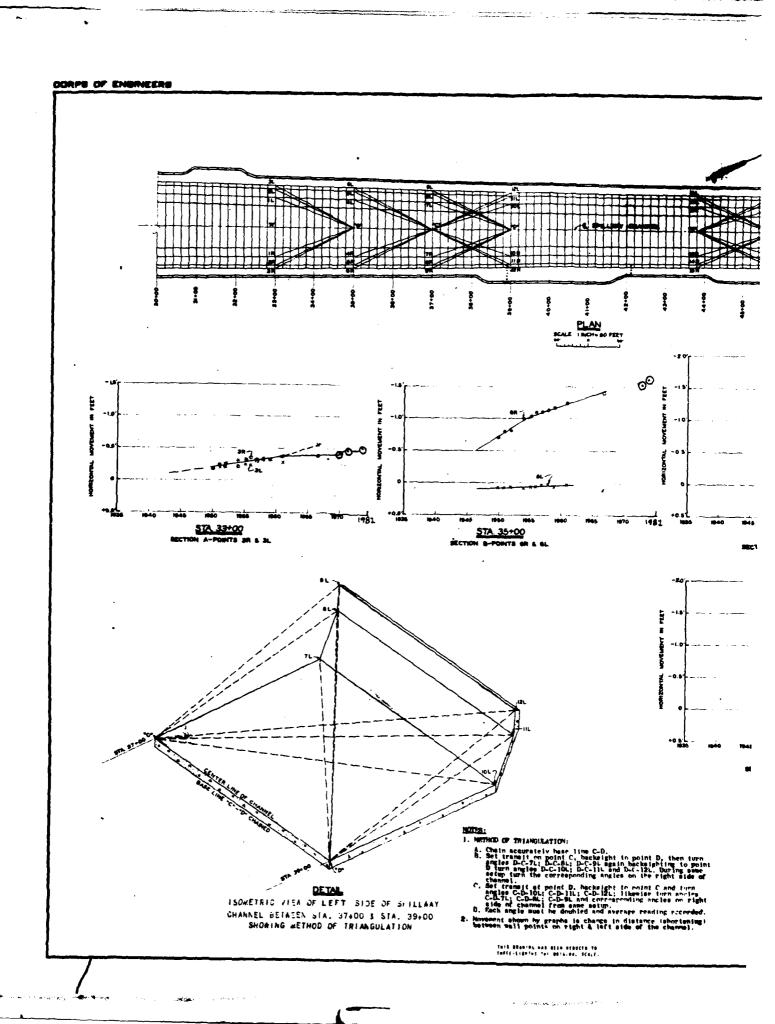


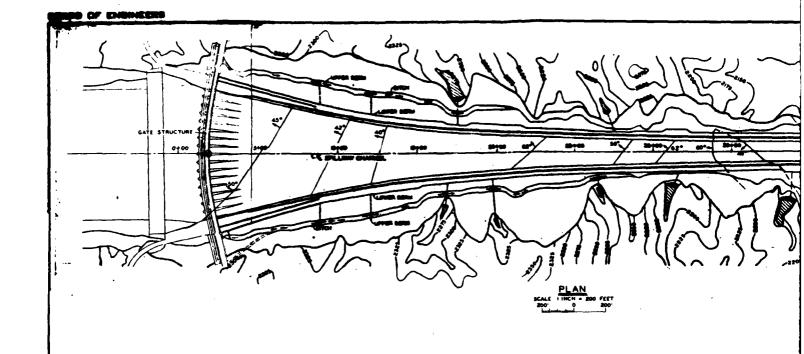


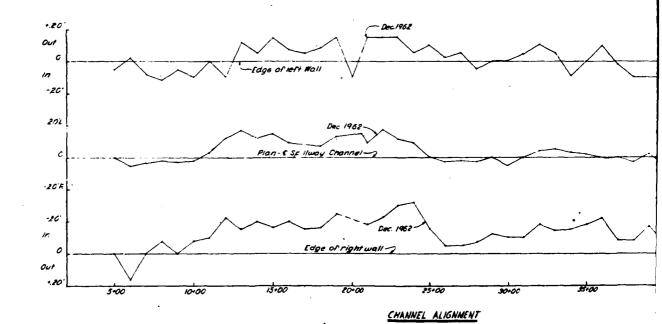






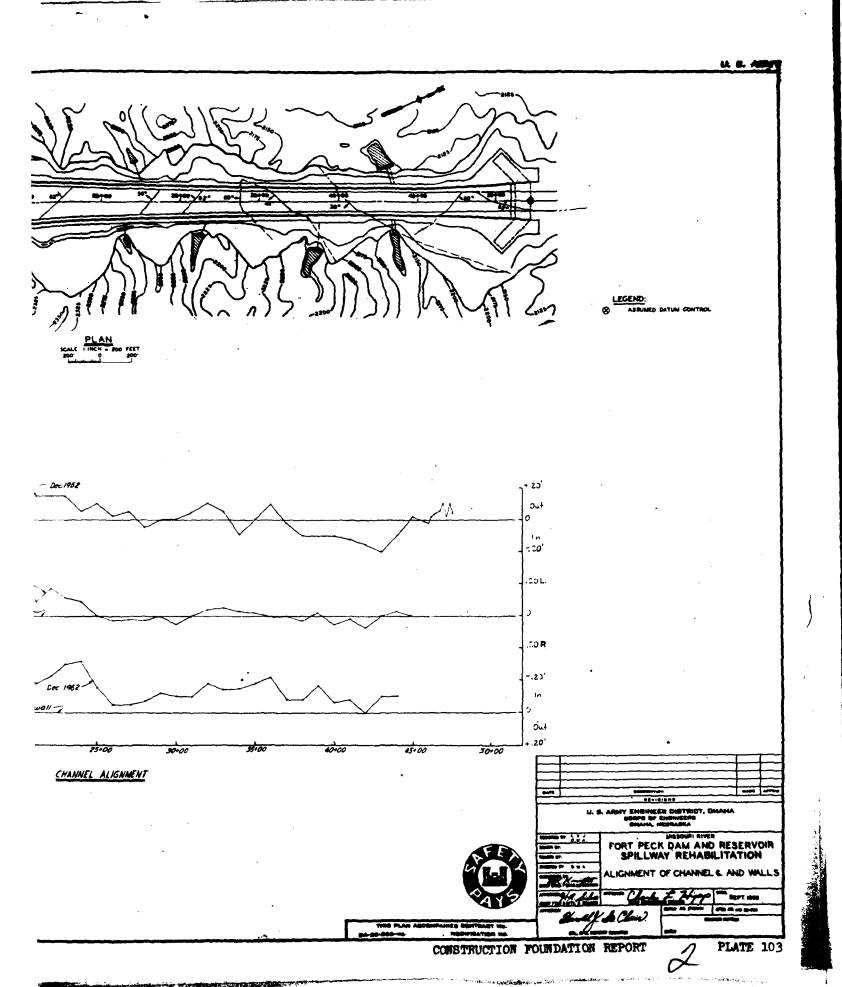


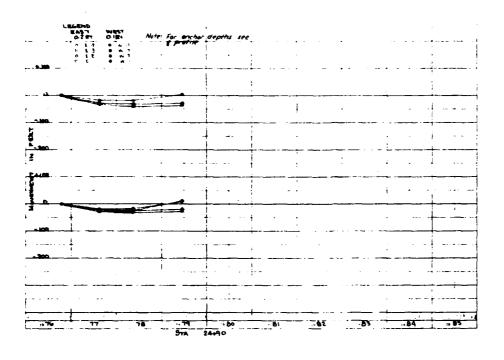


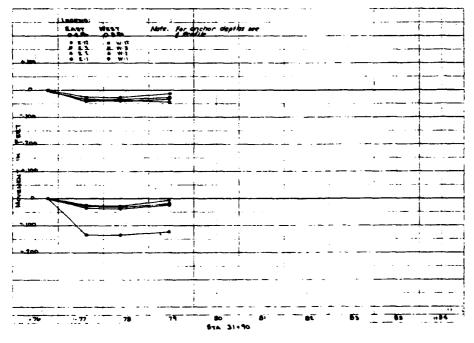


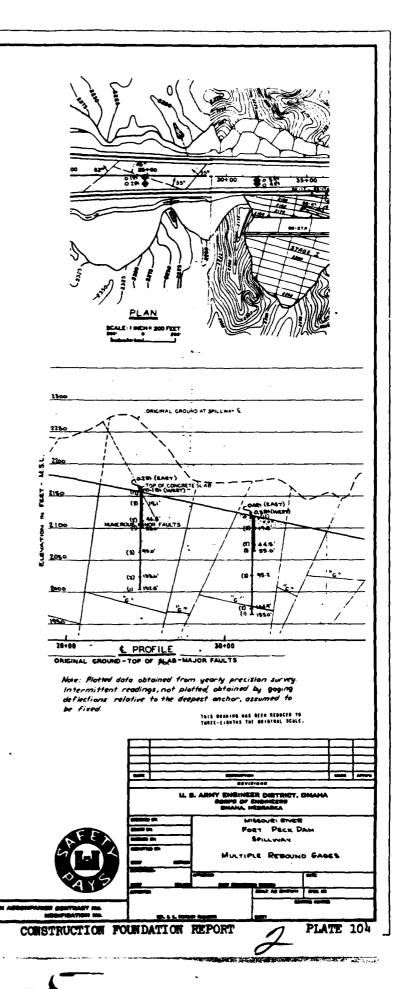
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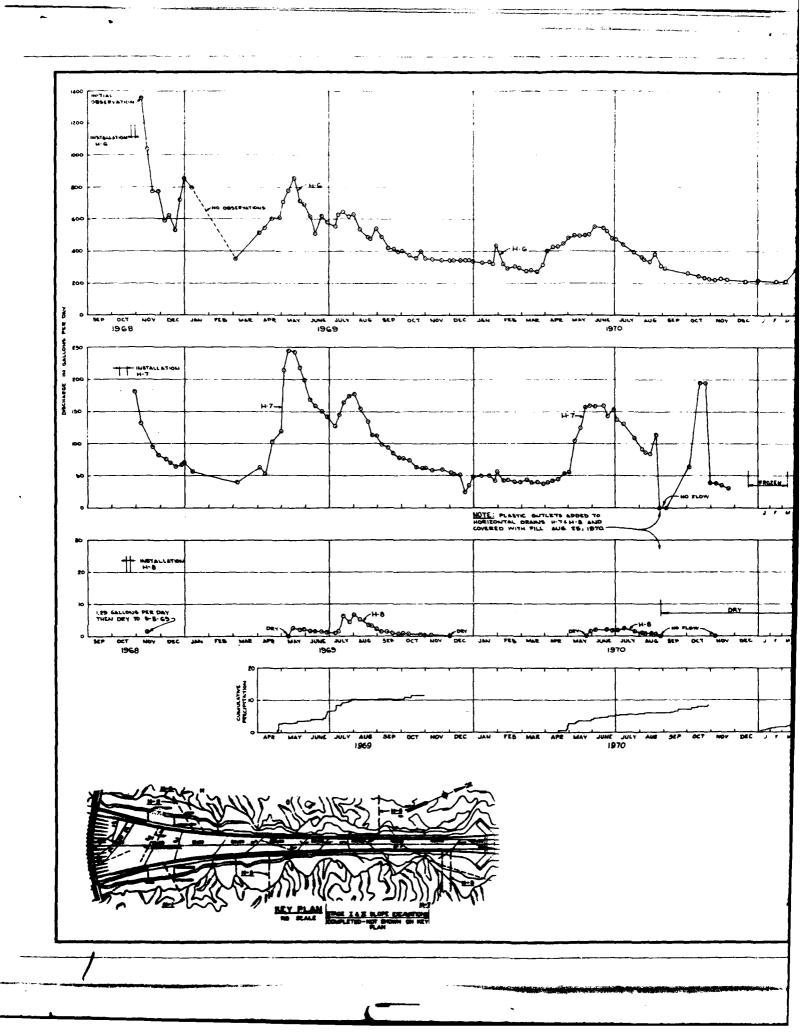
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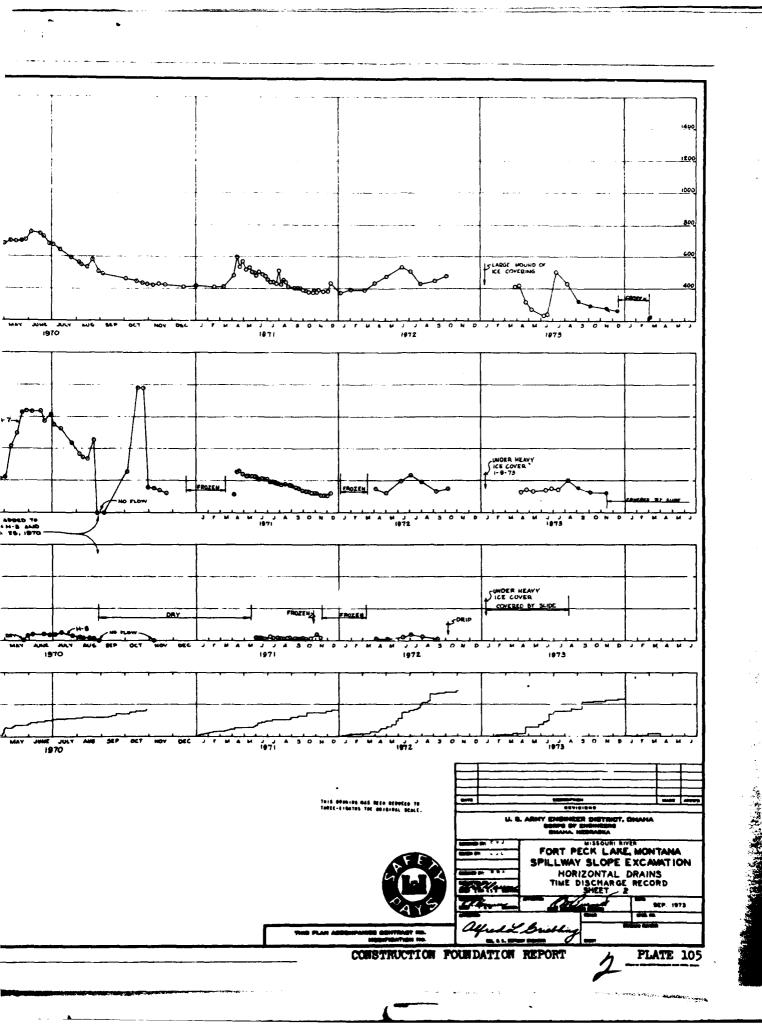


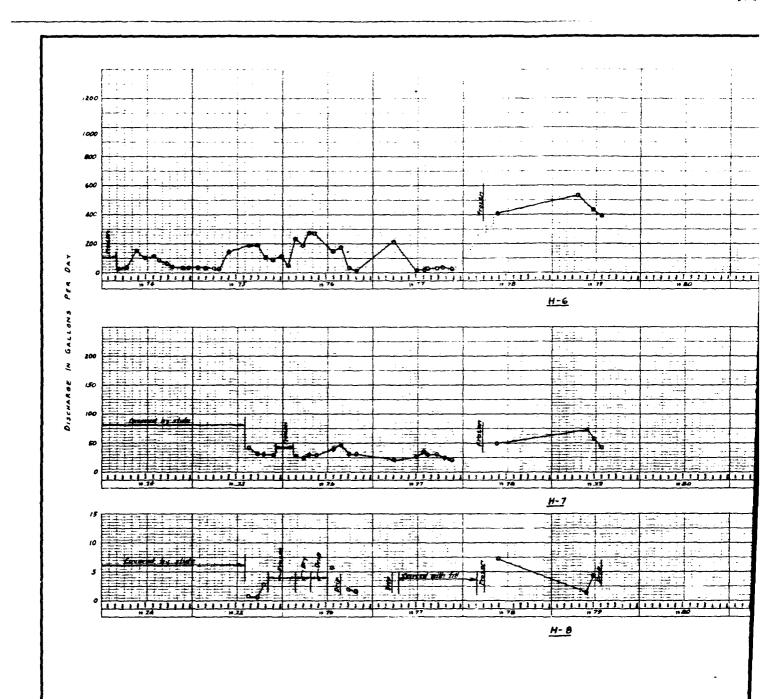


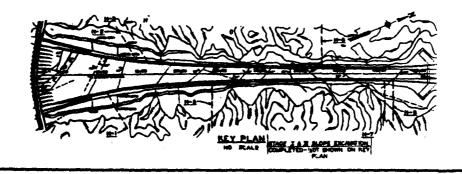












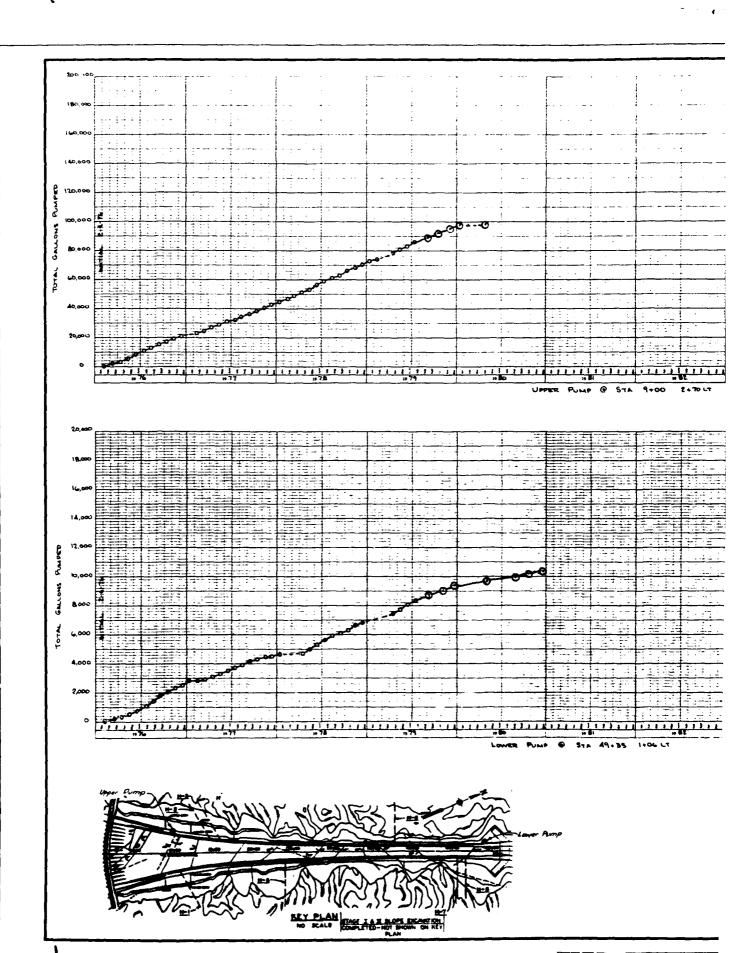
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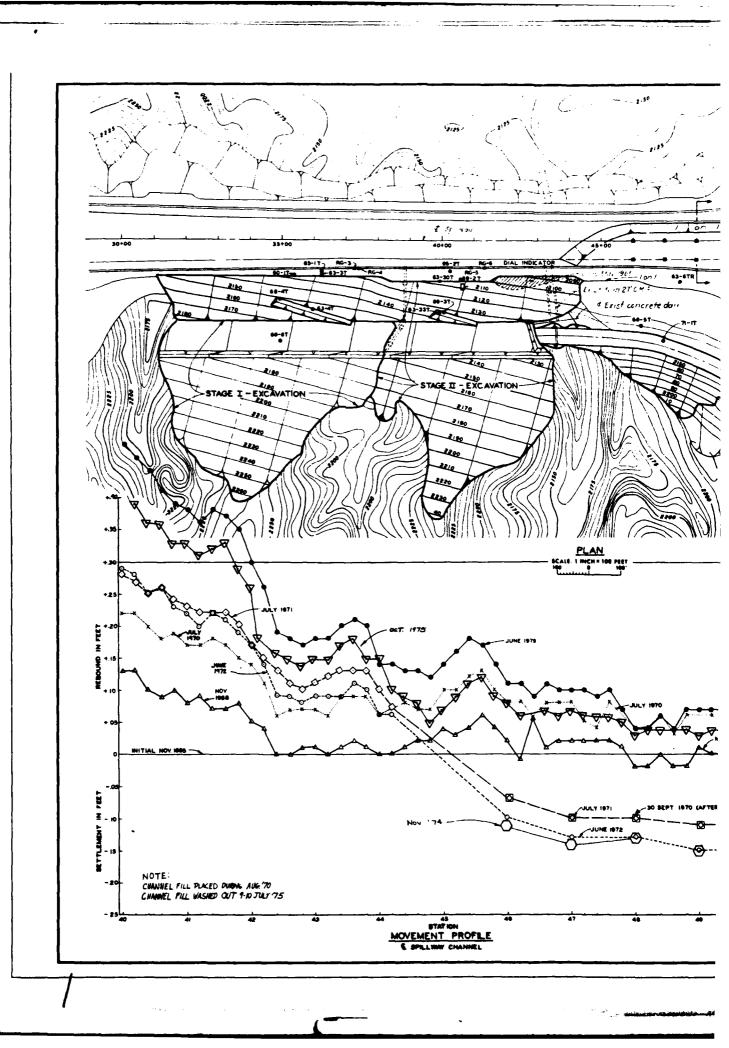
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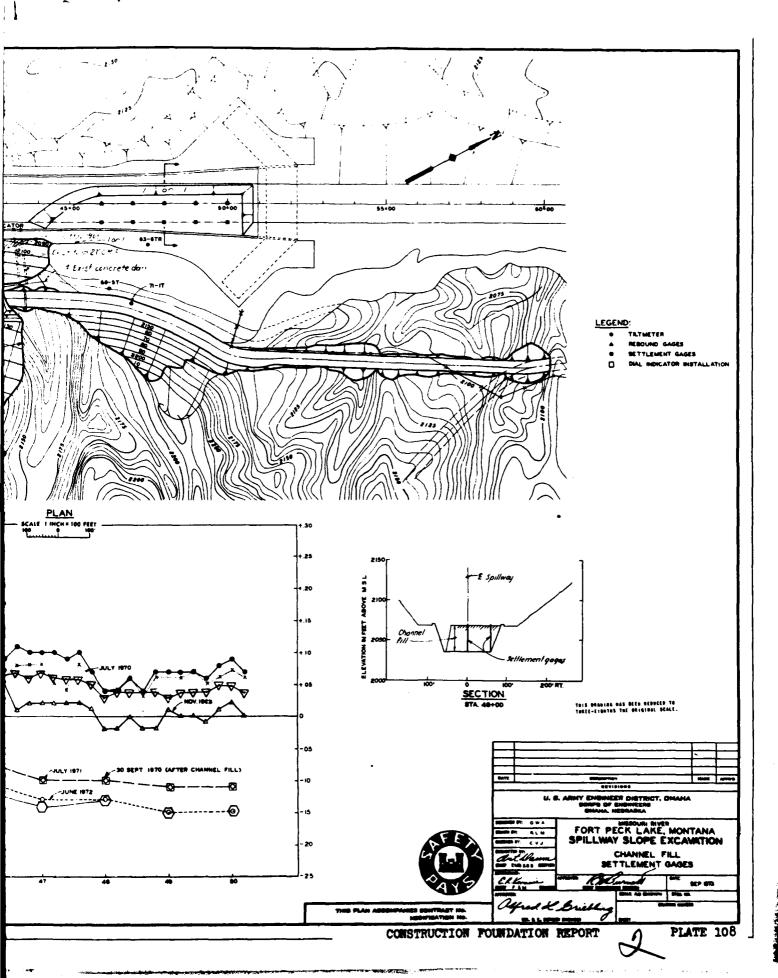
CONSTRUCTION FOUNDATION REPORT

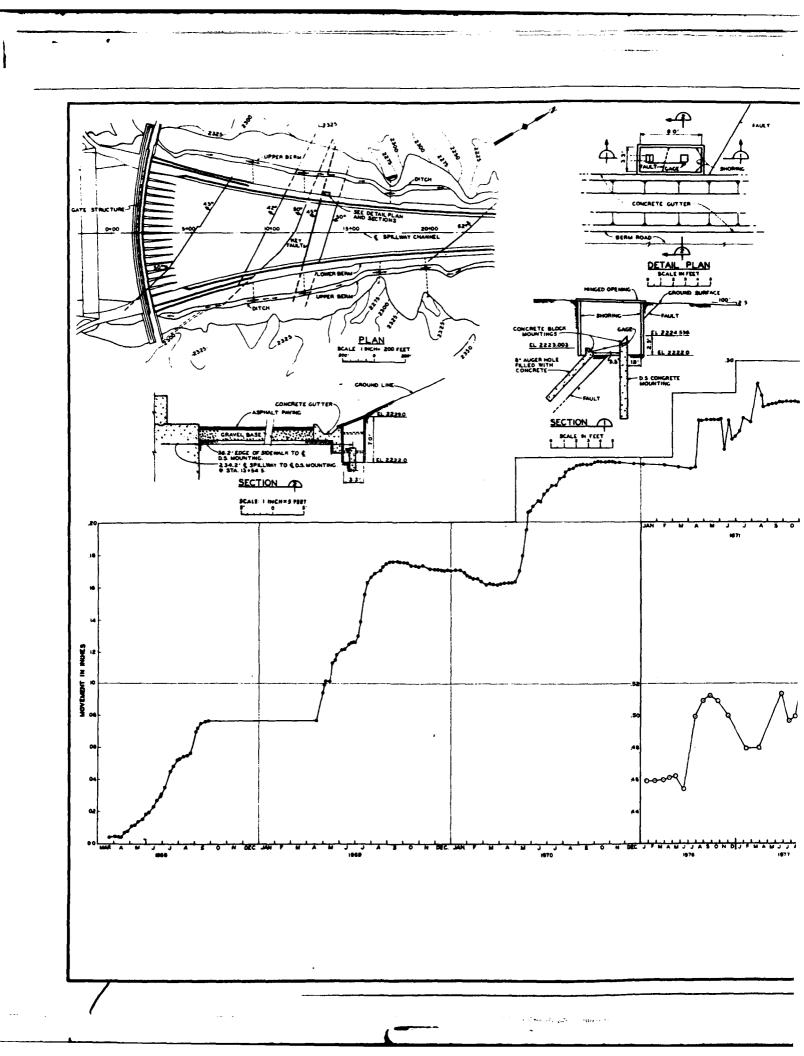
PLATE 106

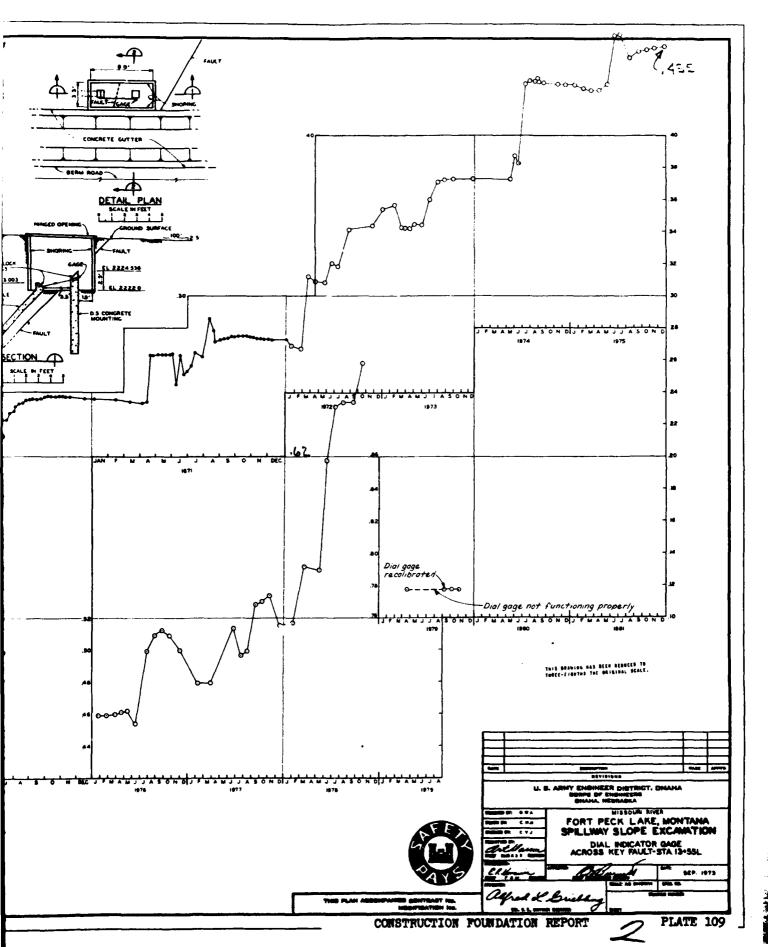


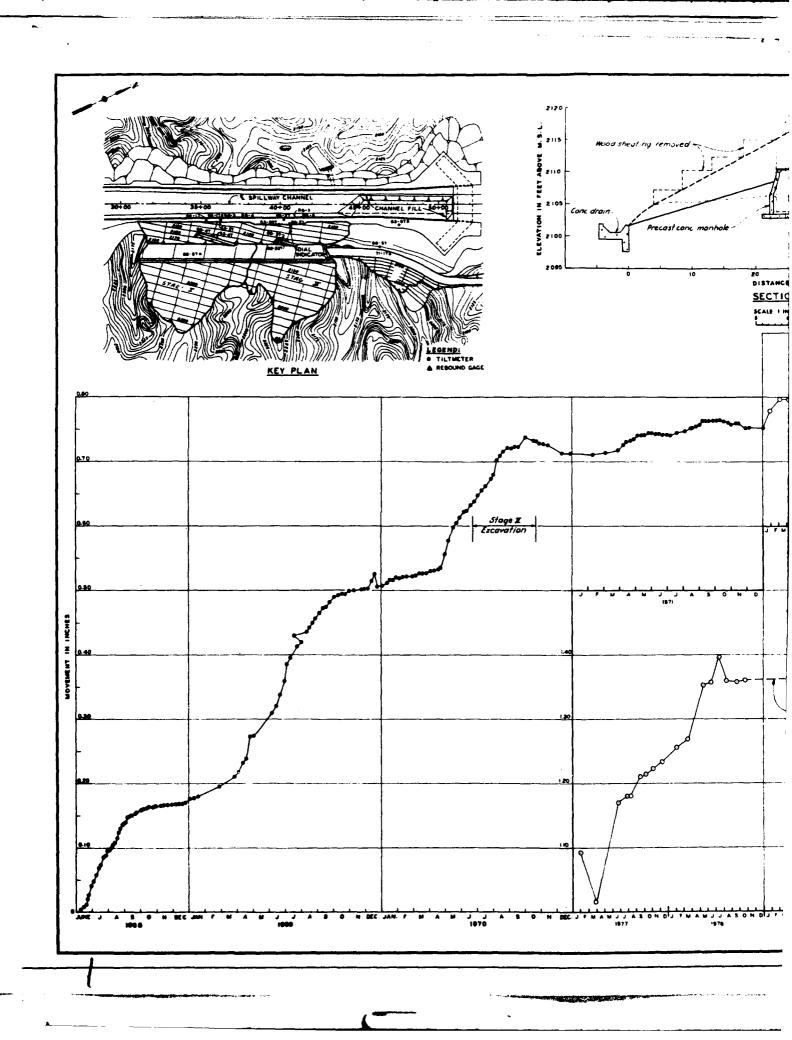
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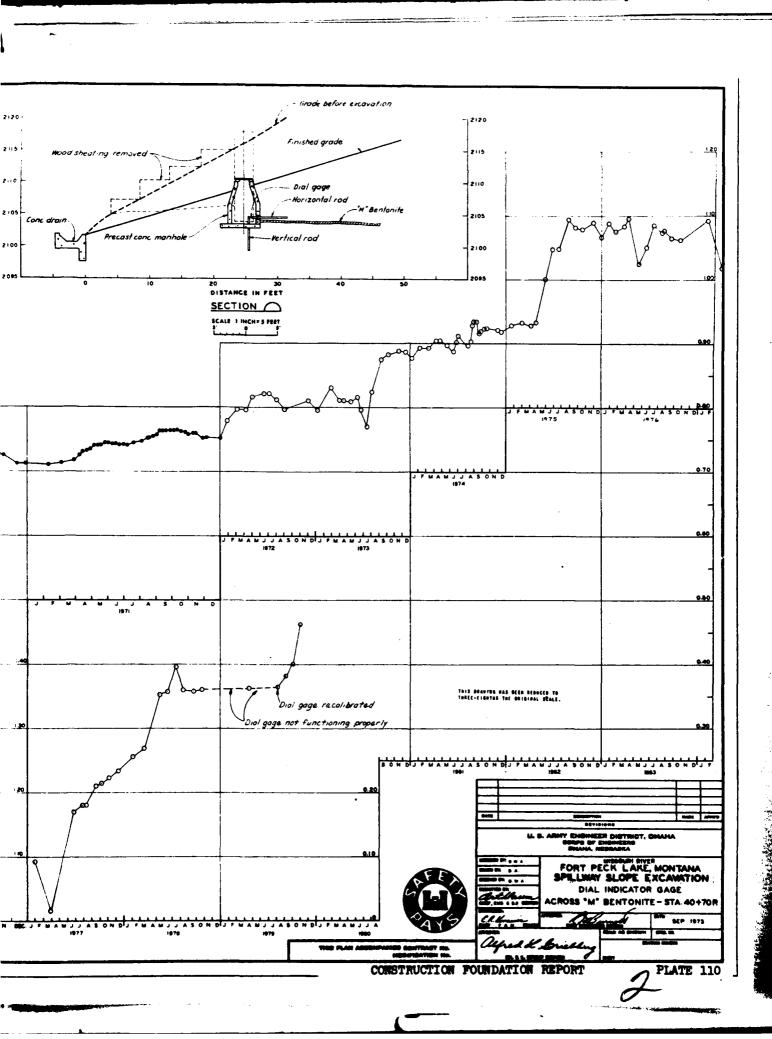


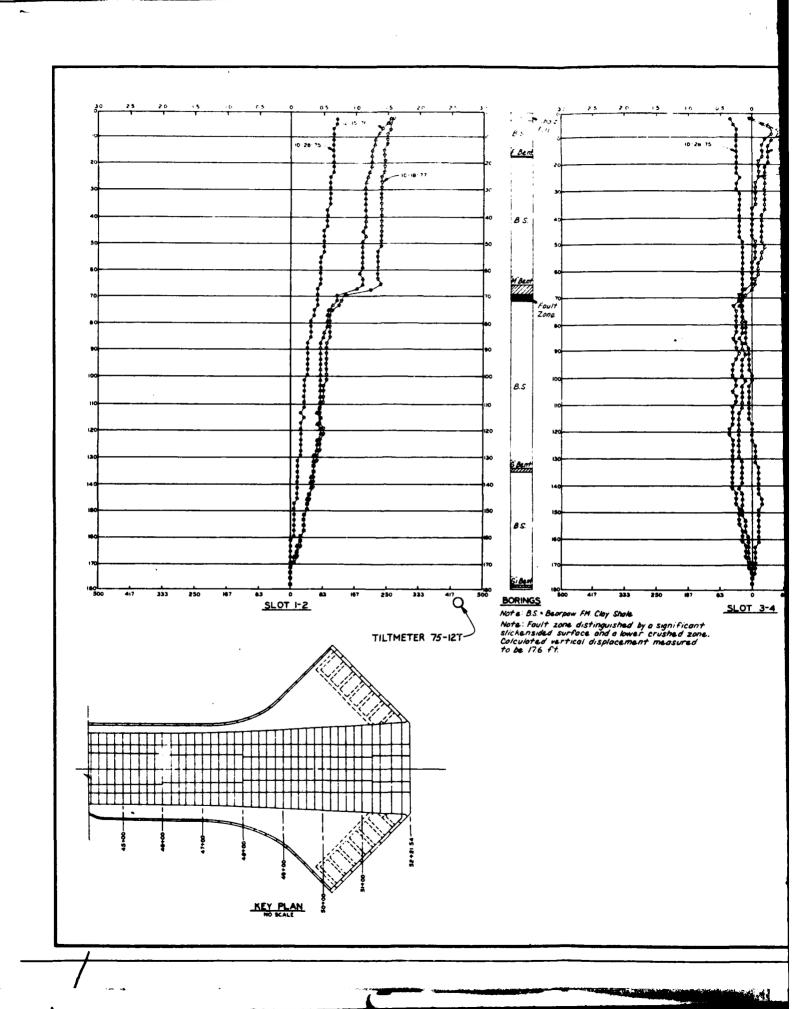


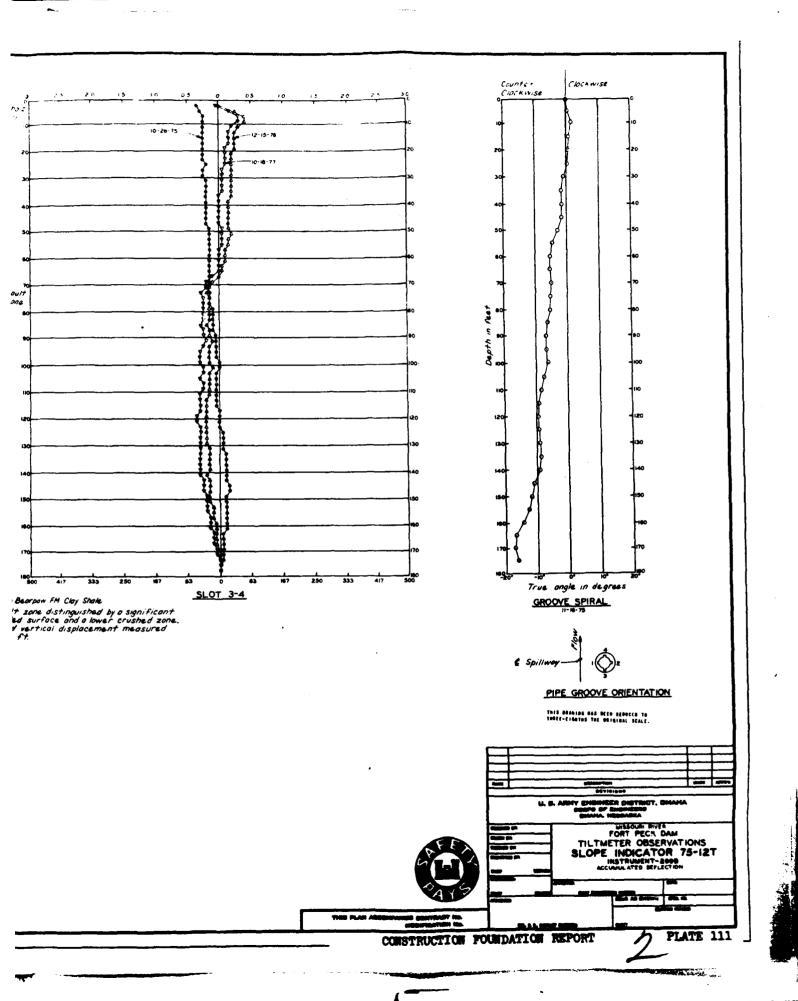


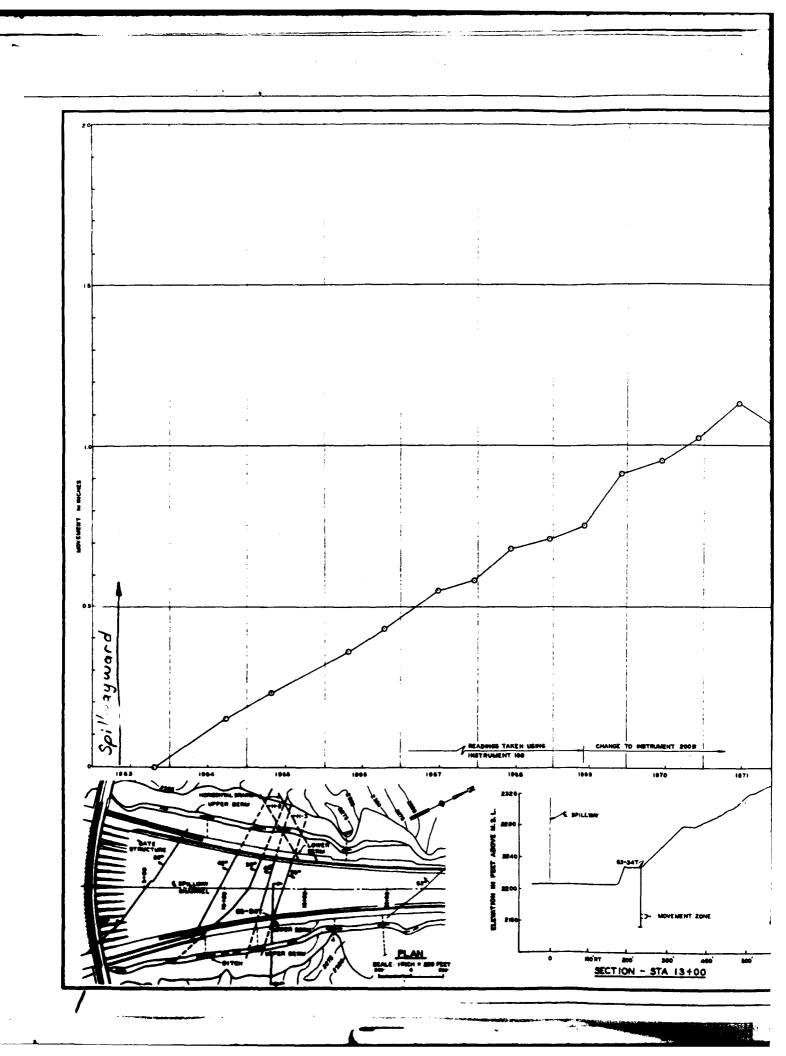


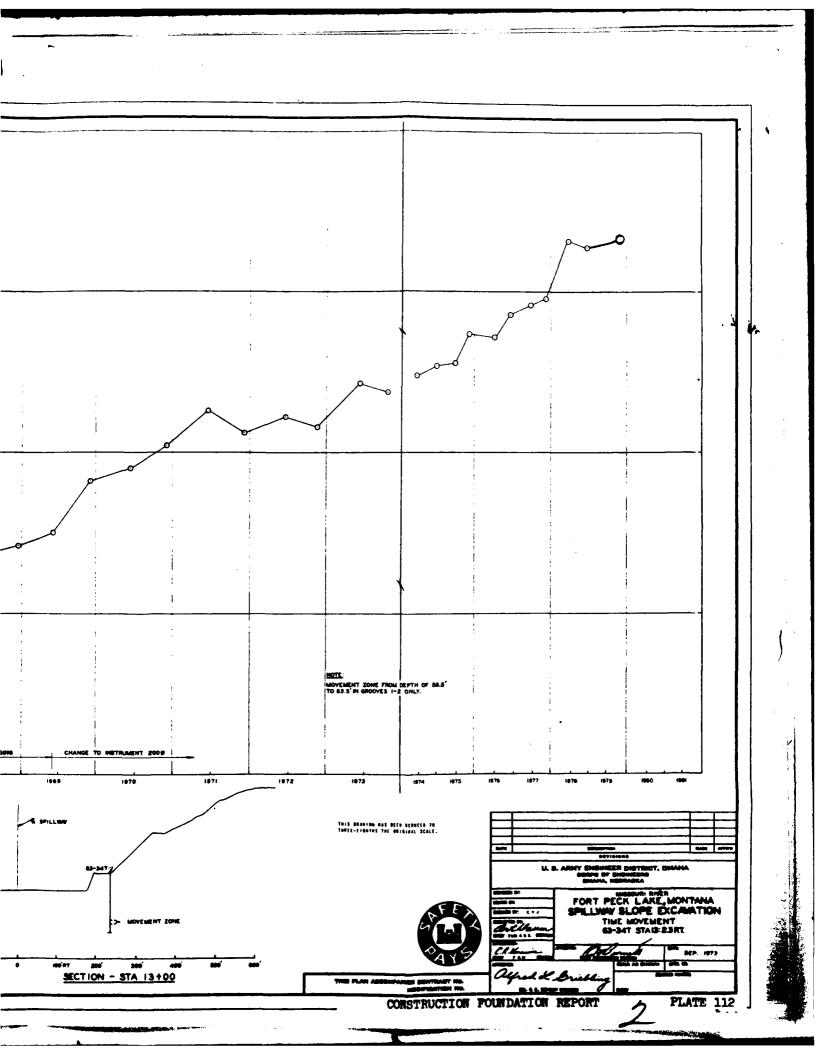


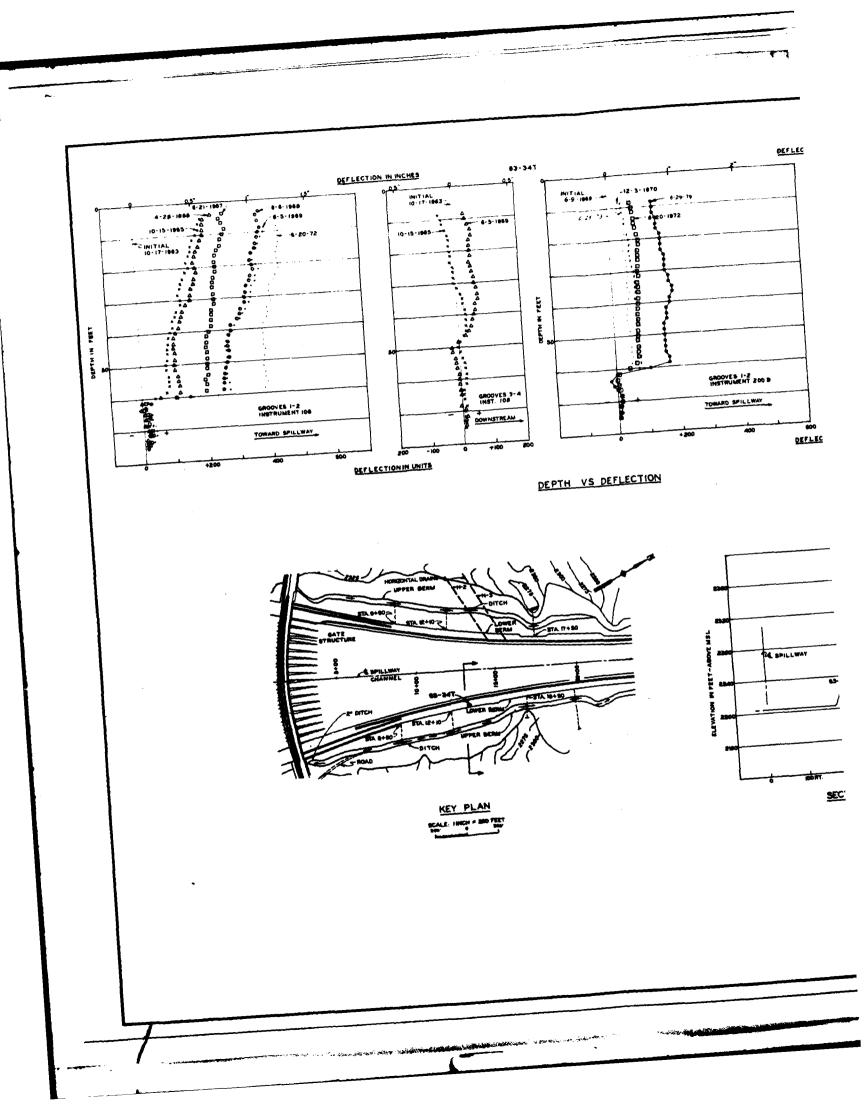


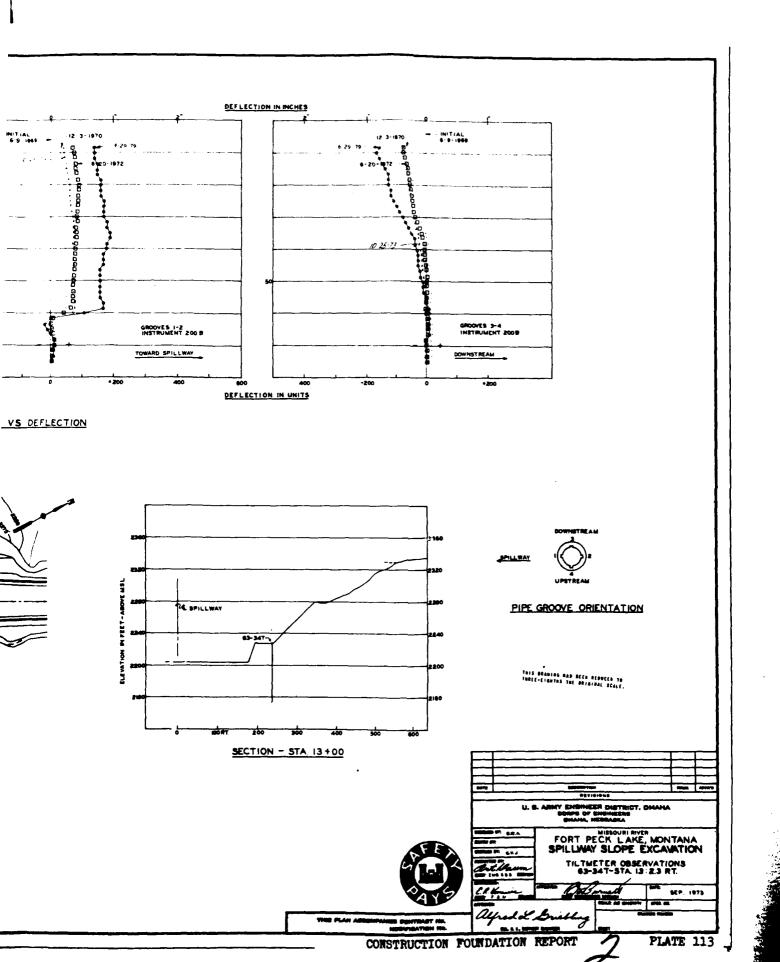




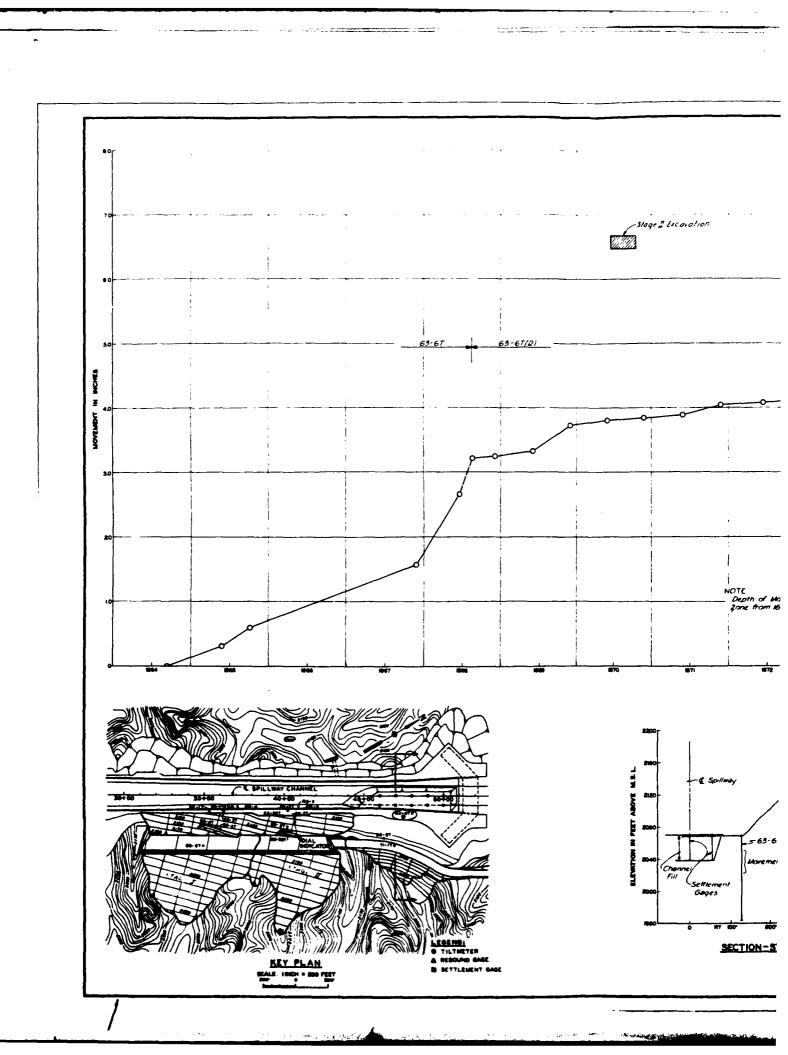


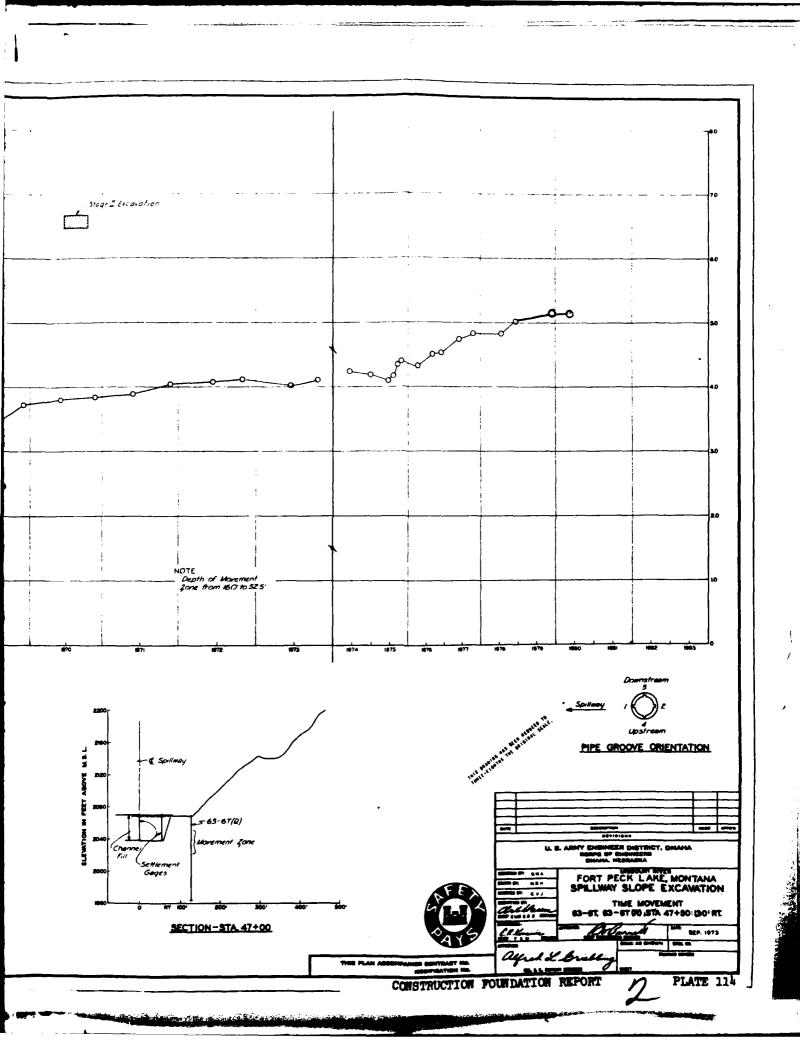


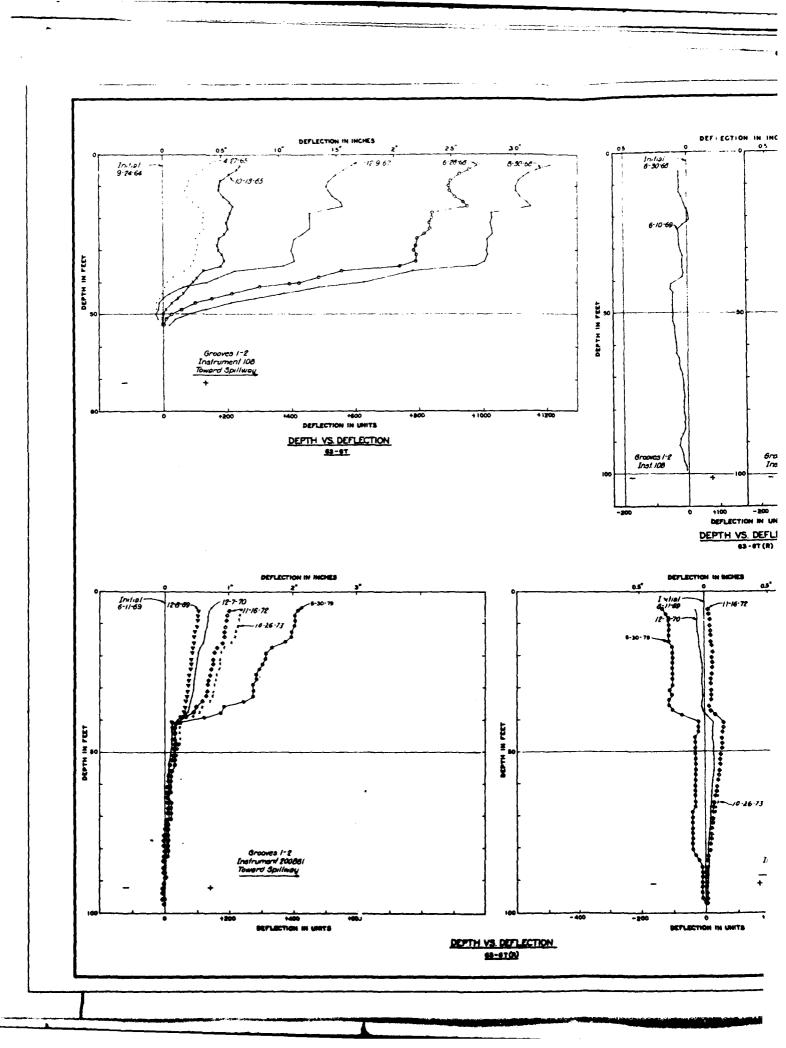


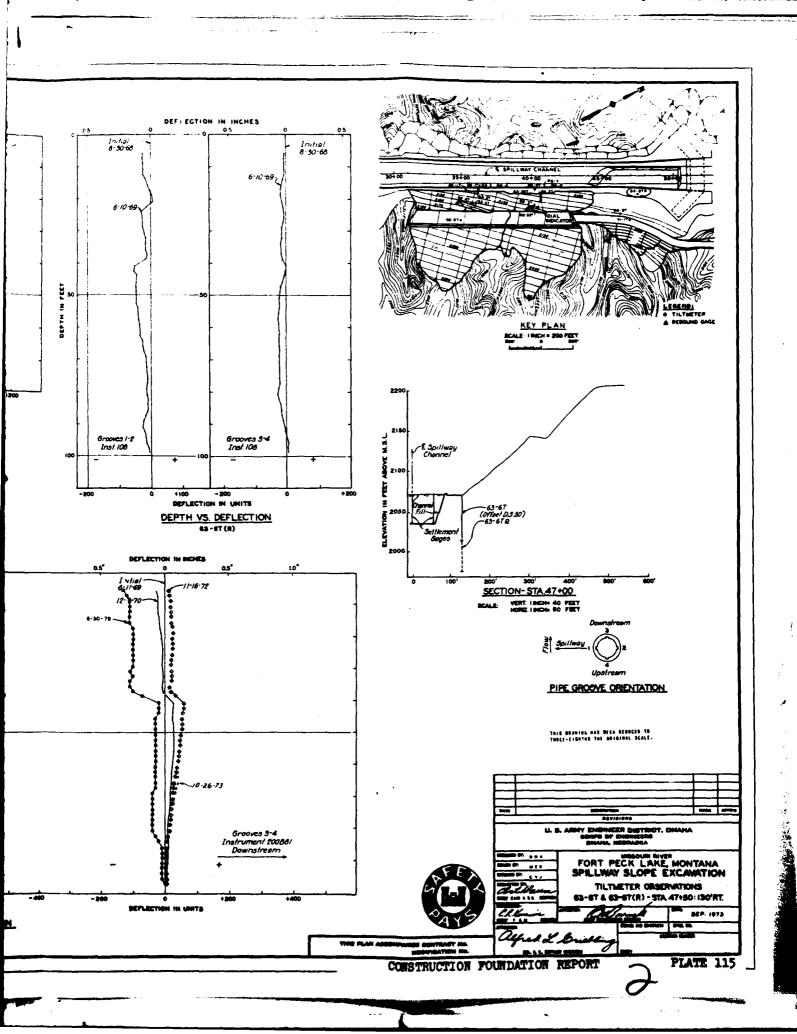


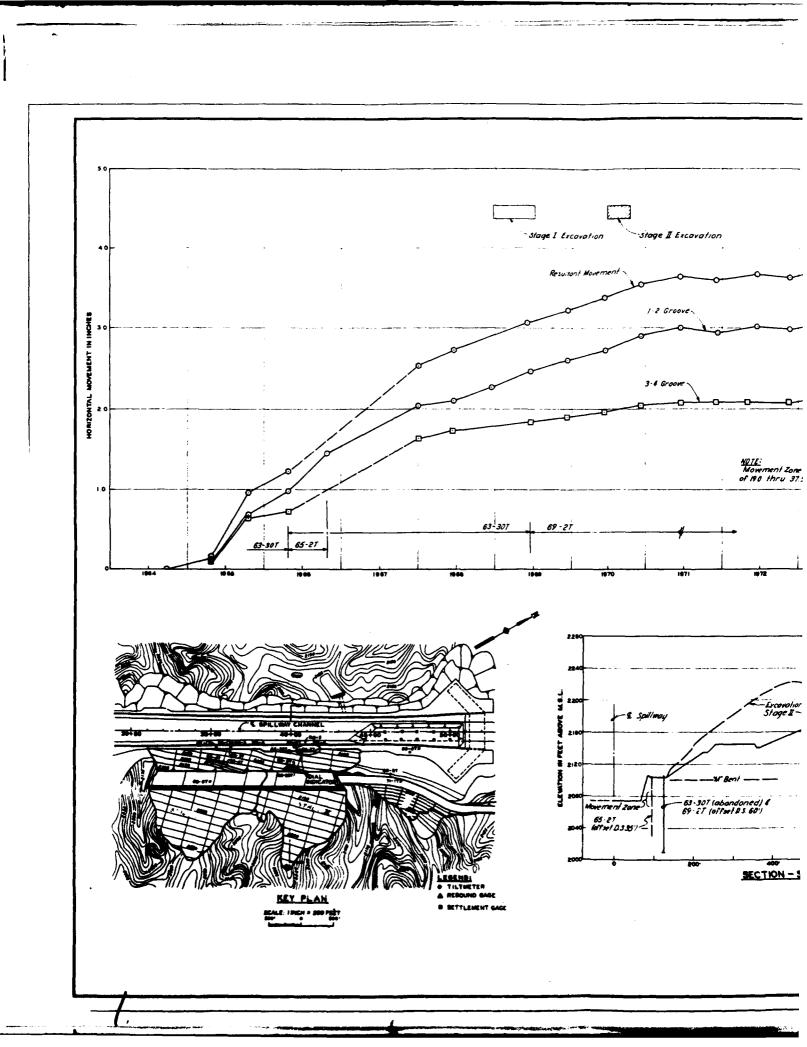
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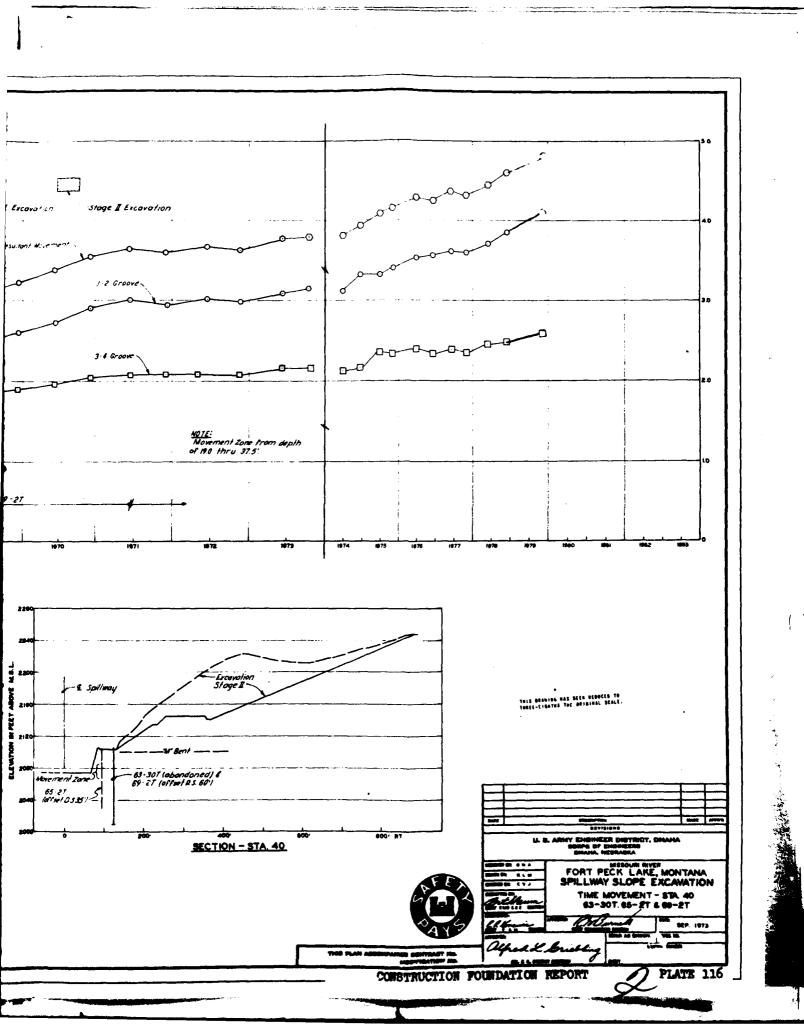


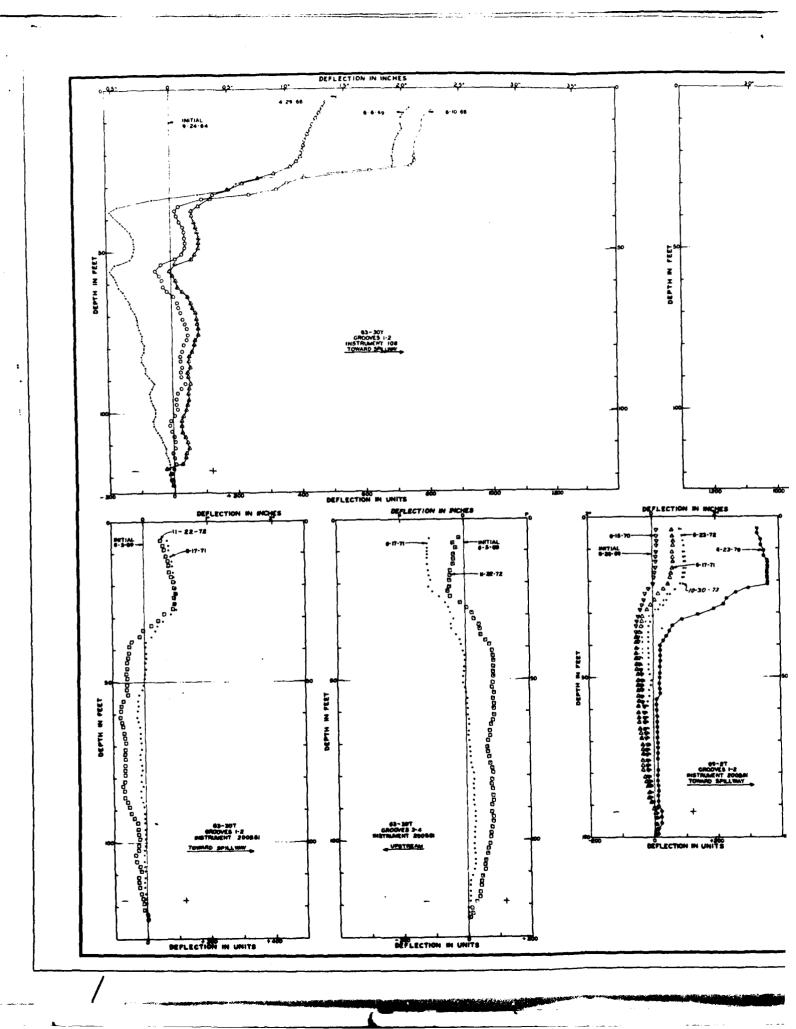


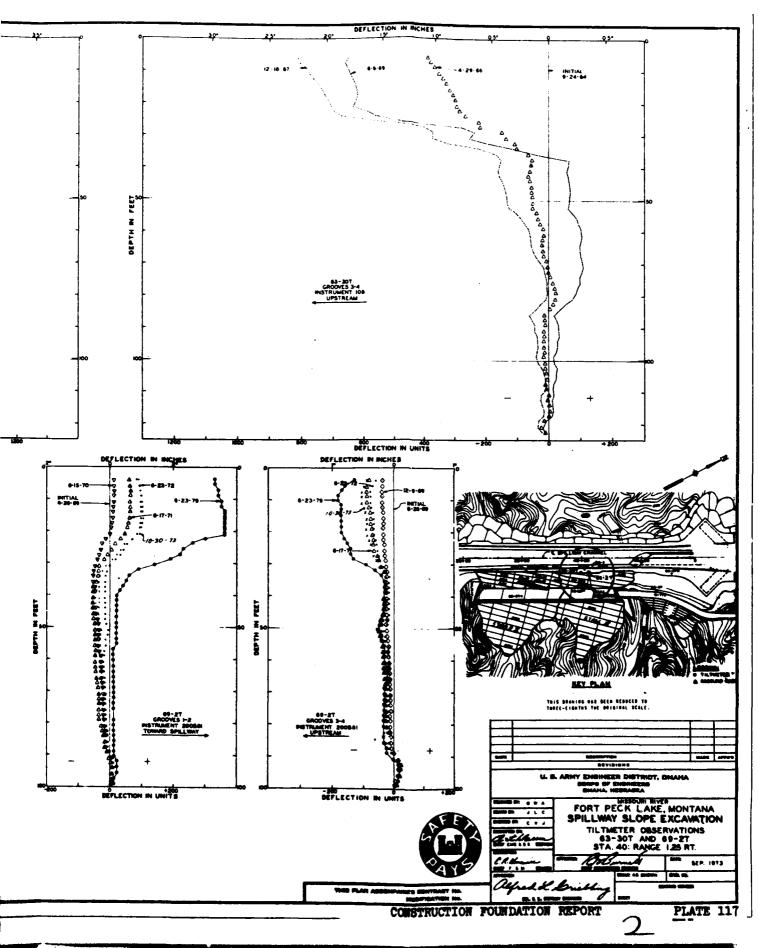




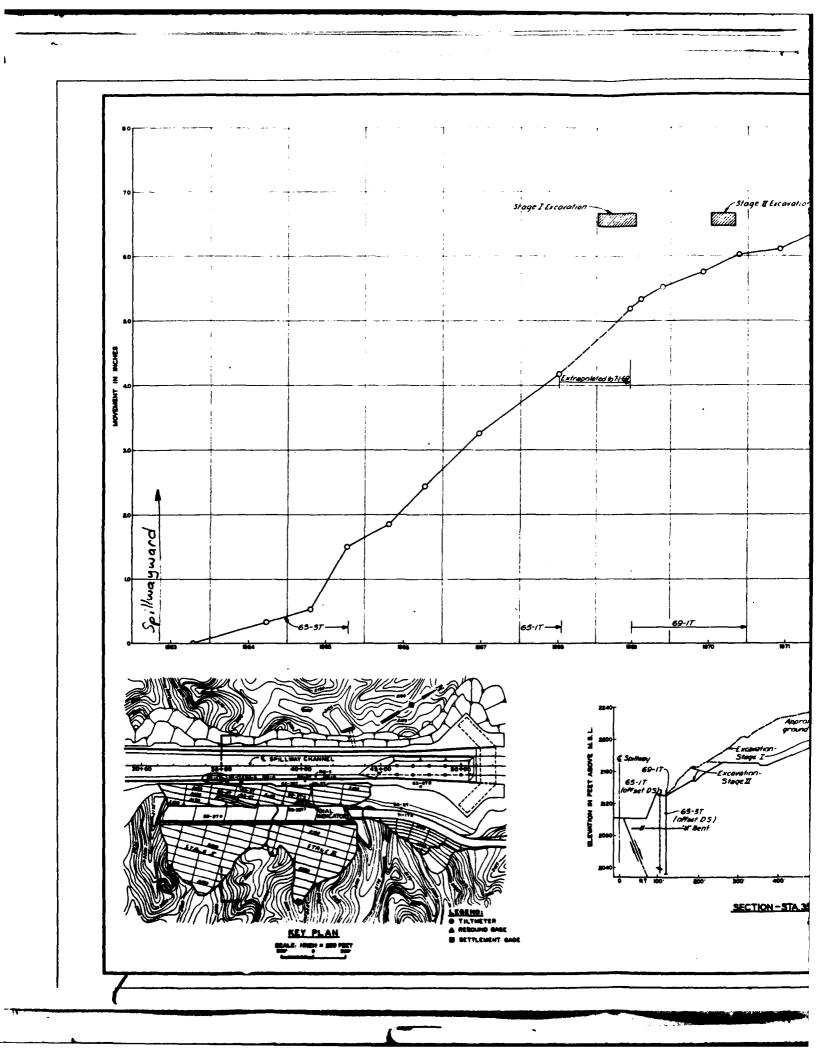


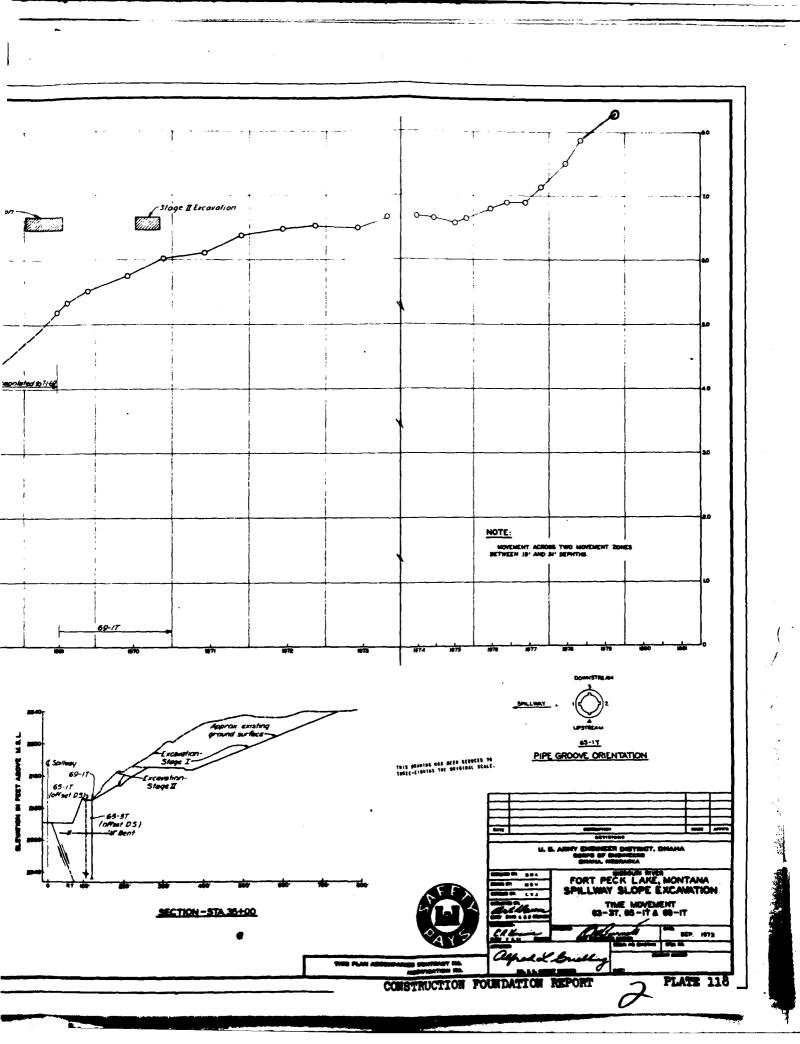


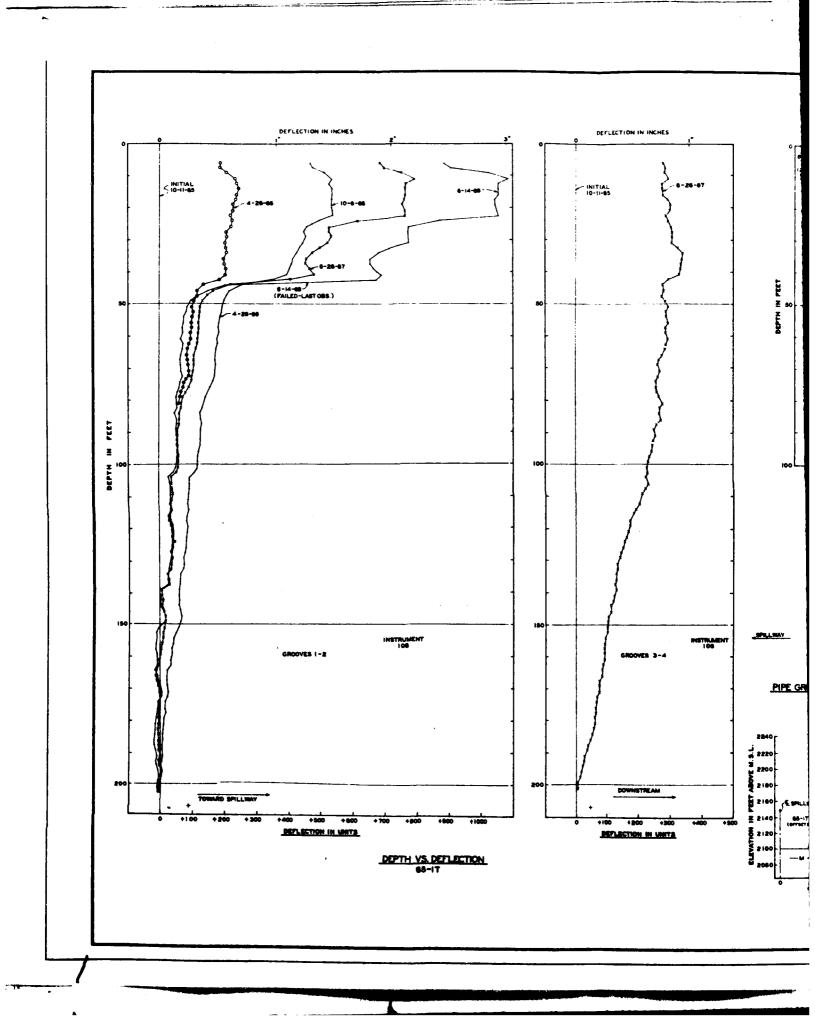


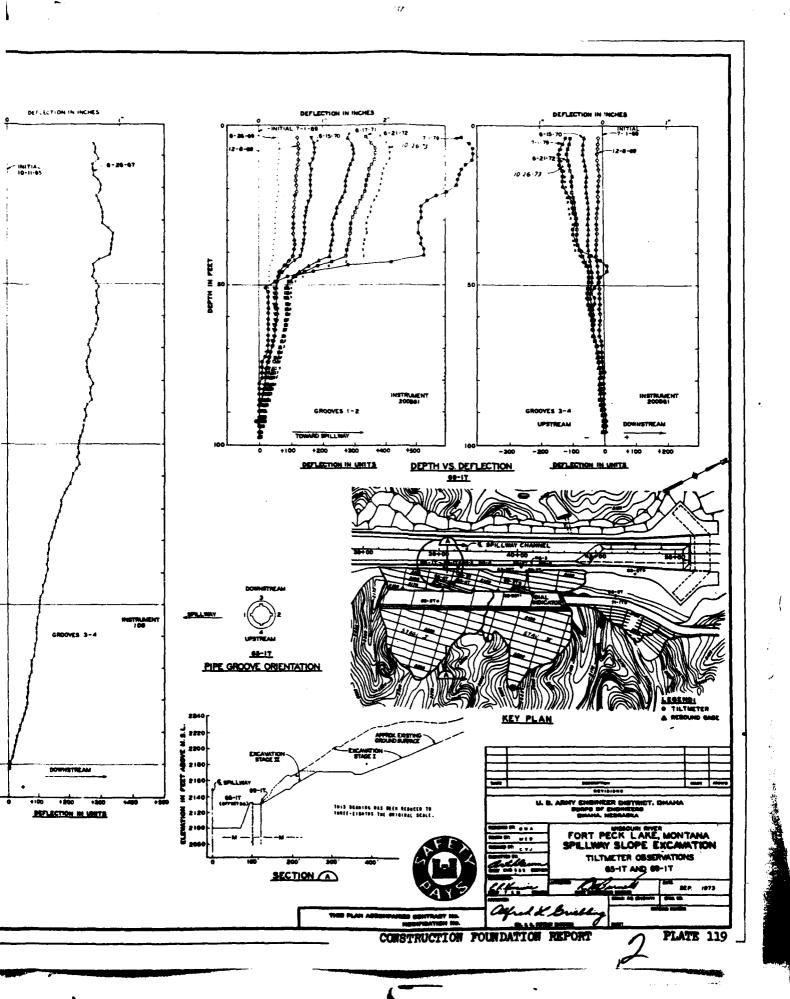


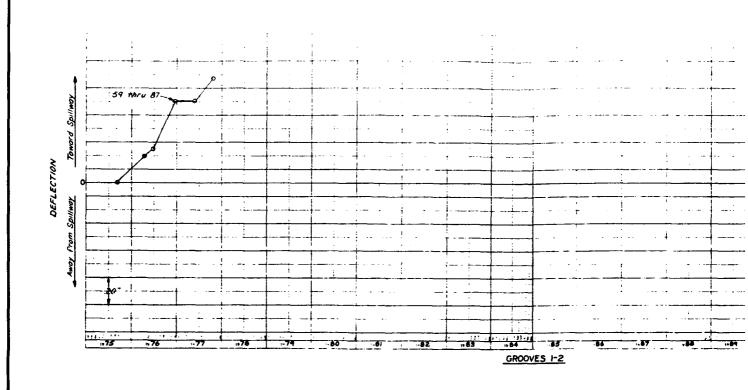
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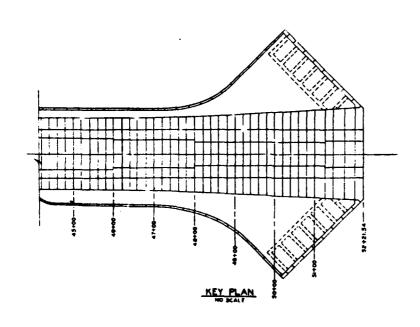








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PIPE GROOVE ORIENTATION

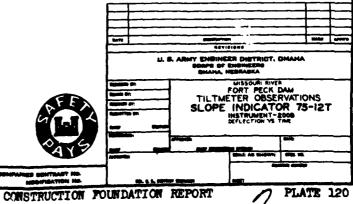
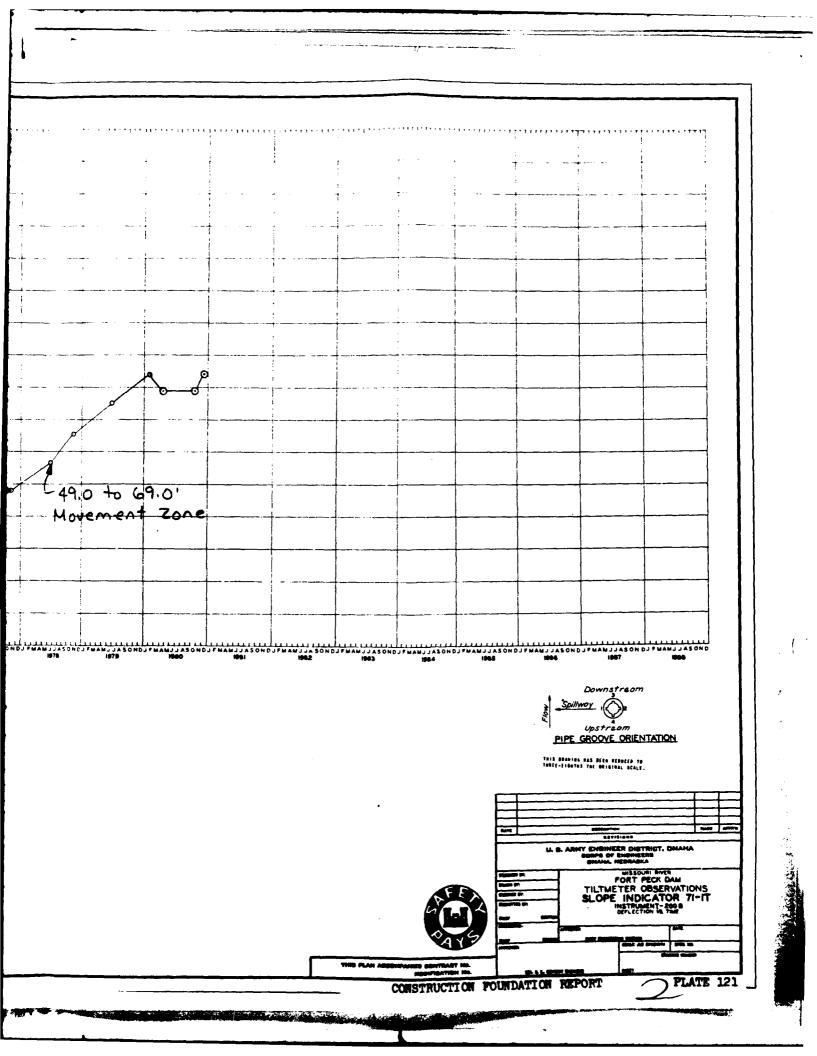
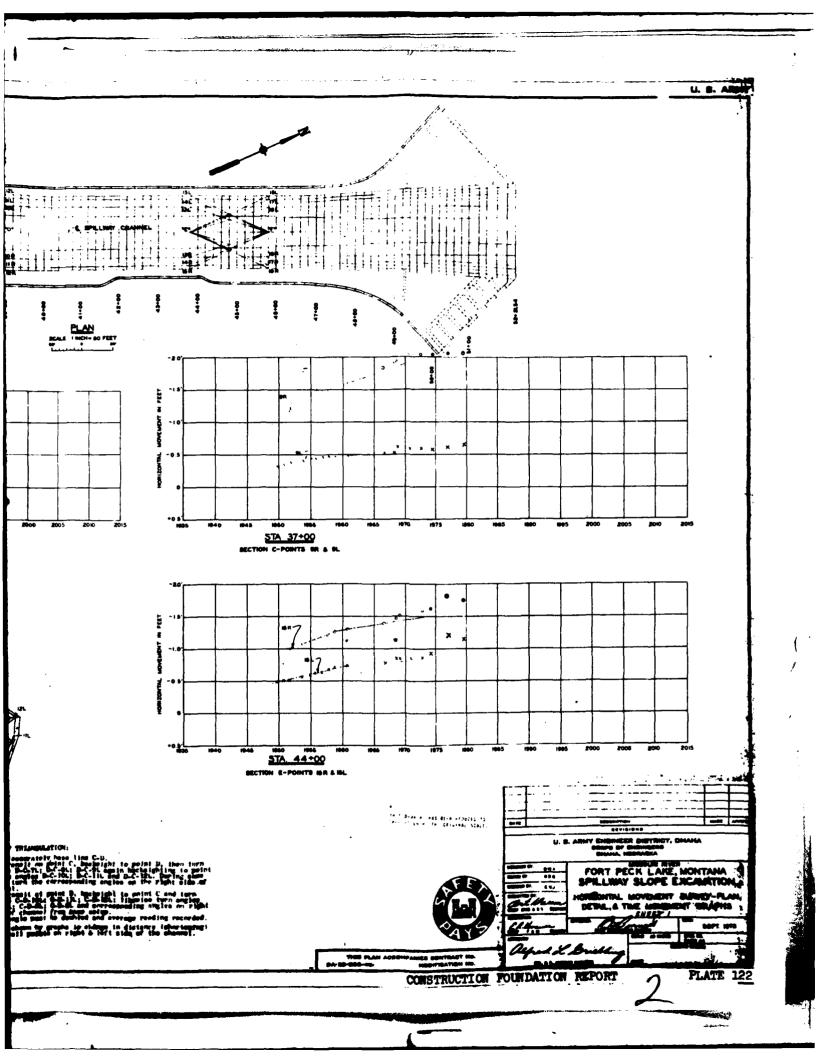


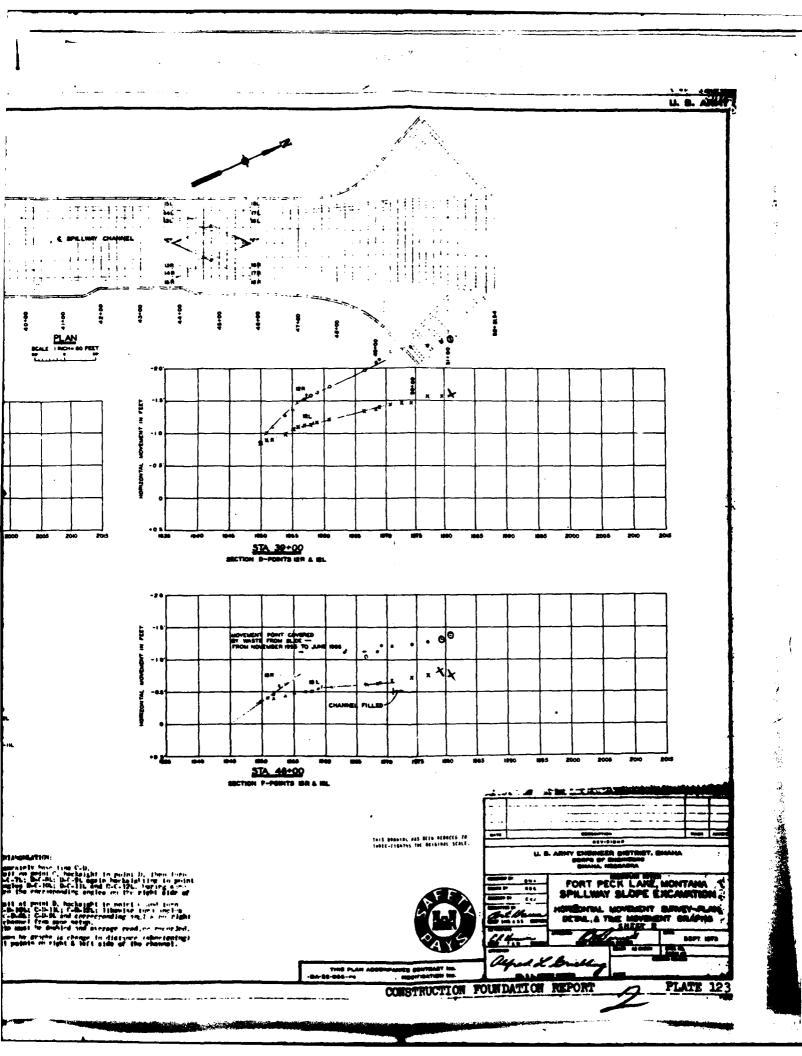
PLATE 120

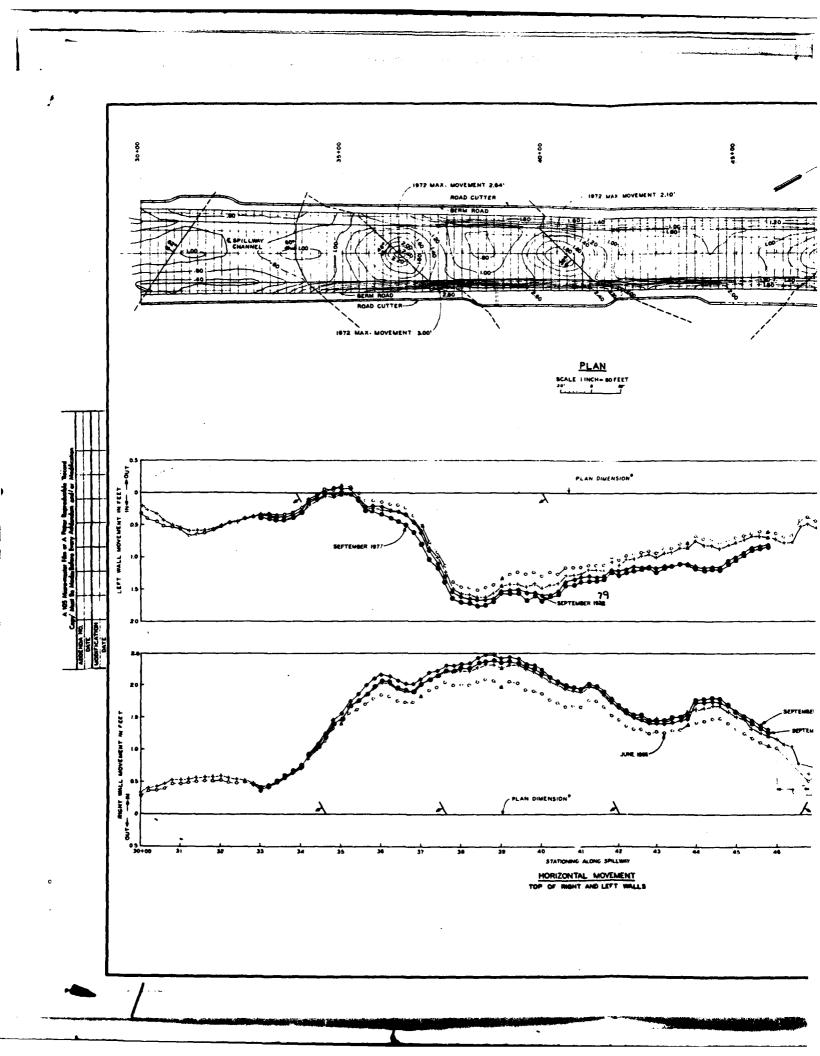


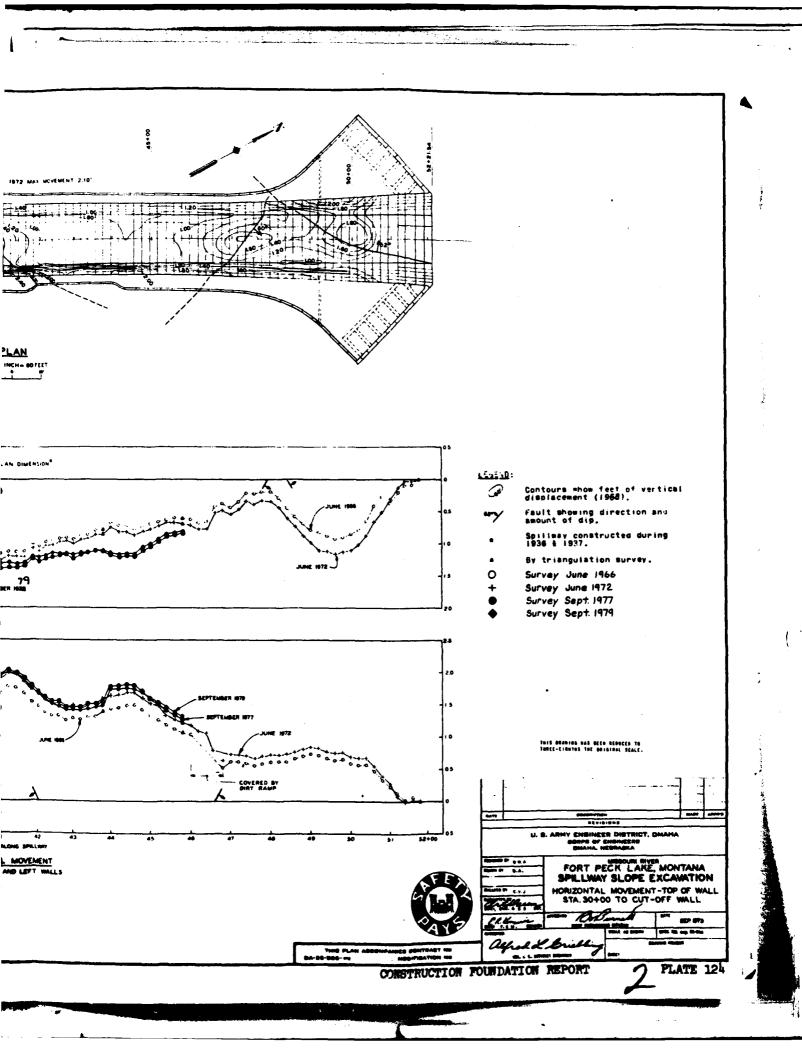
CORPS OF ENGINEERS 32+08 94.00 89-68 # # # STA 33+00 SECTION A-POINTS SR & SL ISUNETRIO VIEW OF LEFT SHIE OF SHILLANY CHARAEL PETMEEN SIA. 37400 8 87A. 3940C SHOWING METHOD OF TRIANGULATION

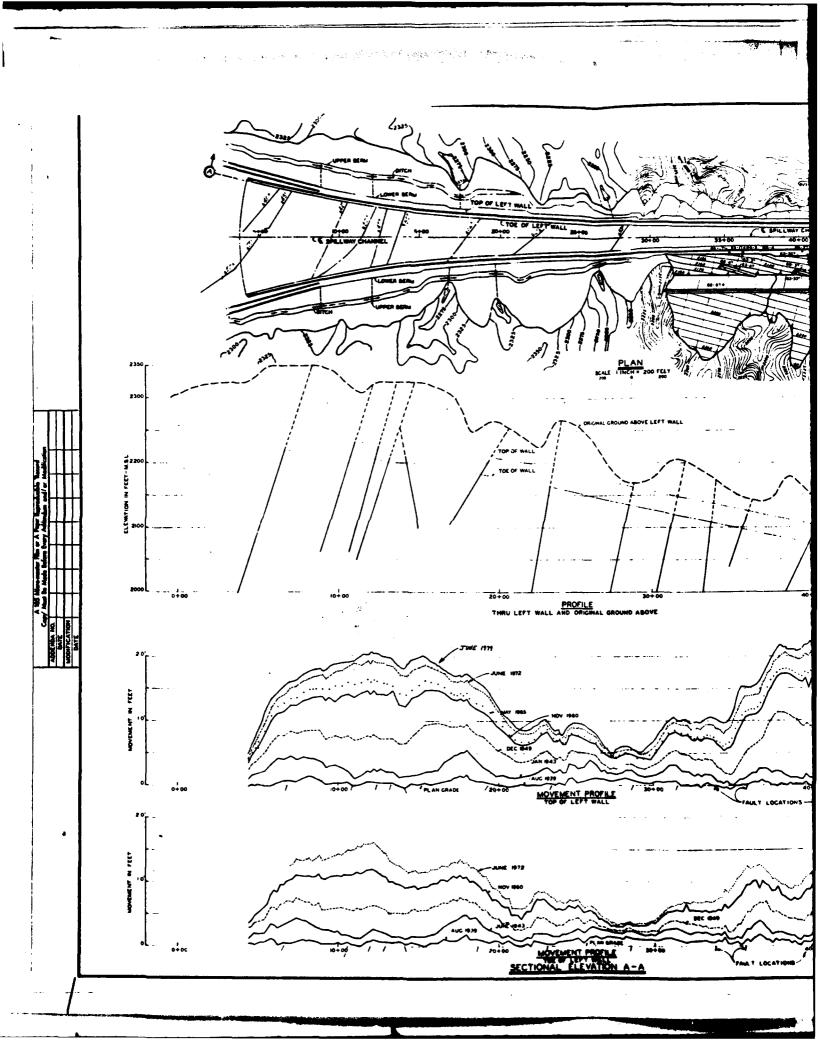


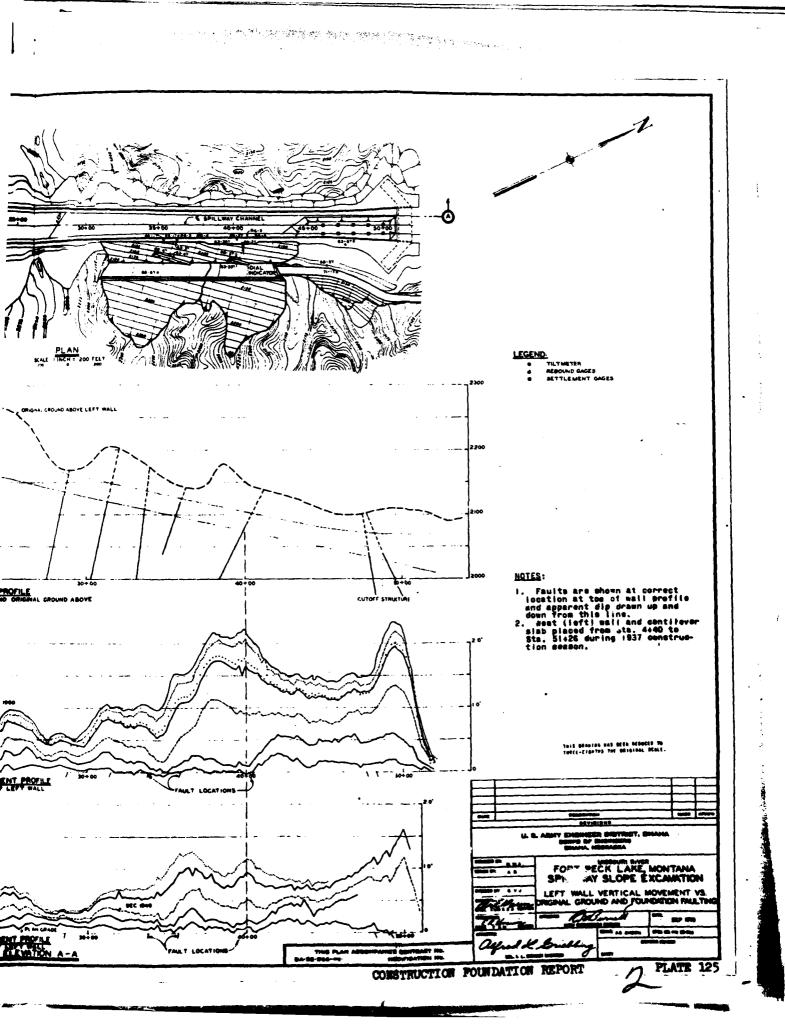
14 min --------CORPS OF ENGINEERS 32-00 STA 35+00 SECTION S-POINTS OR A SL ₹~ ; ; · * MINE: 1. MINE OF THE ANGULATION: i. TO IT STO INTO SELECT A OF STREET THE CONTRACTOR OF THE SERVICE OF THE SHARE STATE OF THE SHARE SHARE STATE OF THE SHARE SERVICE OF THE SERVICE OF THE SHARE SERVICE OF THE SER 2. Surgicing about he graphs to change in distance schoolsely between will points in right 5 left side of the change.

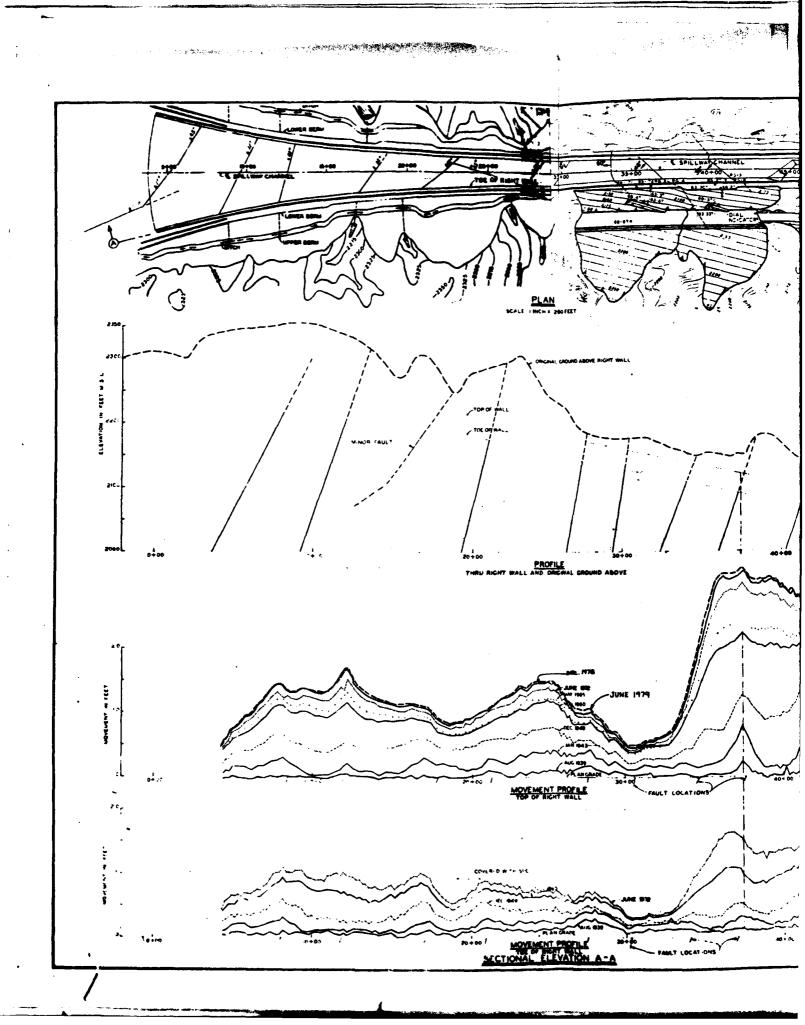


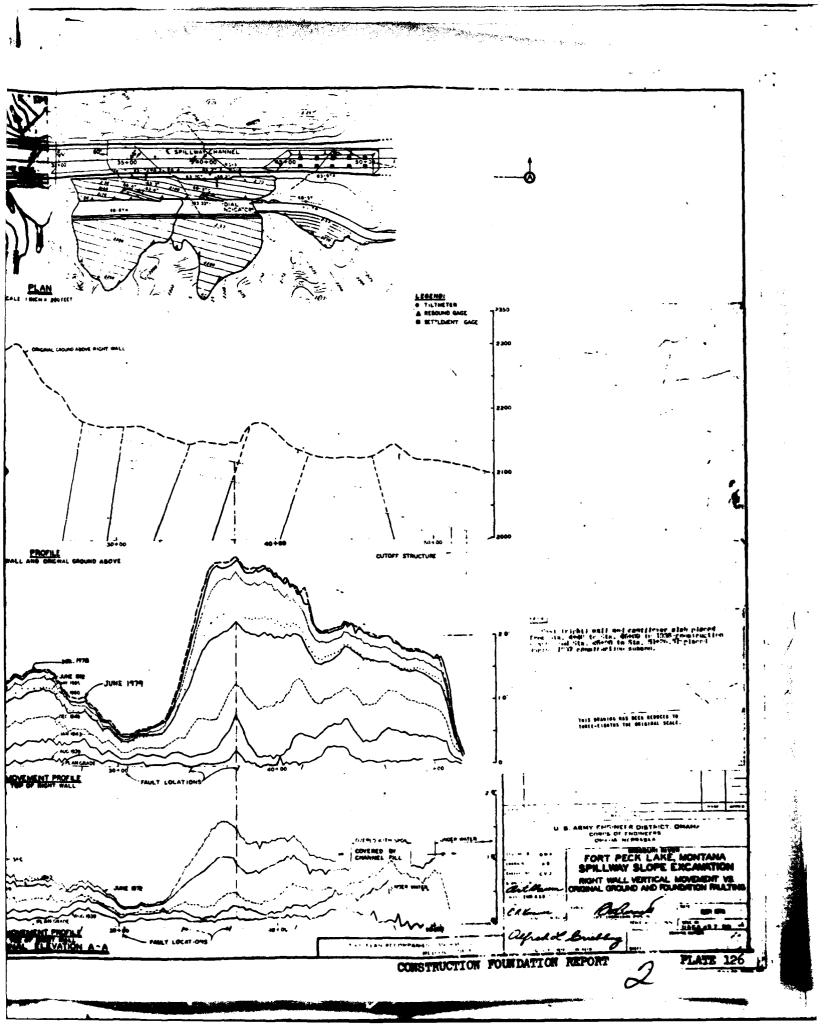


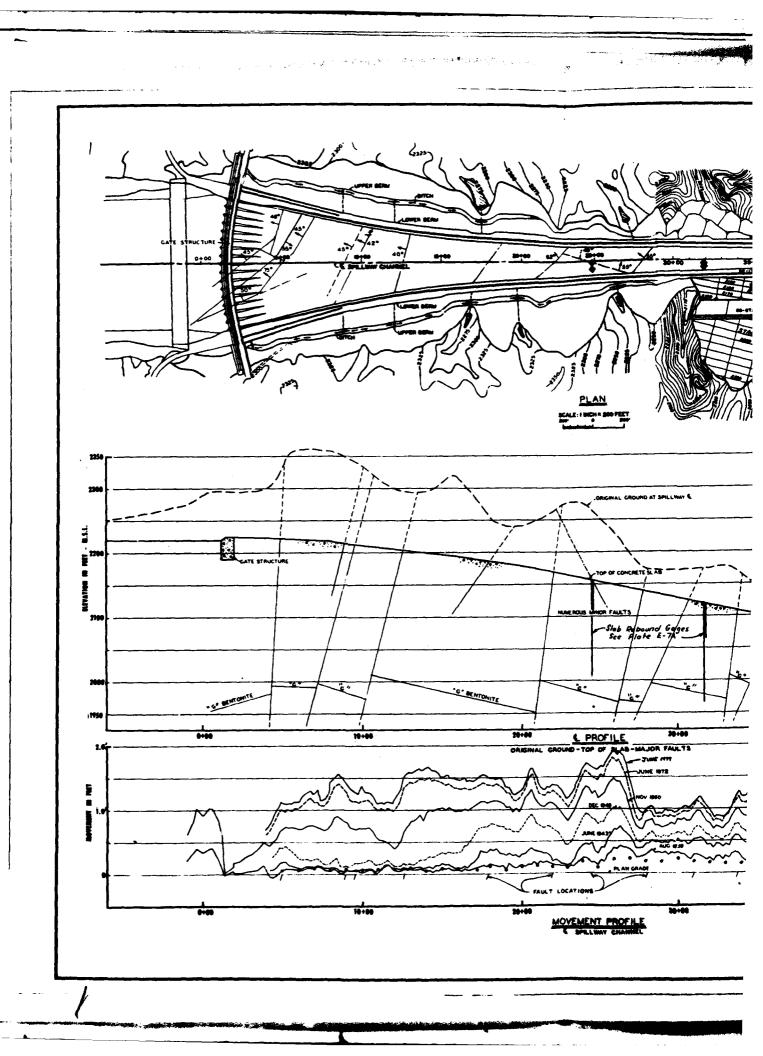


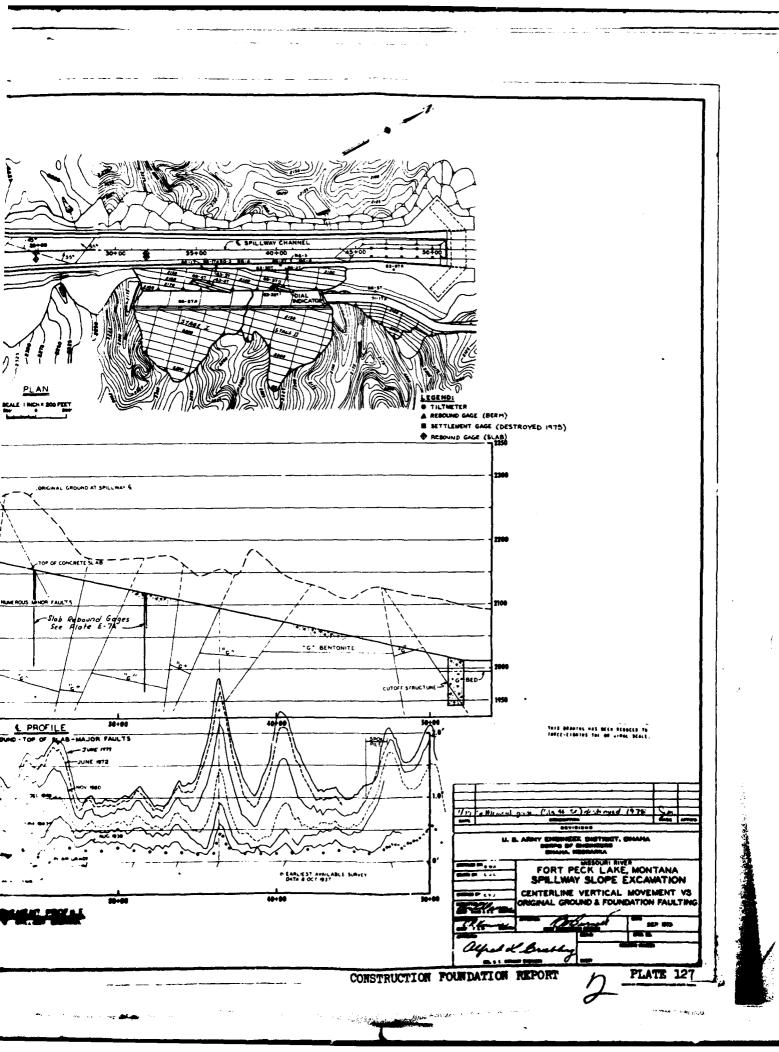


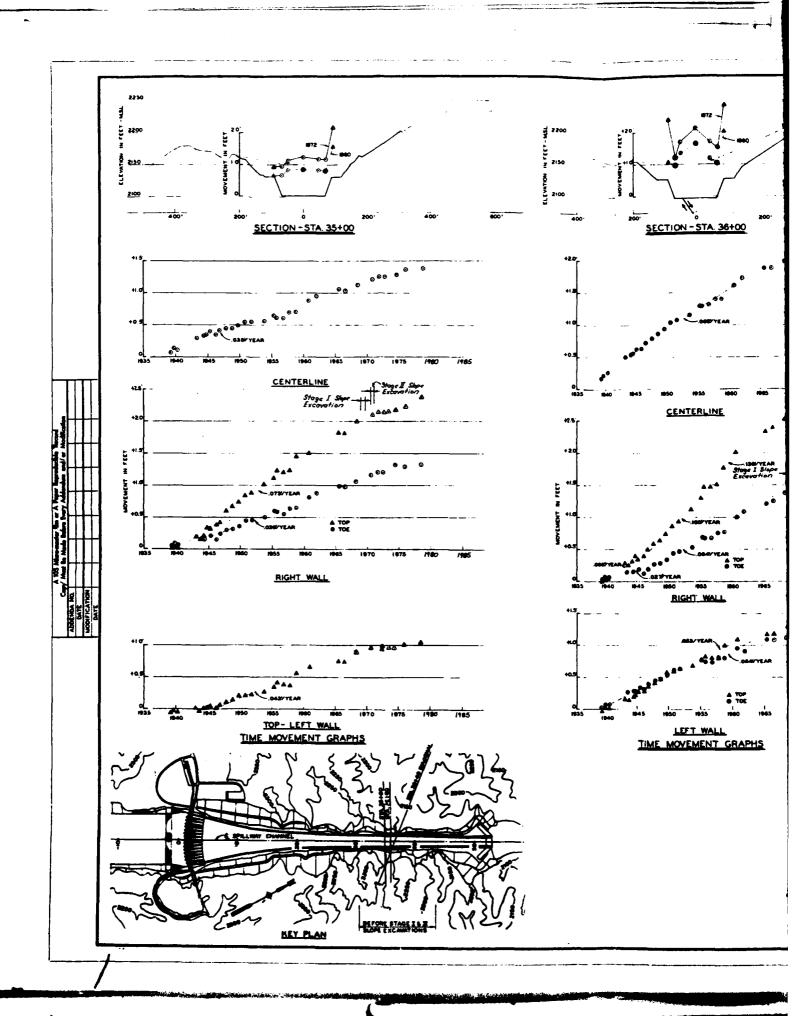


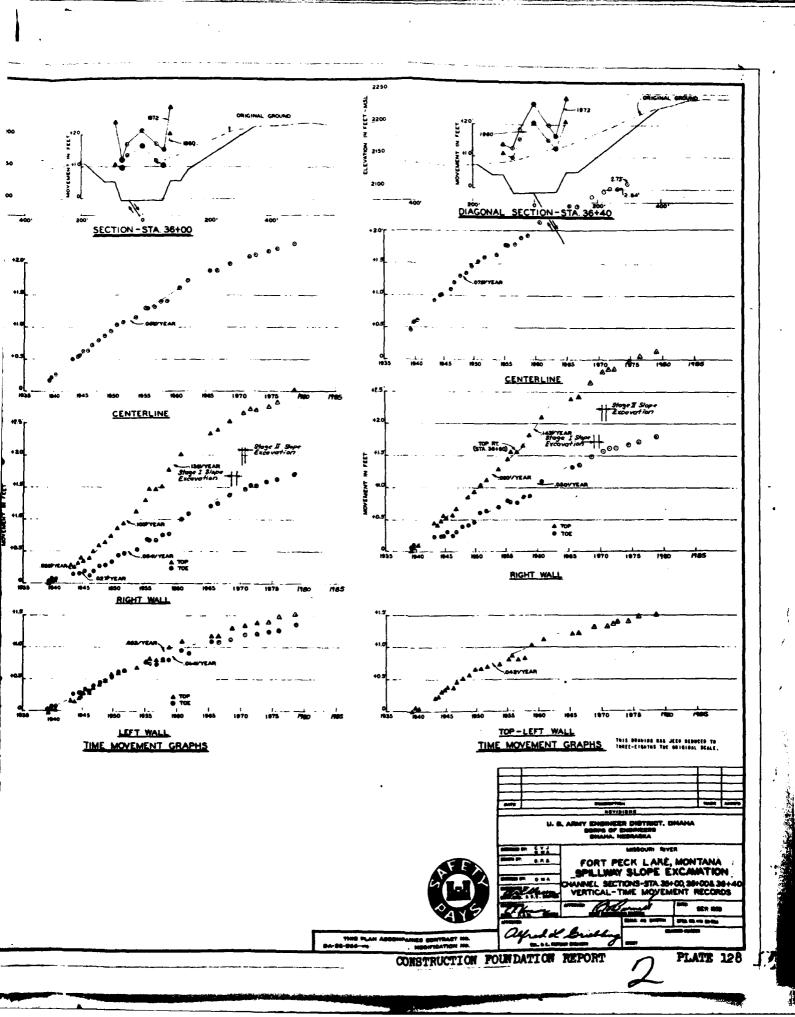


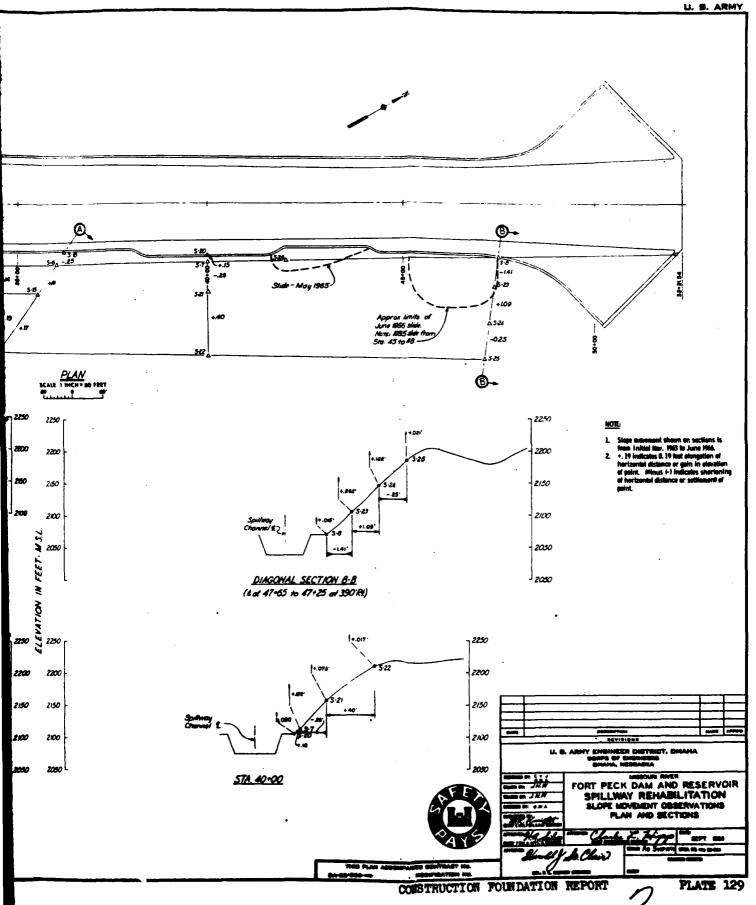


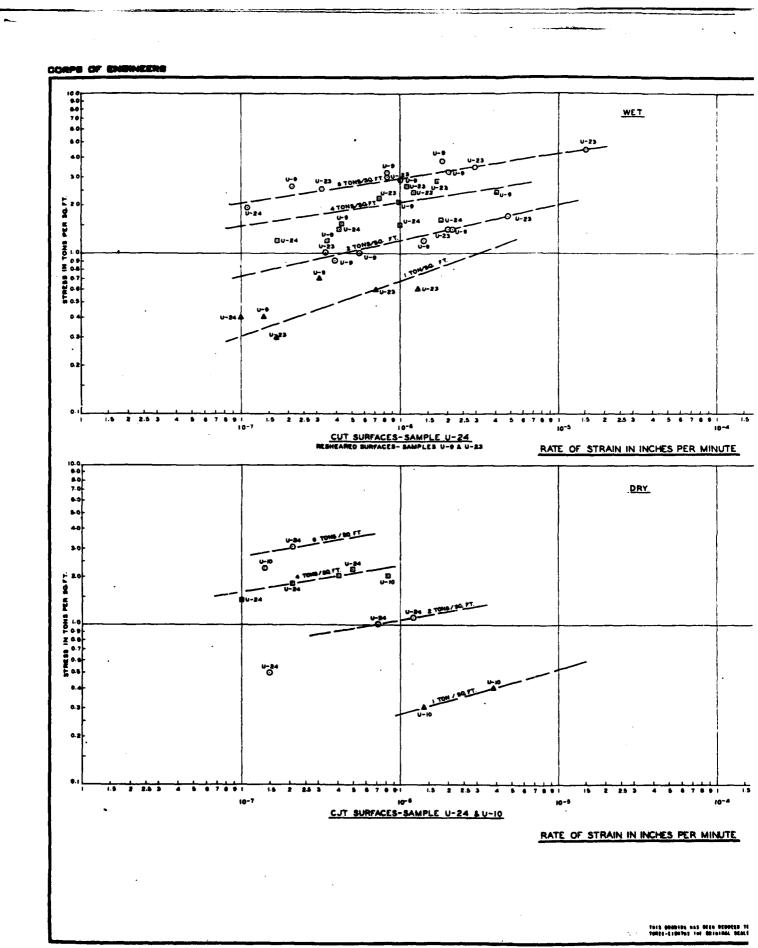


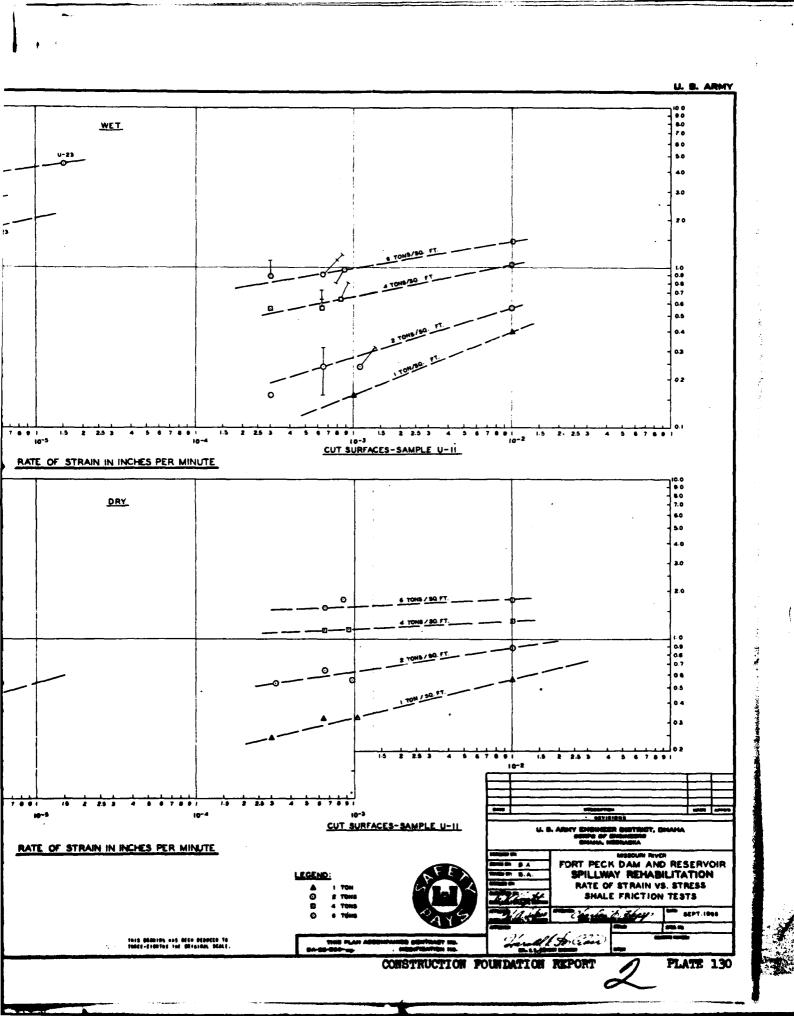


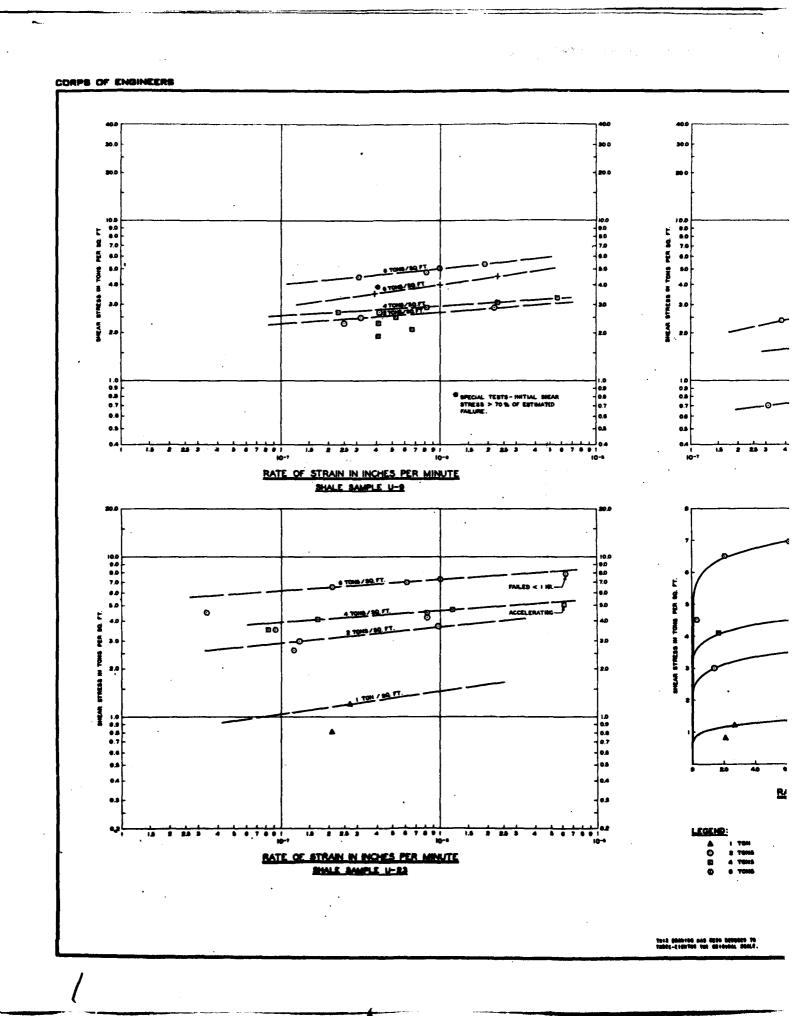


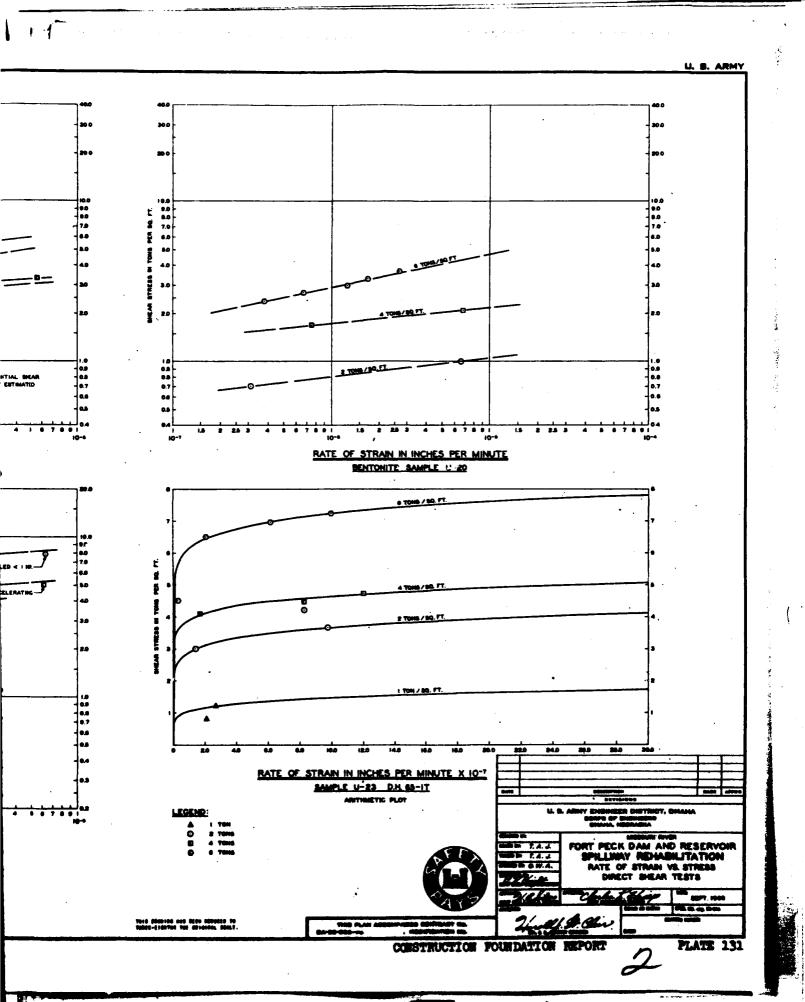












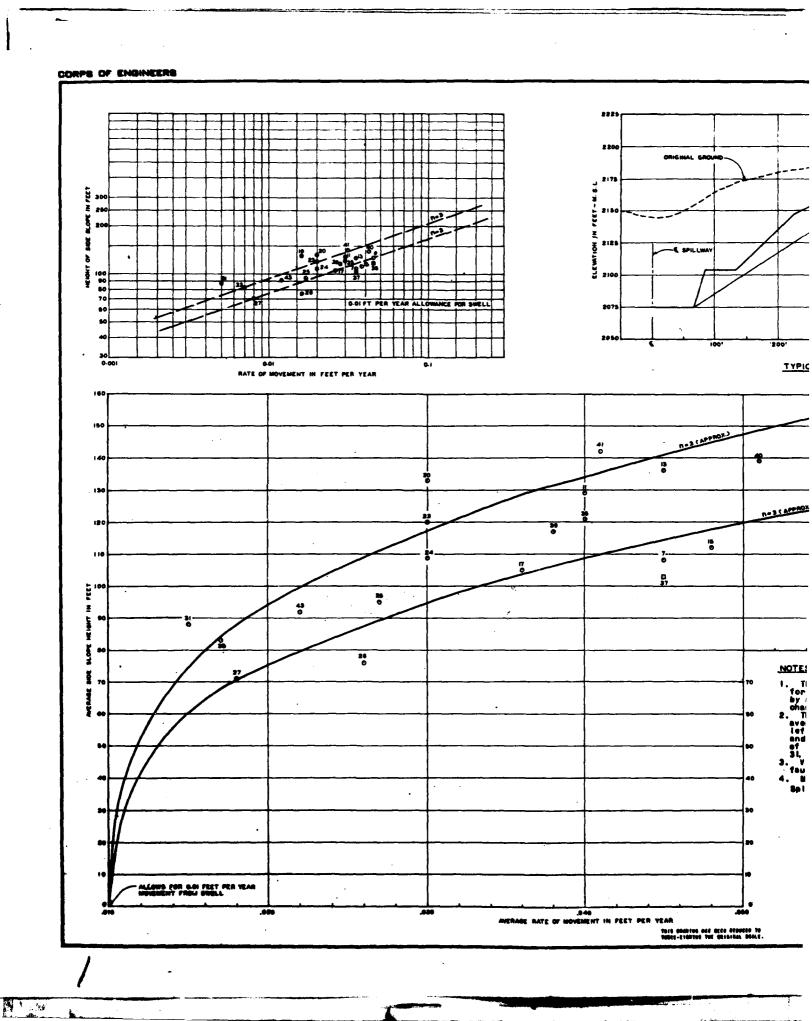
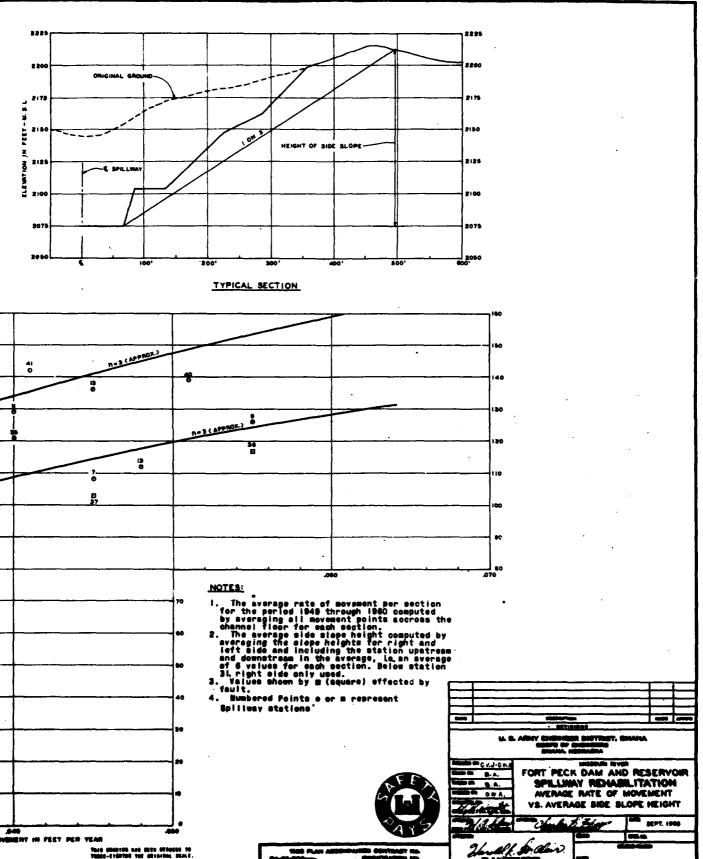
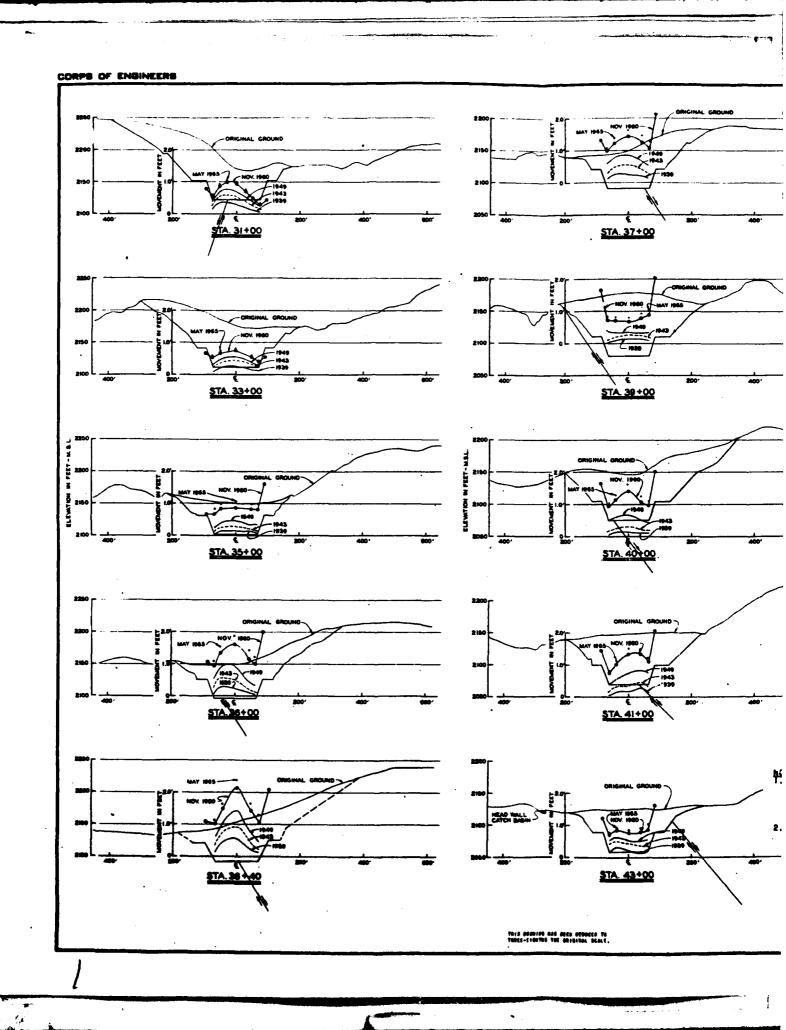
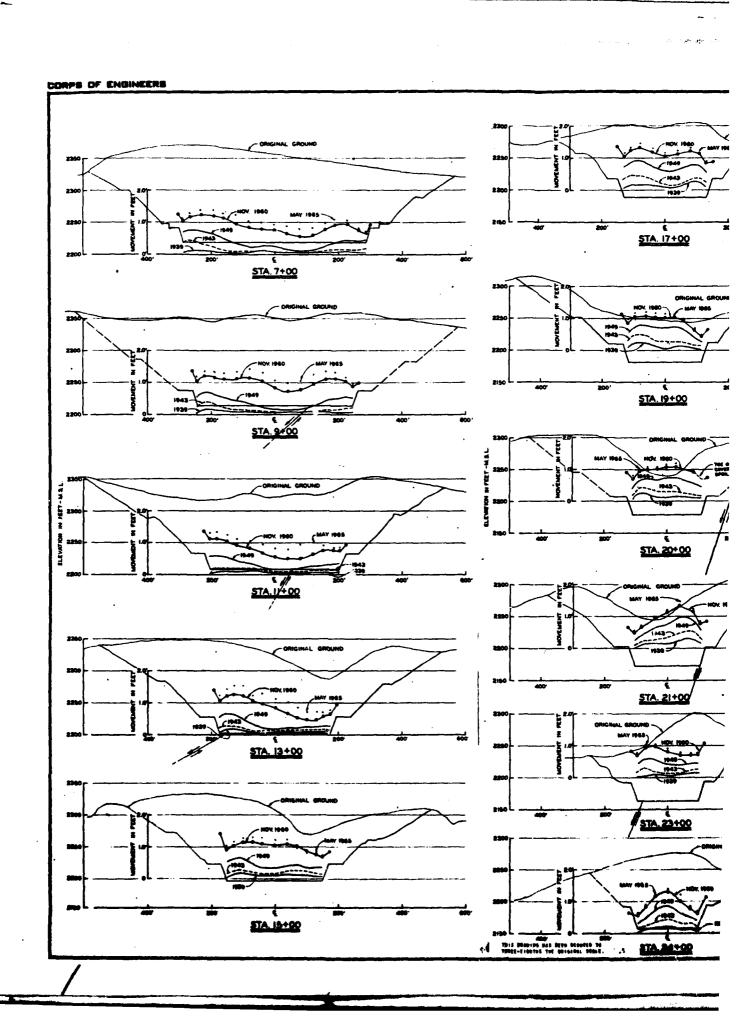


PLATE 132

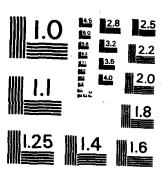


CONSTRUCTION FOUNDATION REPORT

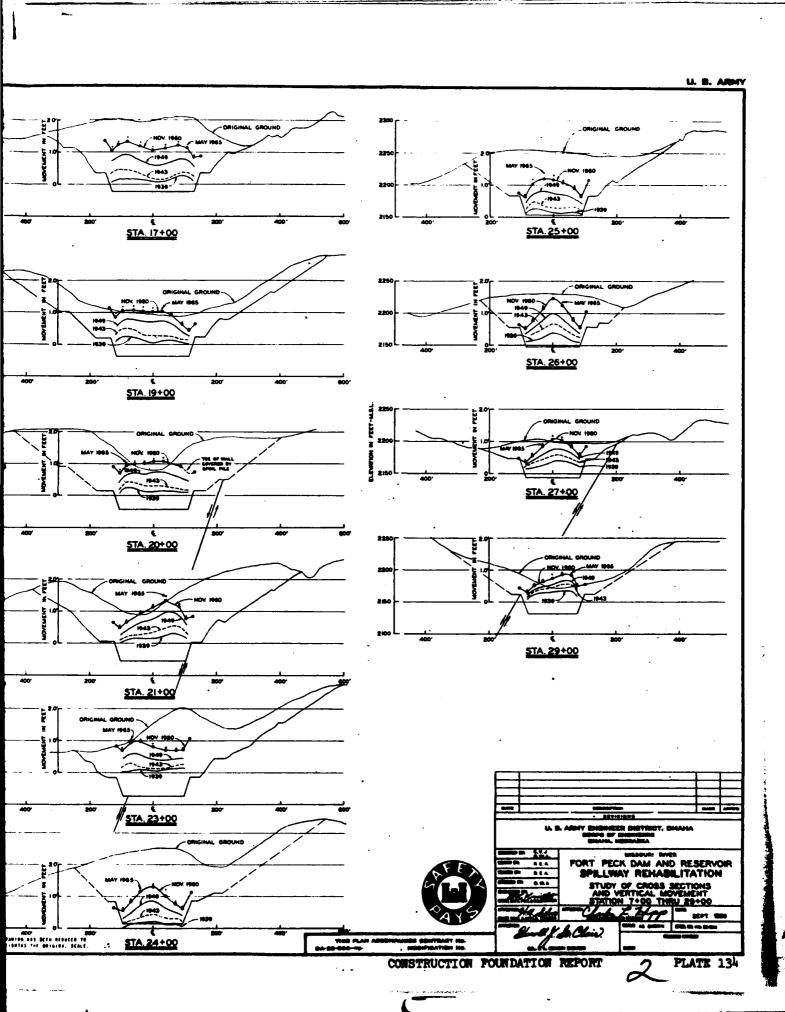


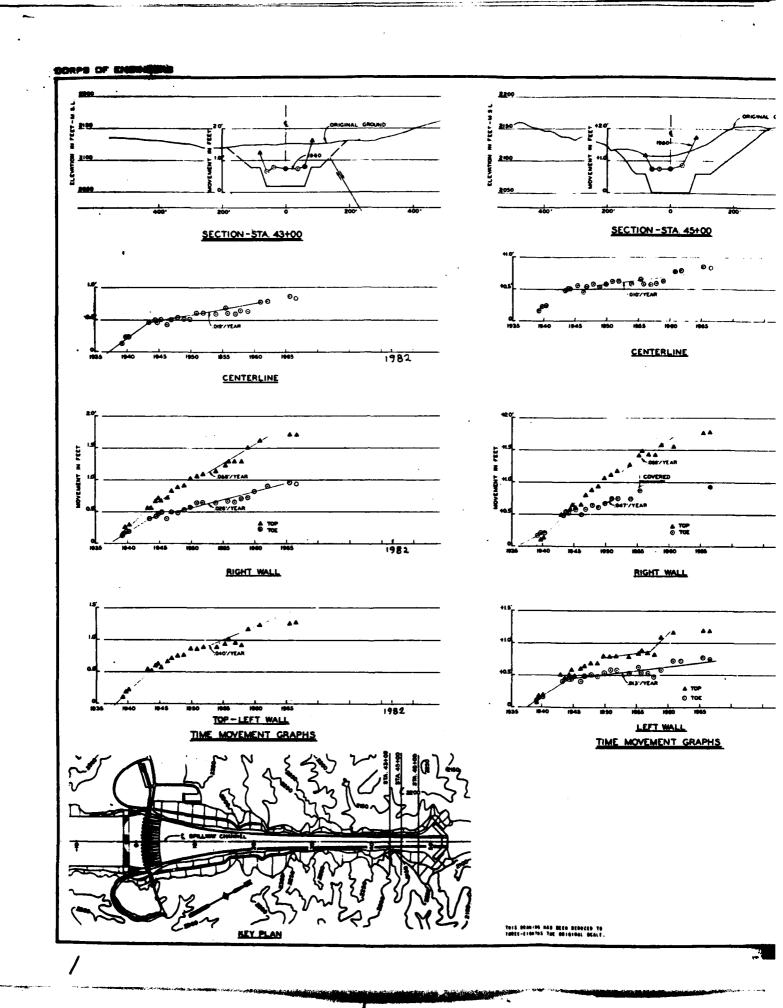


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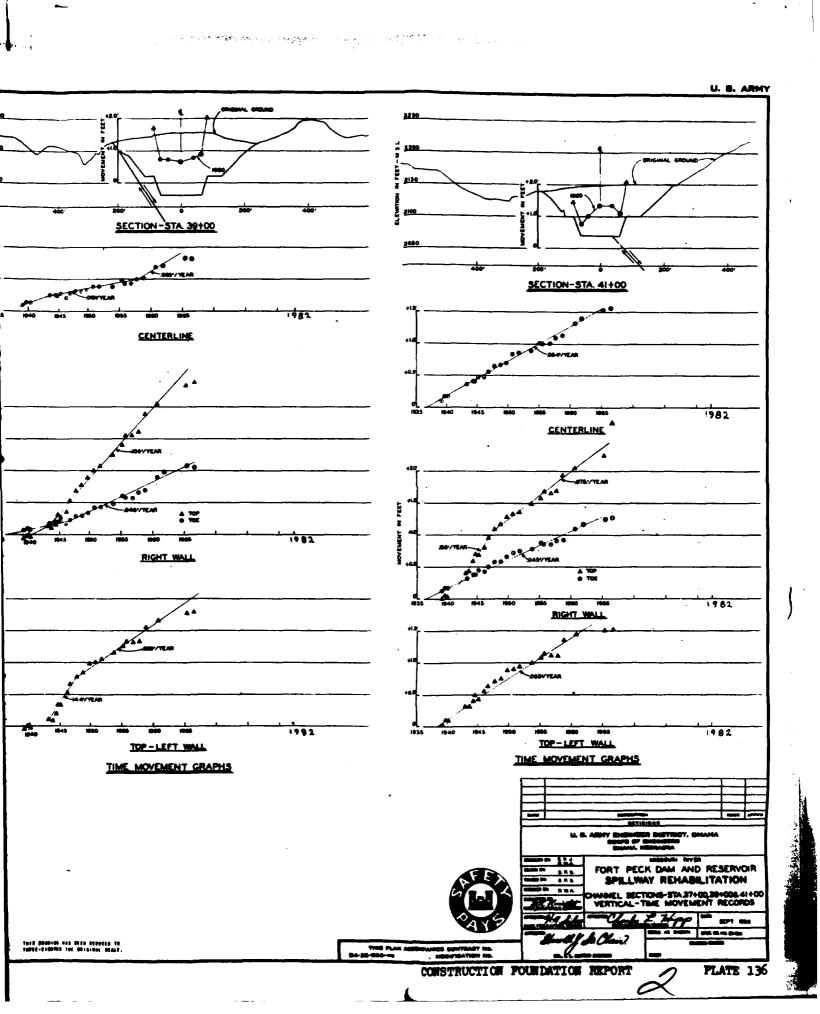


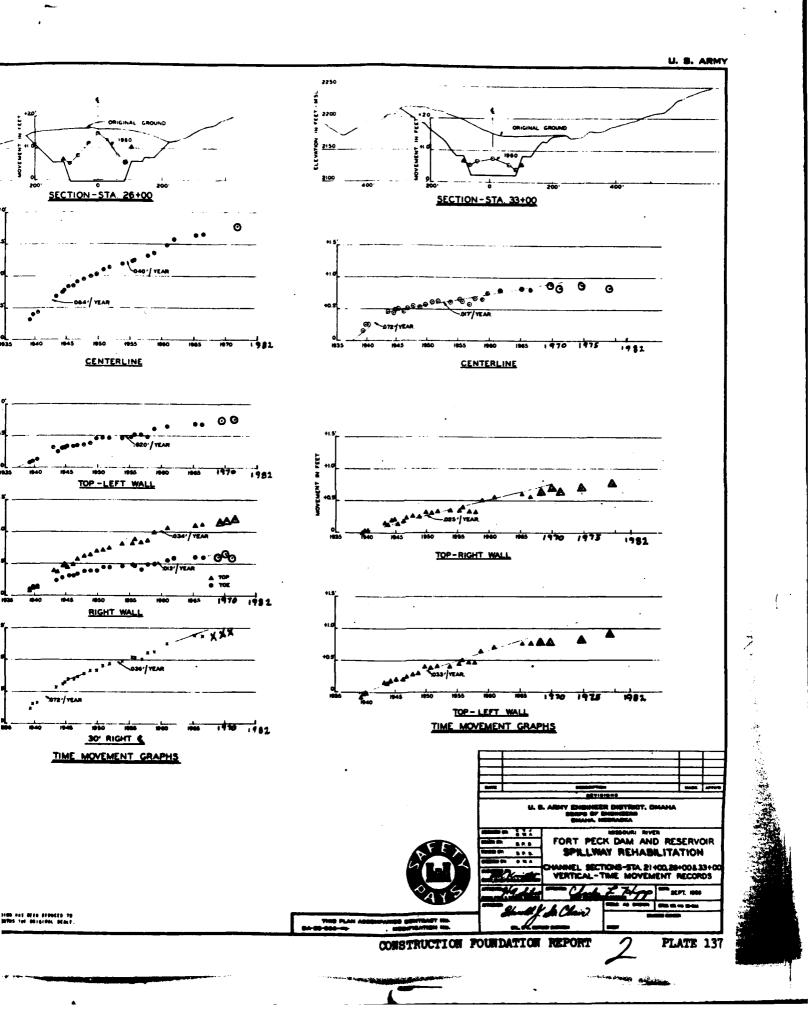
MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS -1963 - A

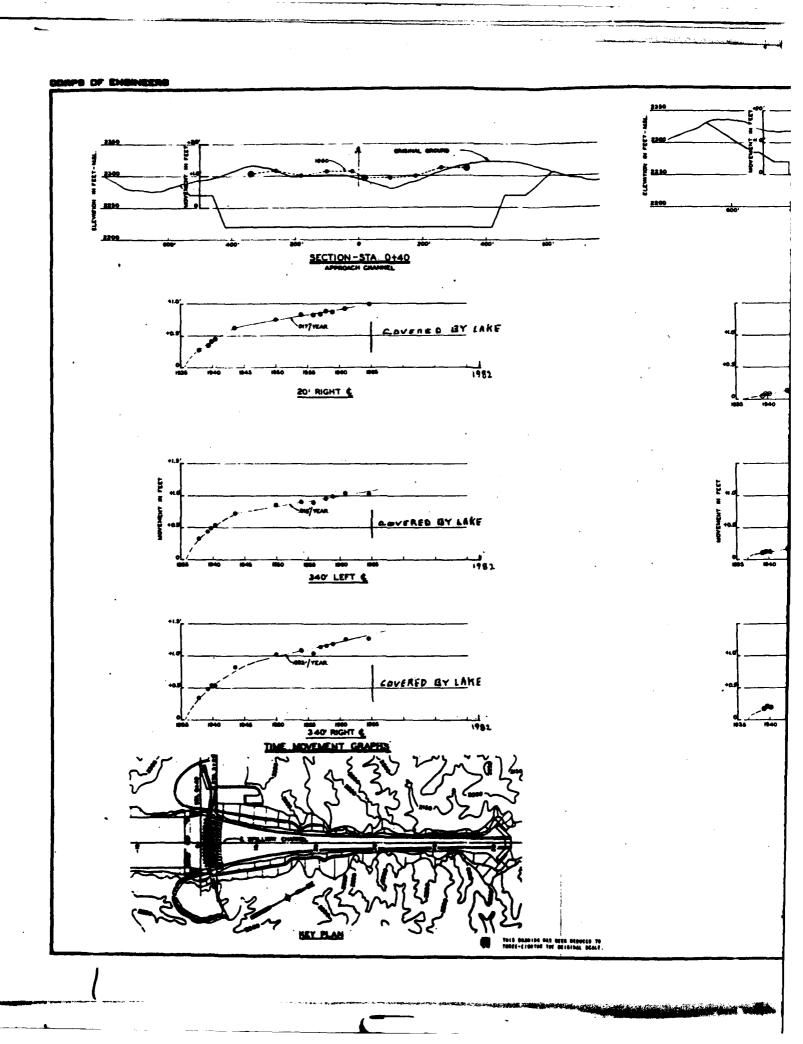


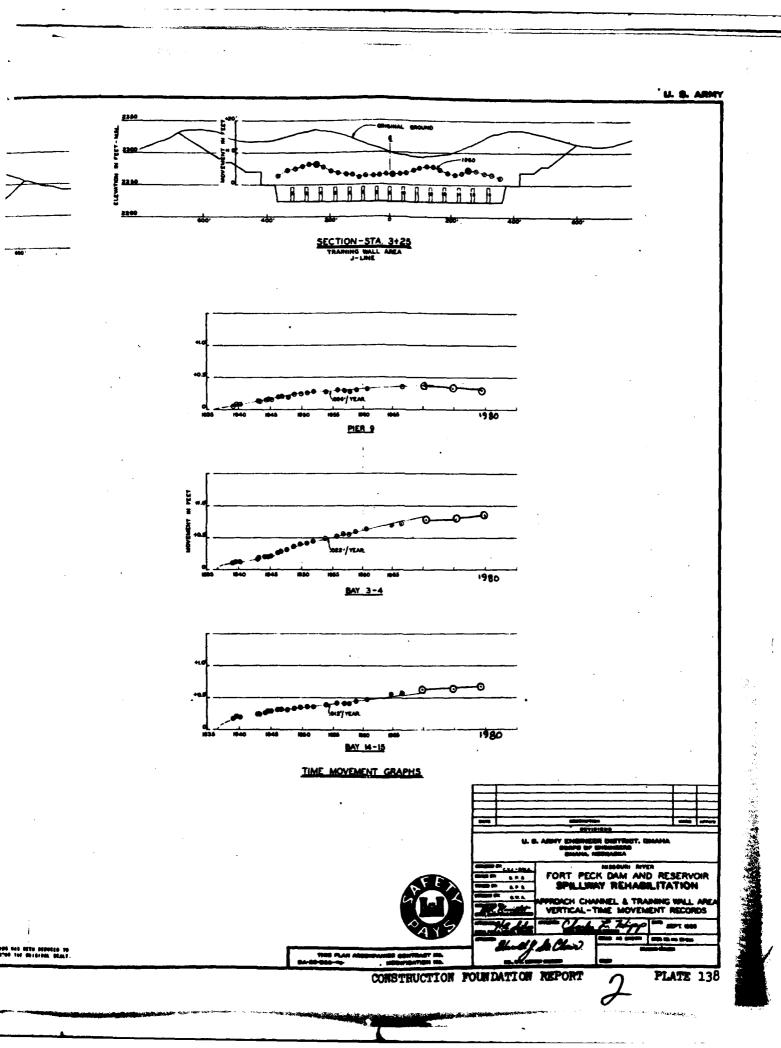


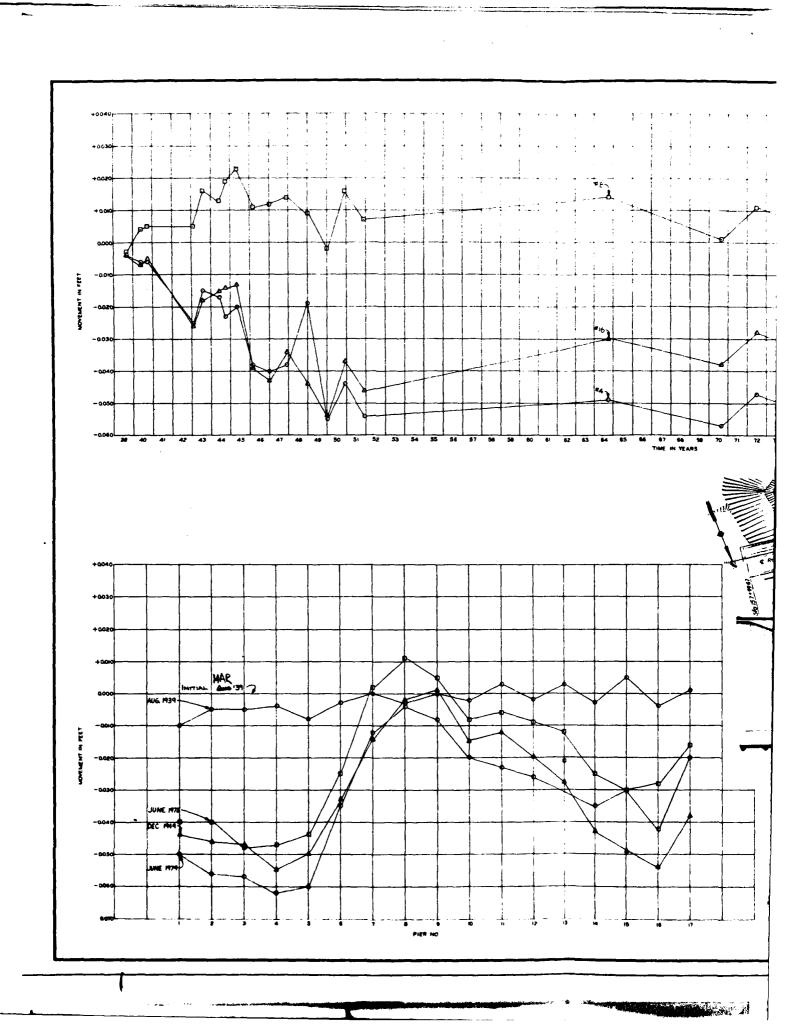
THIS DESCRIPTION HAS BEEN REPORTED TO THREE-TIMETER THE BRIDGE SCALE.

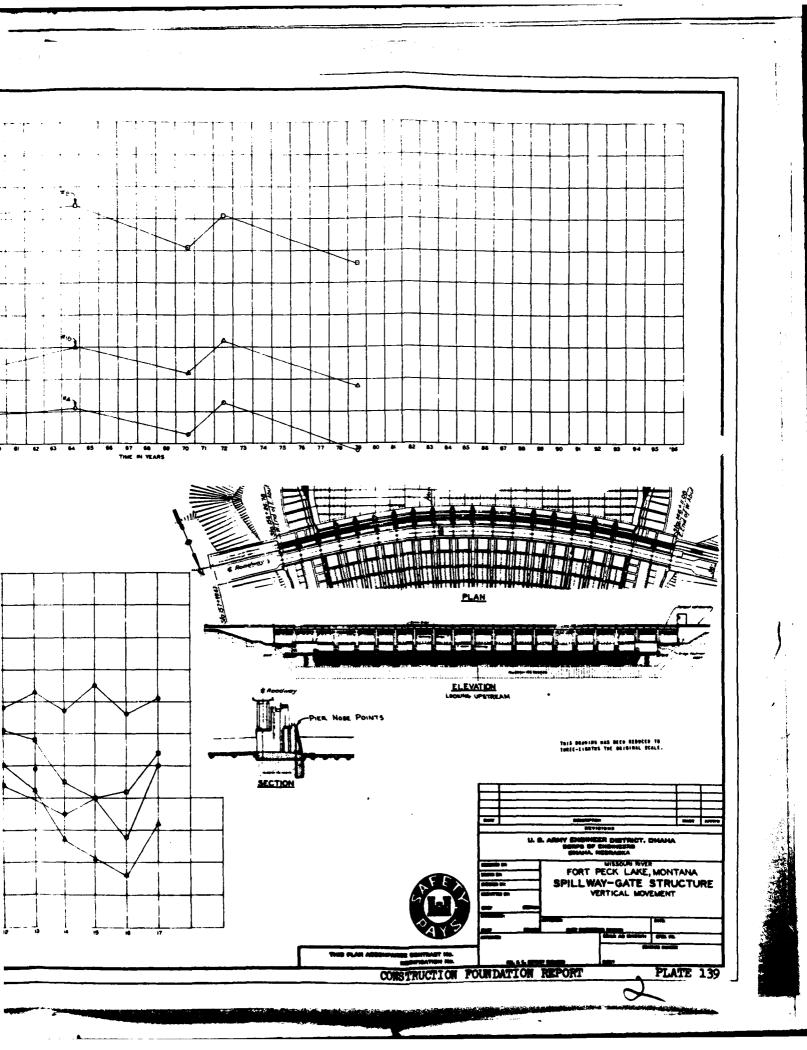


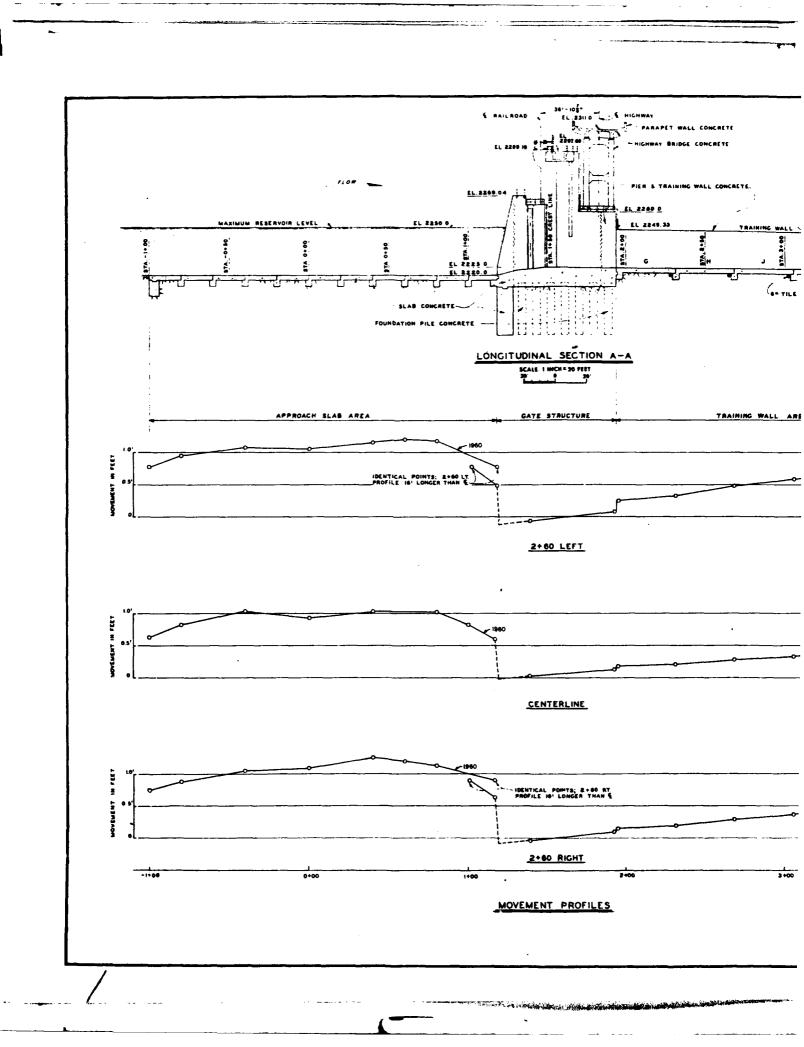


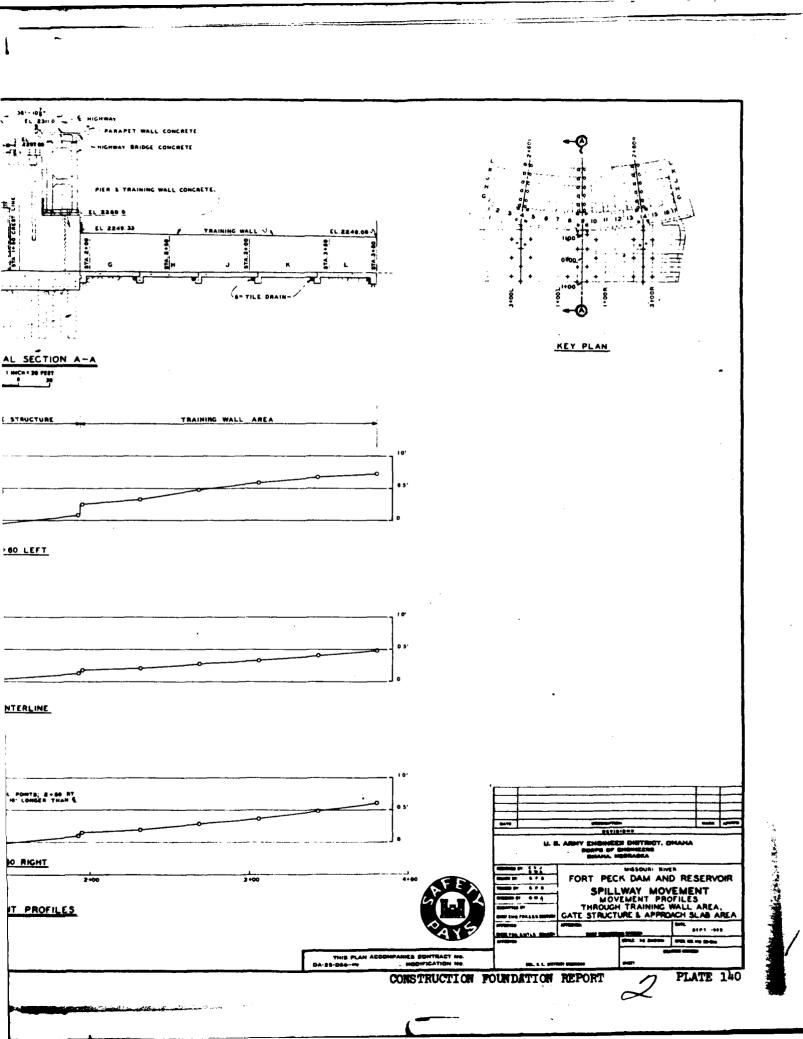


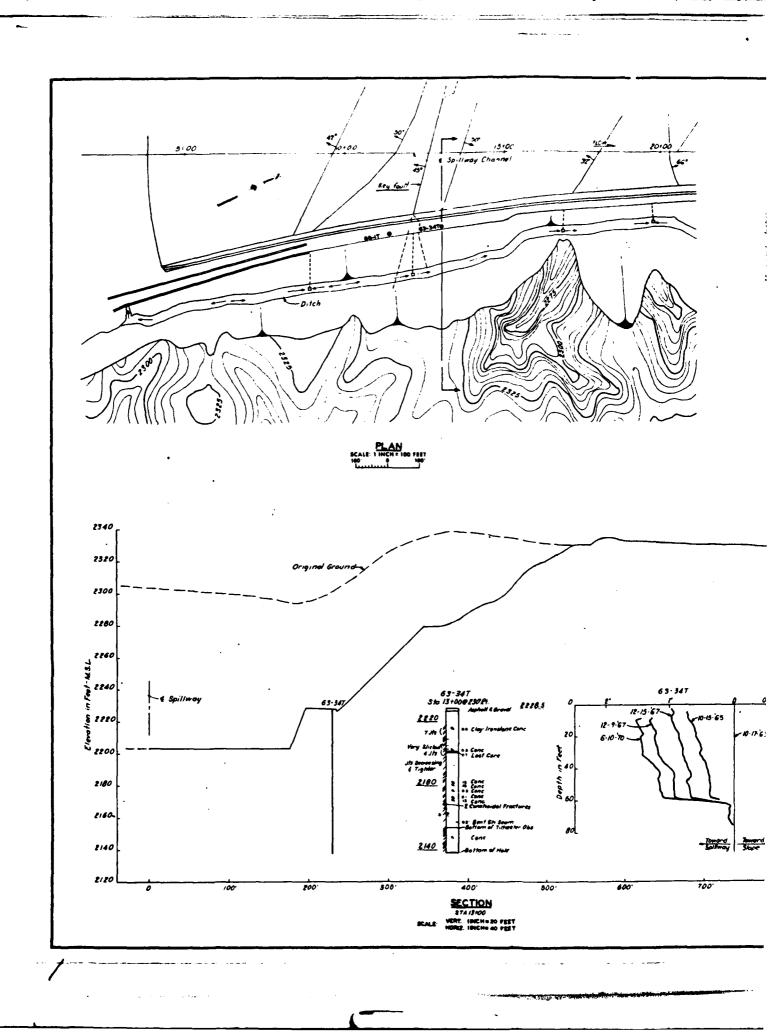


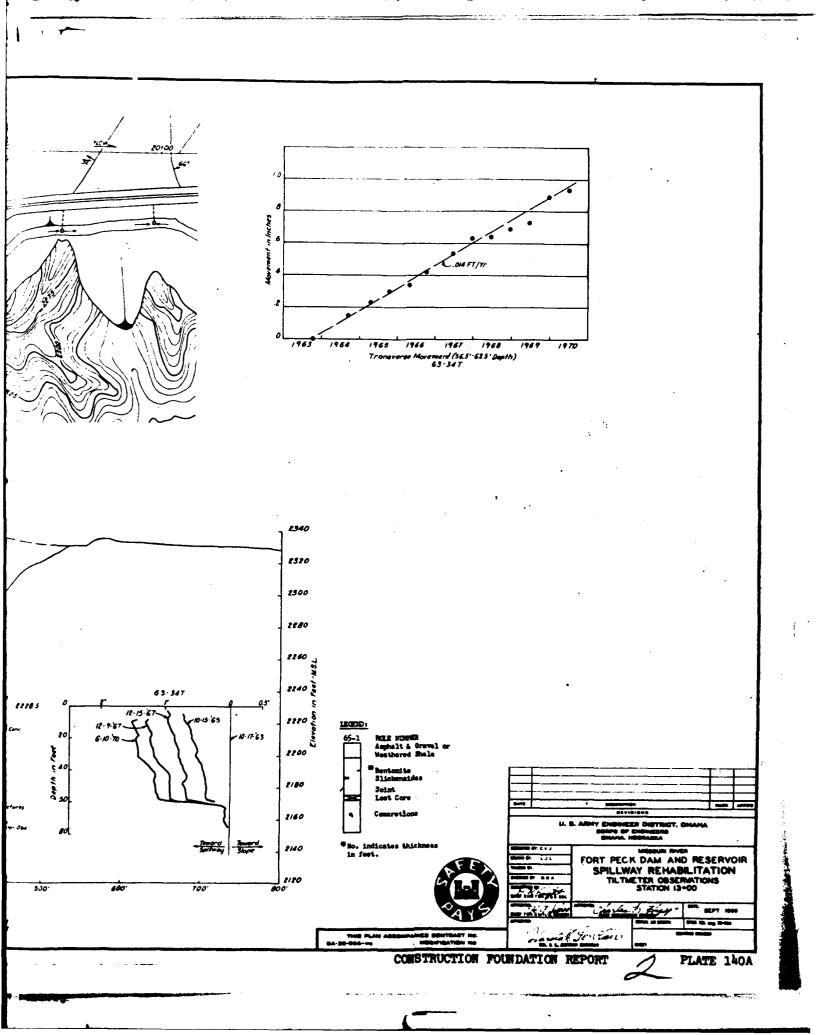


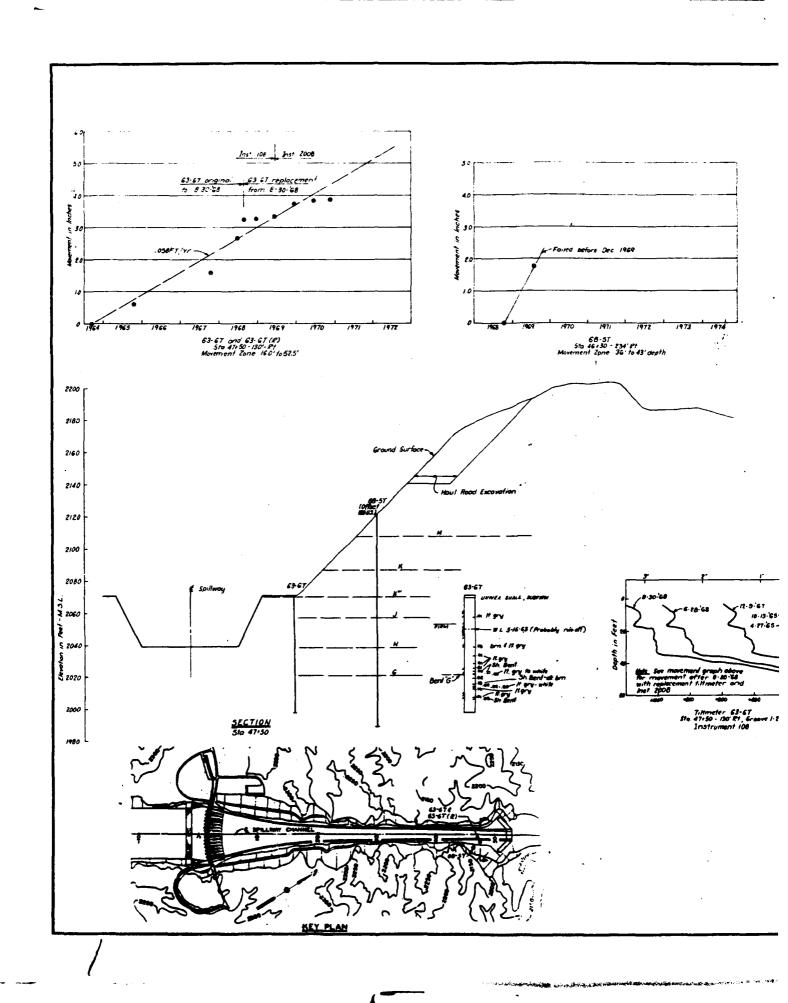


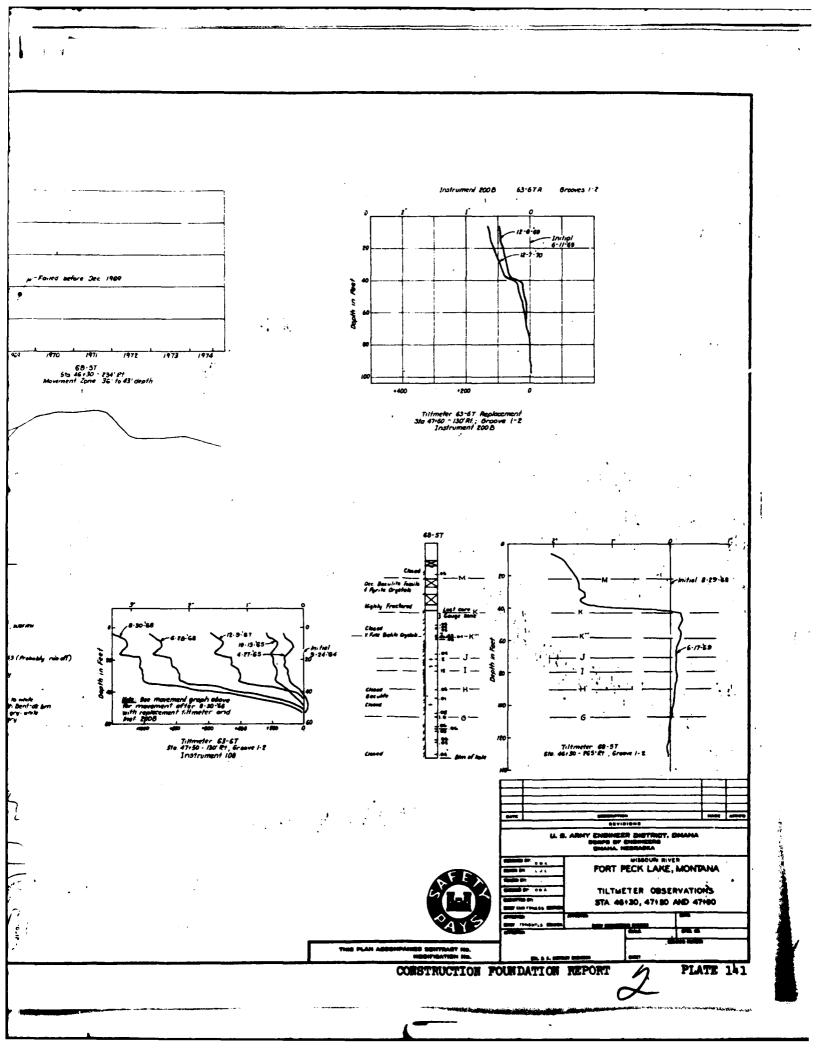


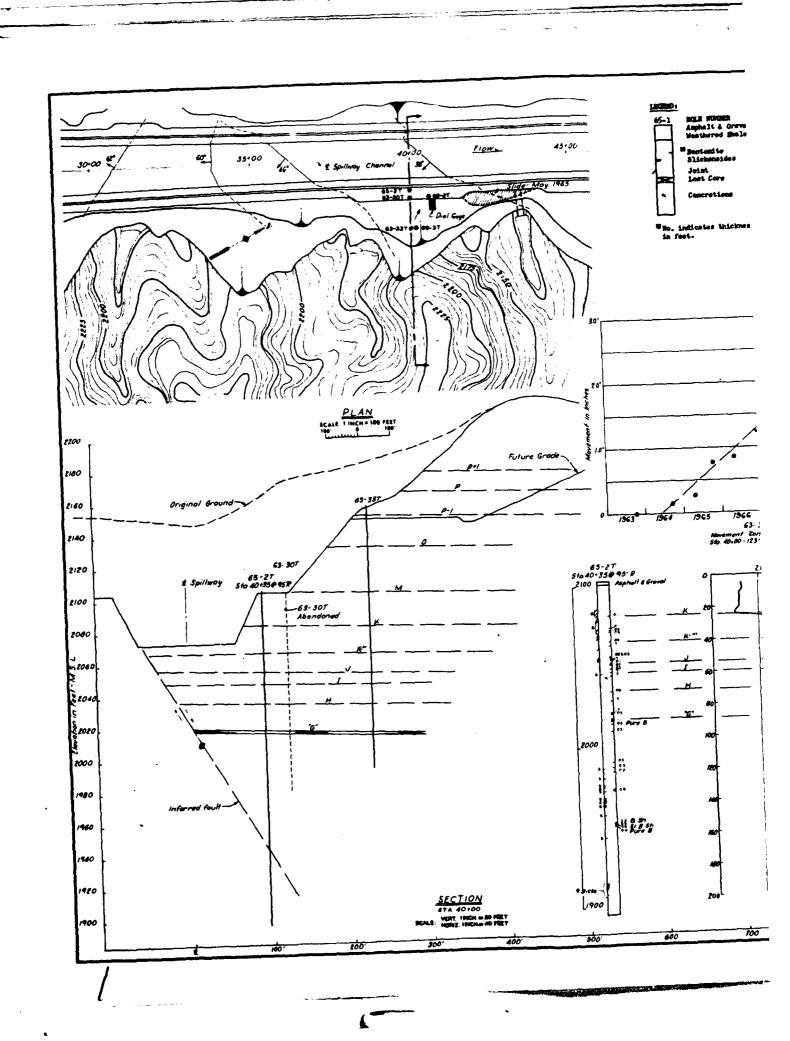


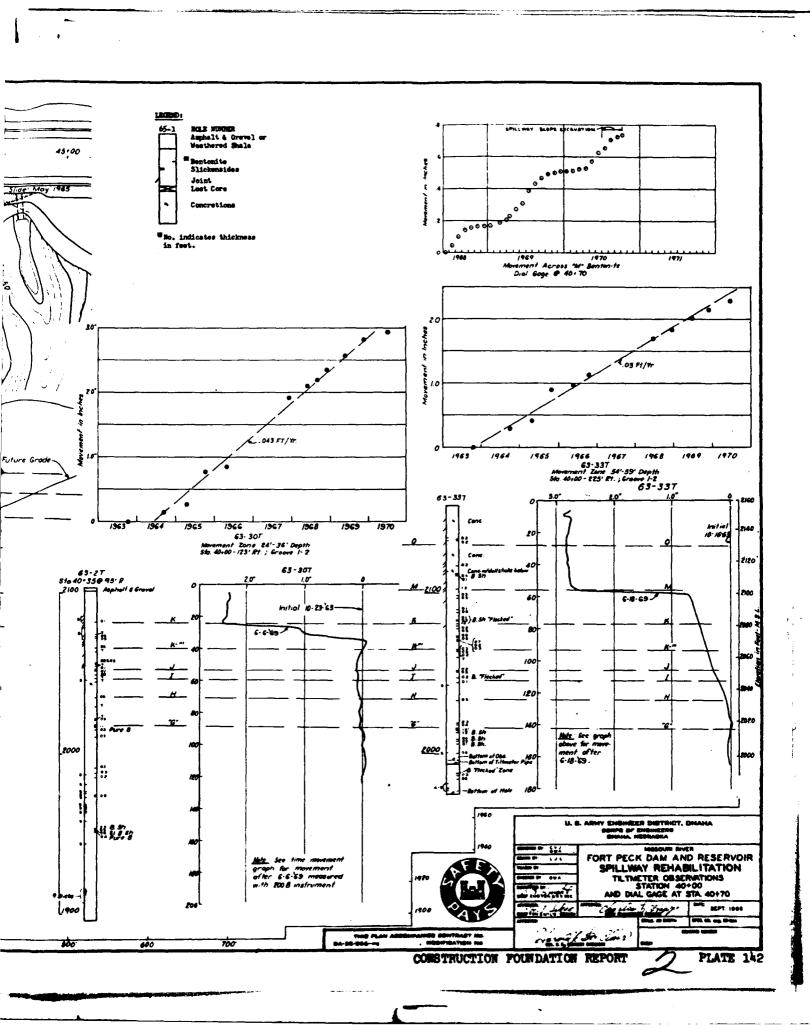


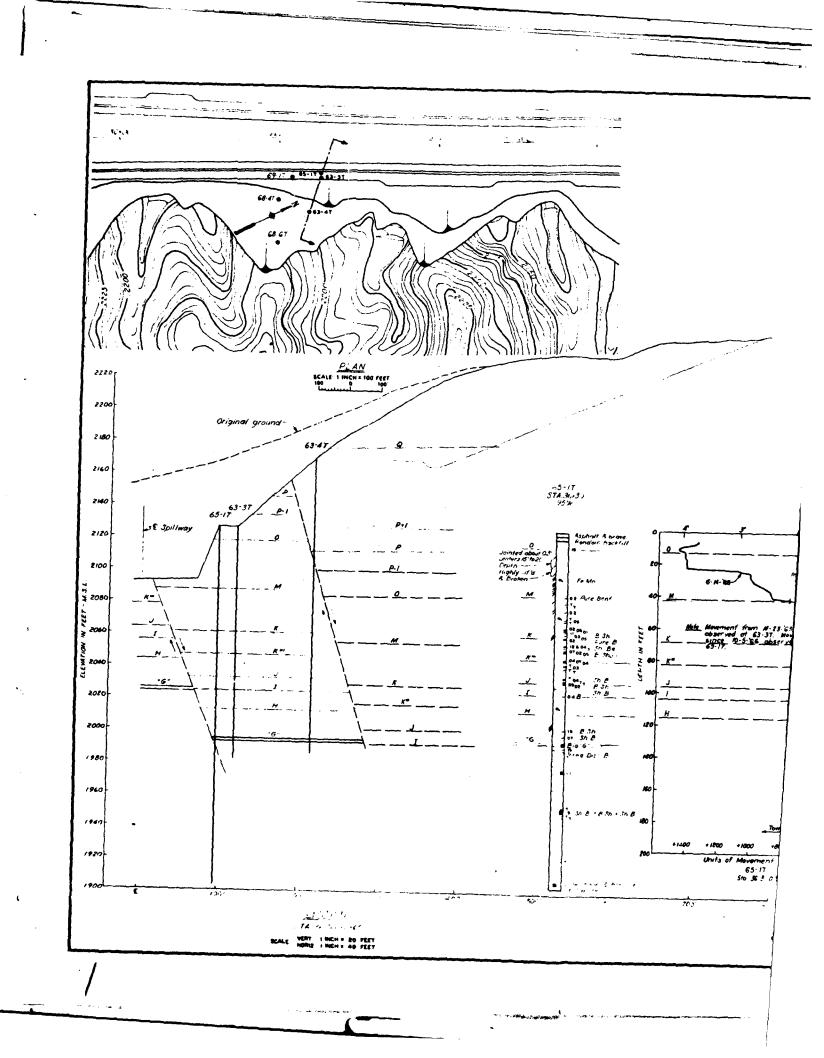


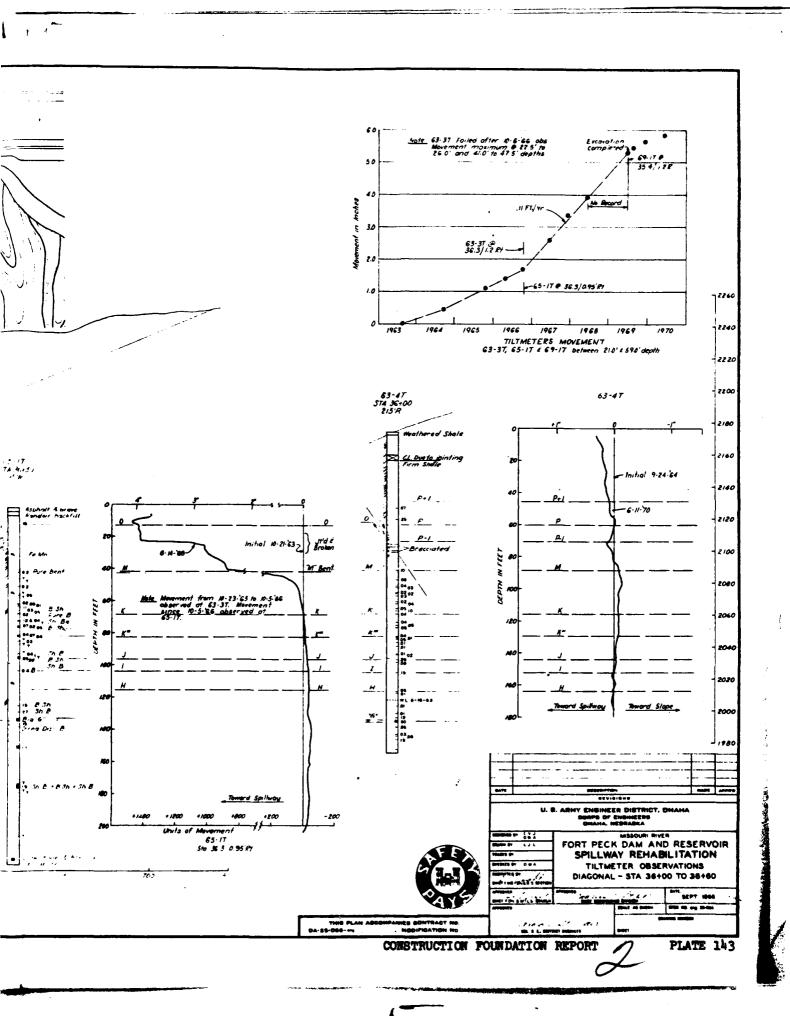


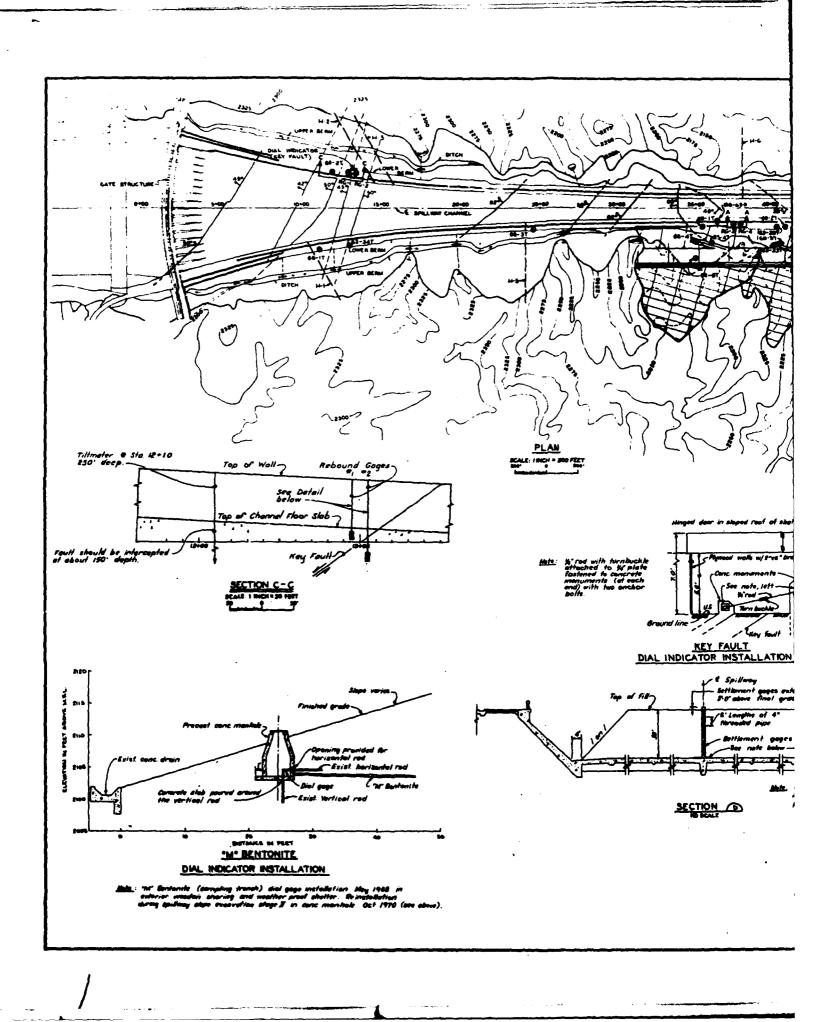


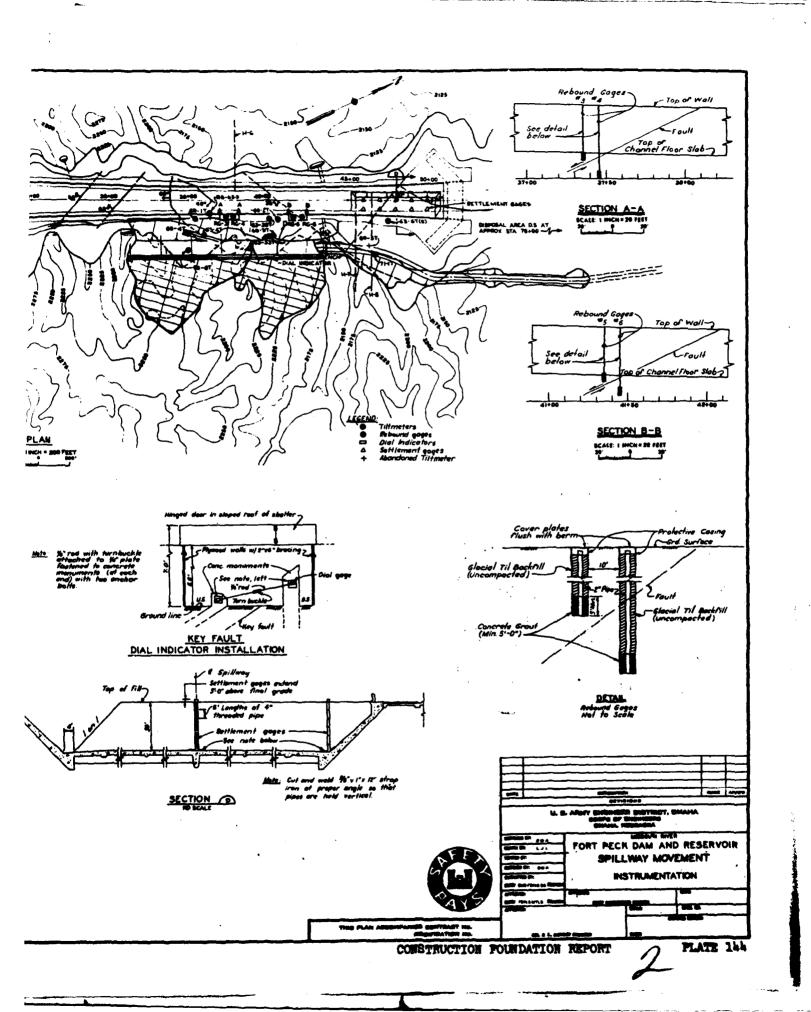


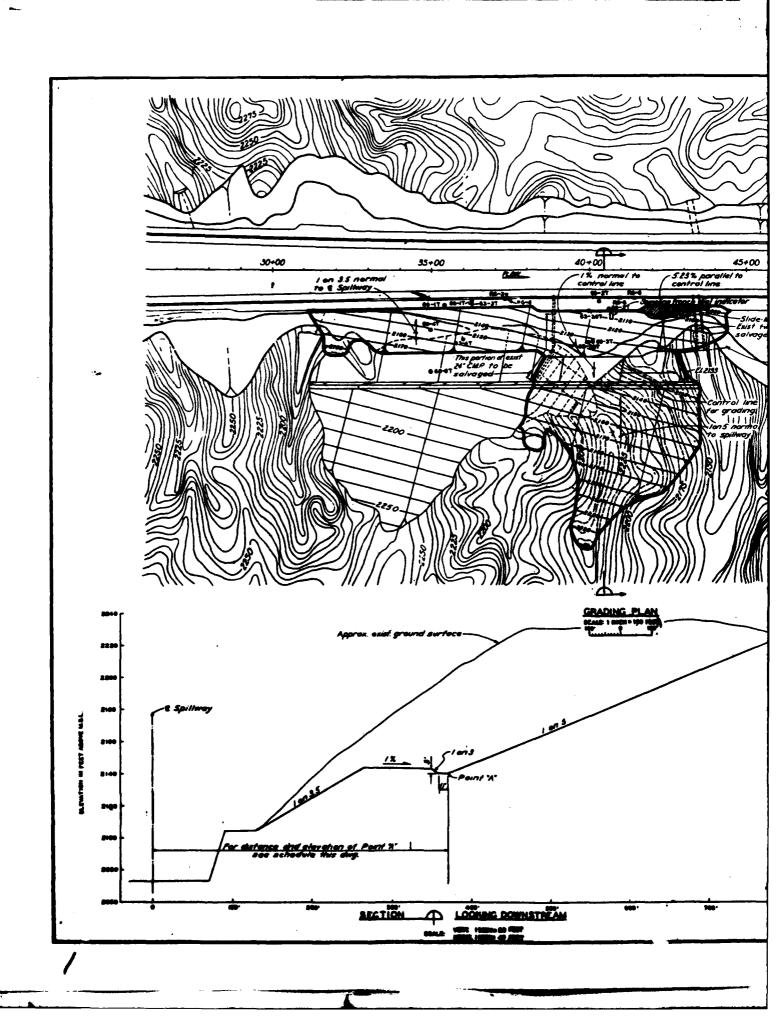


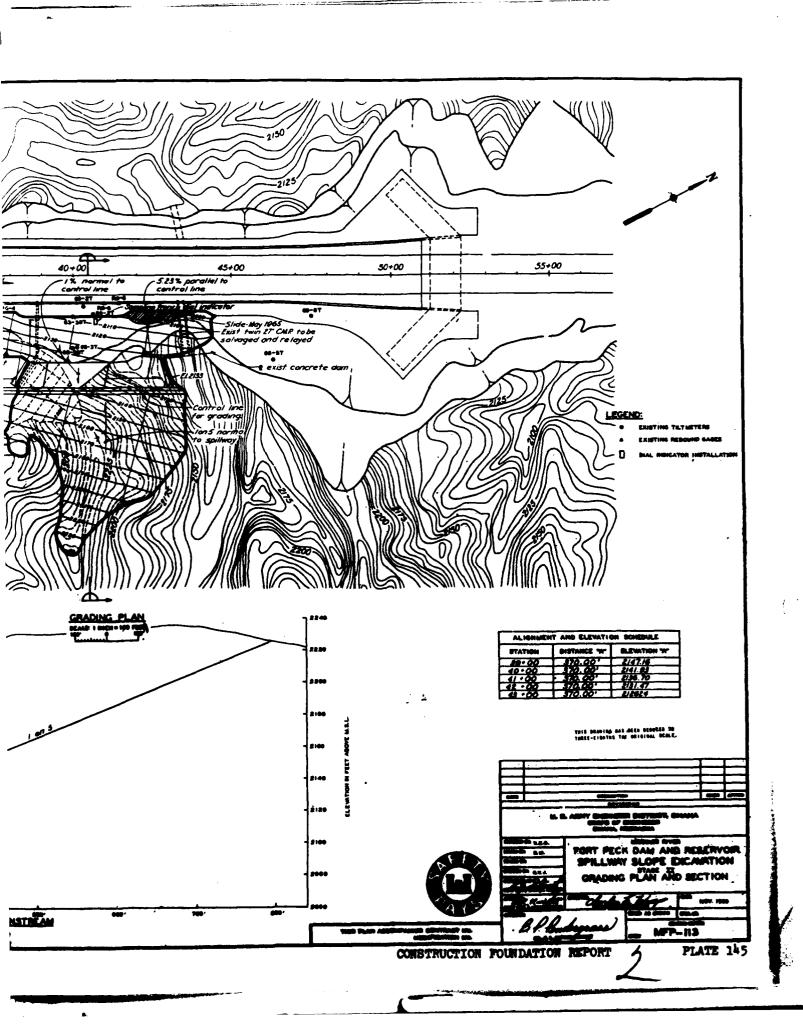


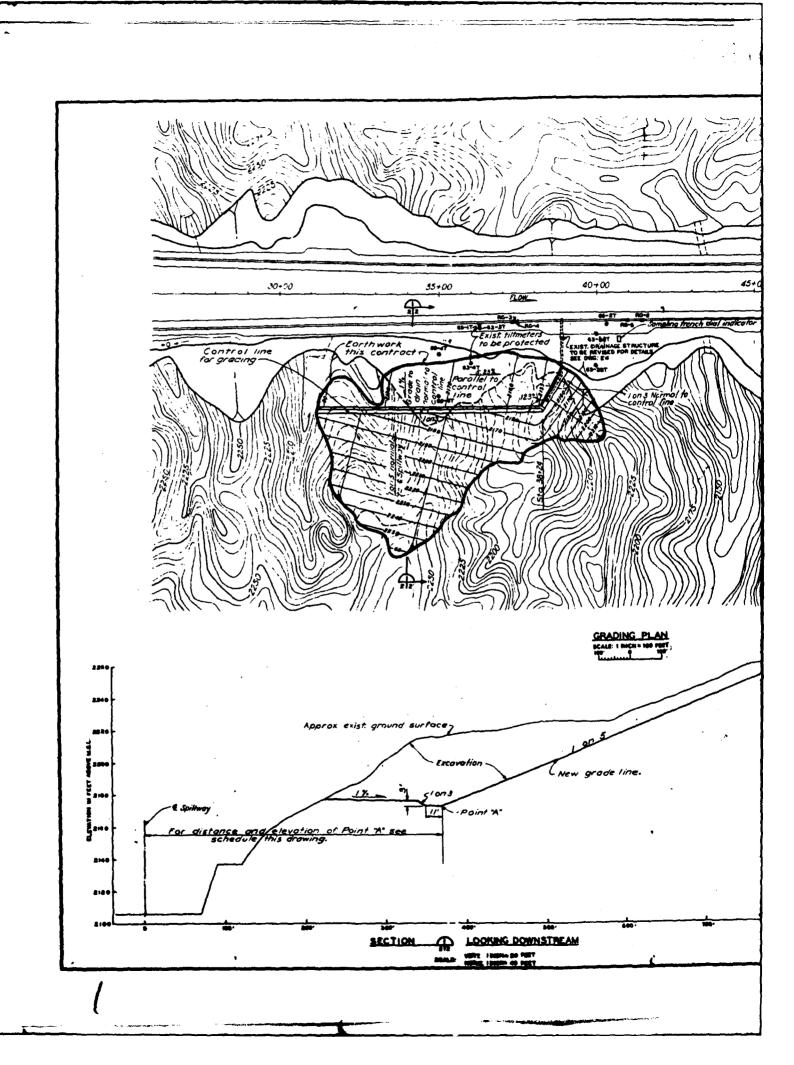


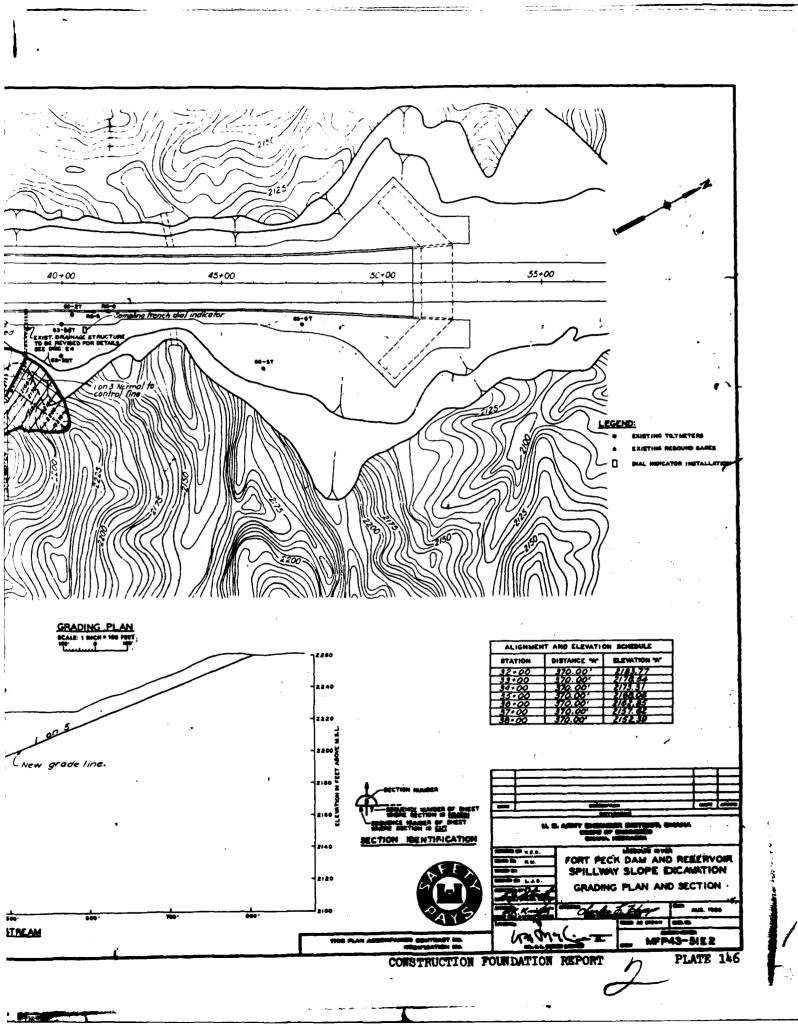


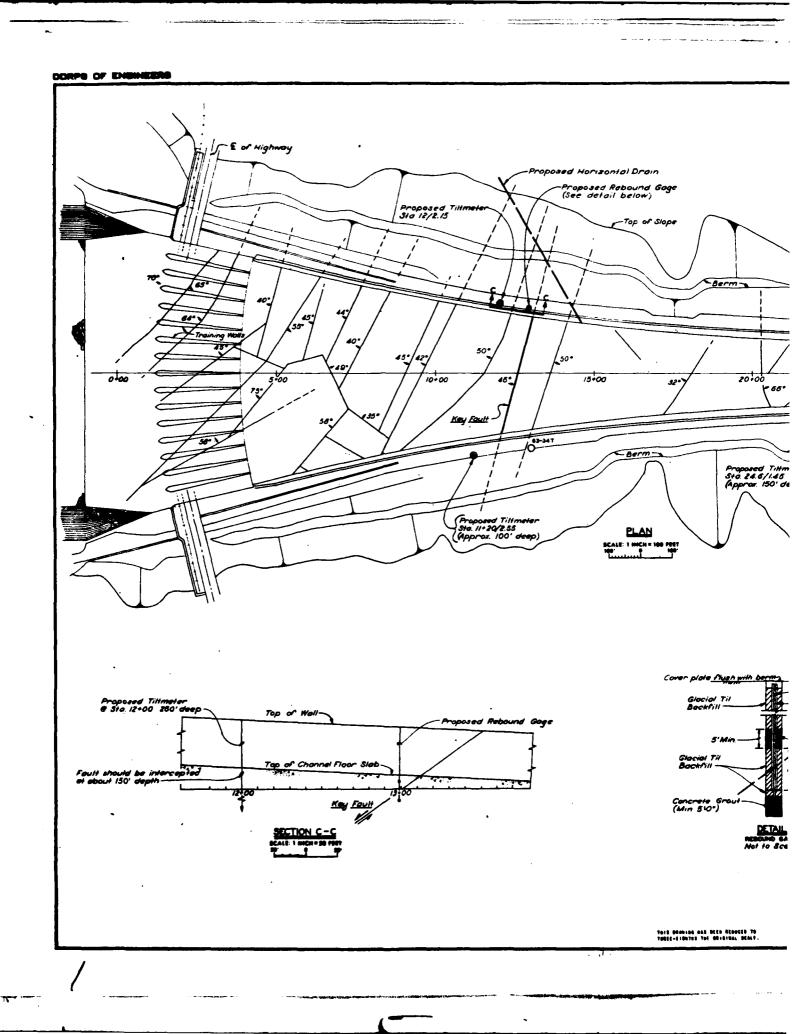


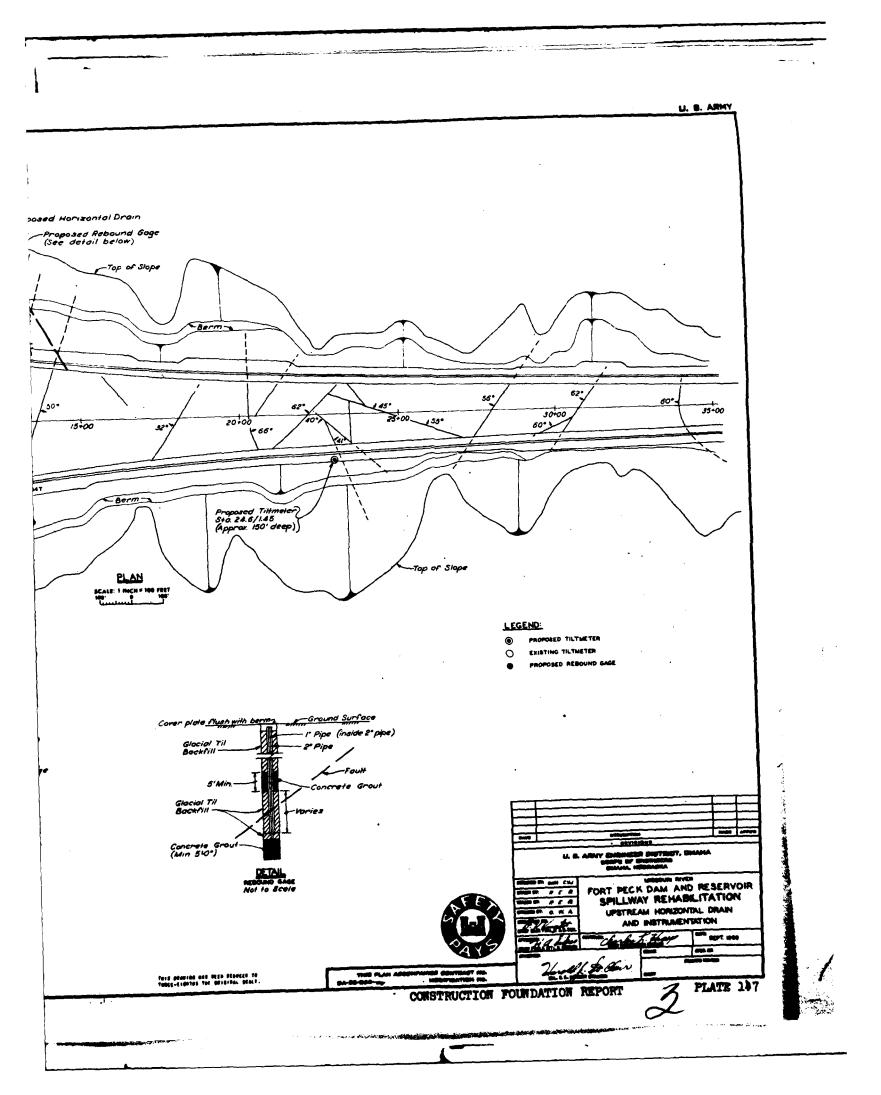


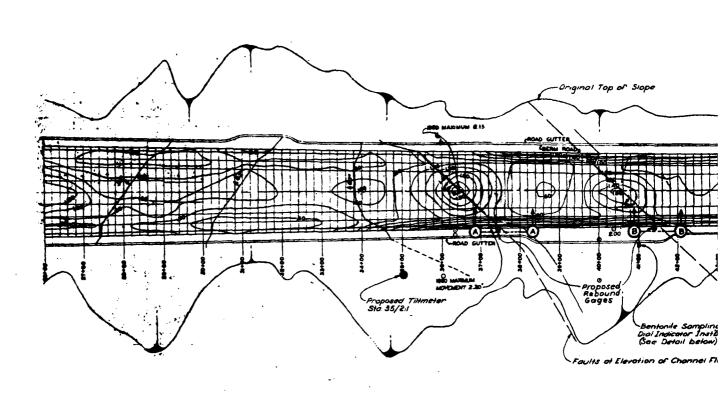




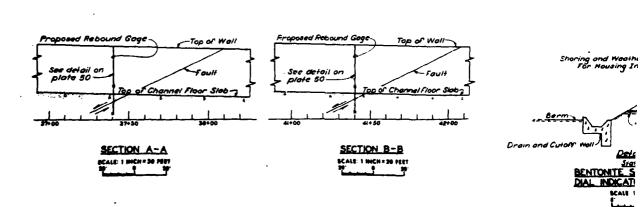




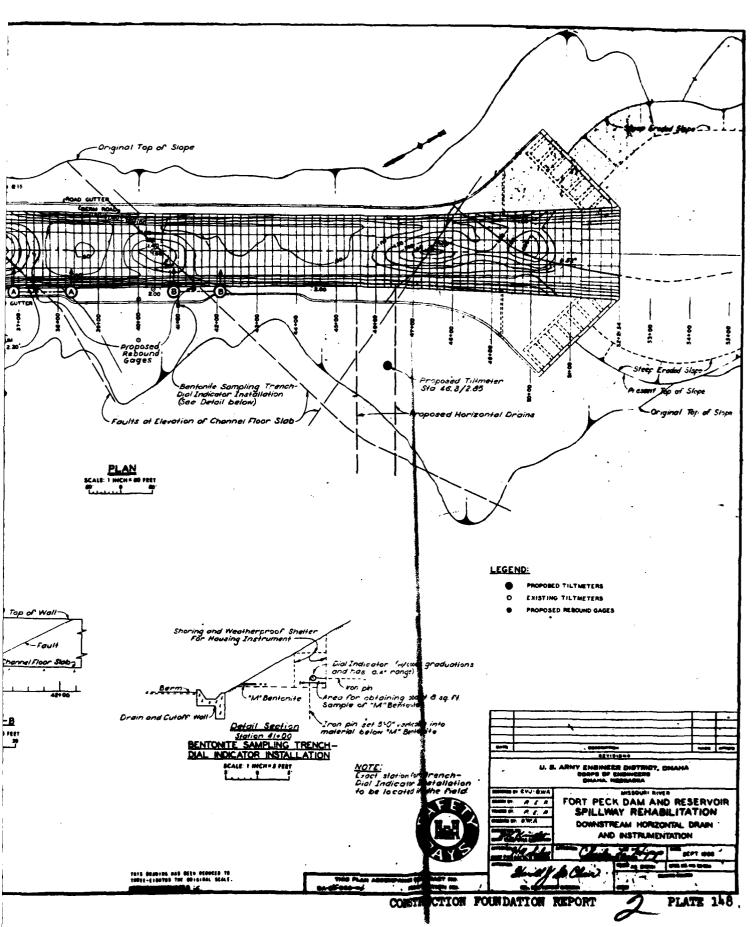




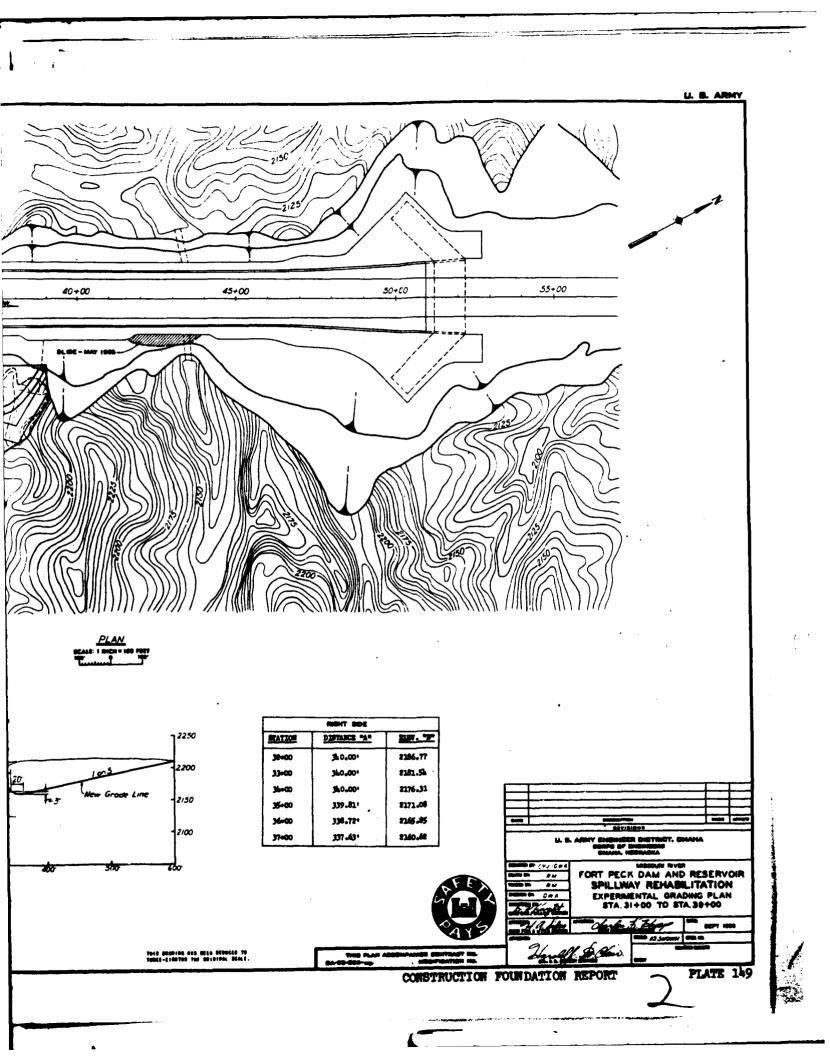


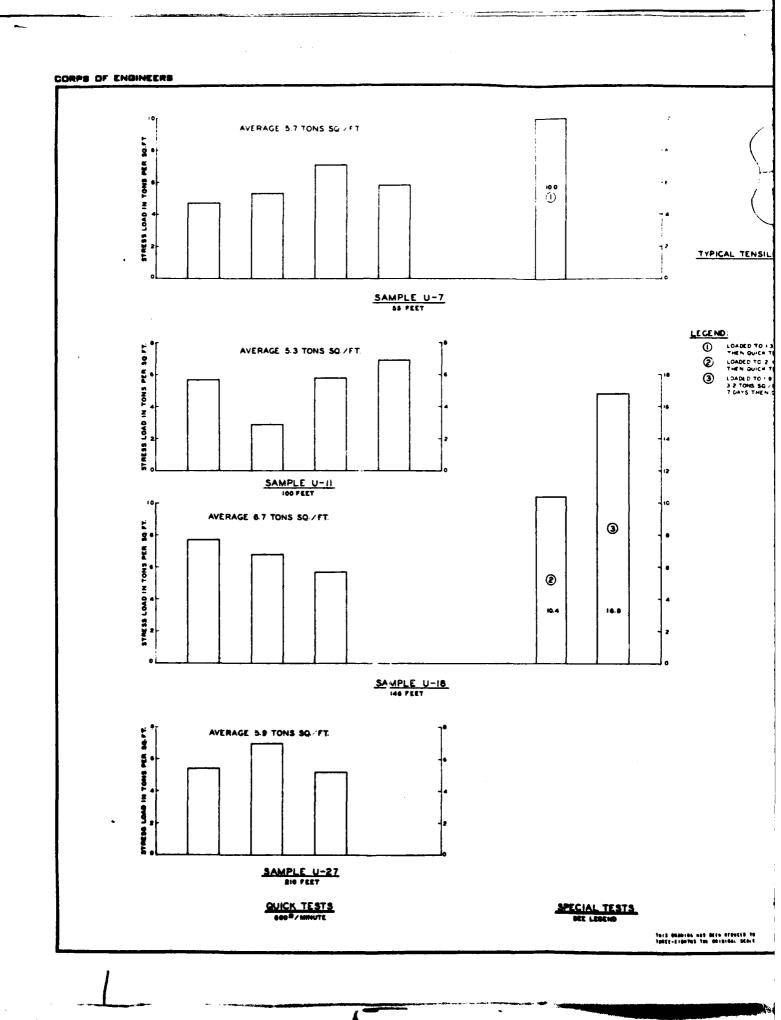


THIS DEADING HAS DEED DEDUCED TO THREE-ELONTES THE BUILDING MALE.



CORPS OF ENGINEERS 45+00 30+00 35+00 40+00 FLOW ገ*2250* 2250 ELEVATION IN PEET - KS.L. Original Ground 2/50 2100 STA 36100 TYPICAL SECTION THIS DESIRE HAS DEER REDUCED TO TRREE-EIGHTRS THE ORIGINAL DEALE.





U. B. ARMY 3 TONS 50 11 T ELDNGAT - 0100 <u>U-7 ①</u> STRESS LOADING (1) TYPICAL TENSILE SPECIMUM FAILURE -0400 LECEND: 0 LOADED TO 1.3 TONS SQ FT. FOR S DAYS THEN QUICK TESTED TO FAILURE 2 LOADED TO 1 9 TONS SQ /FT FOR 7 DAYS; 3.2 TONS SQ /FT FOR 8 DAYS; 4.9 TONS SQ 7 DAYS THEN QUICK TESTED TO FAILURE 3 U-18 (2) I STRESS LOADING 4.9 TONS SO./FT.~ 3.4 = 10-7 3 -3.2 TONS SQ /FT. ž 2 16.8 • • × 10-1 U-18 3 J STRESS LOADINGS BEFORE TESTING TO PAILURE u. B. Army Engineer Bietrigt, Omama Bourg of Engineers Omama, Hormadka FORT PECK DAM AND RESERVOIR
SPILLWAY REHABILITATION SUMMARY OF RESULTS TENSILE TESTS SPECIAL TESTS BEFT 1900 THIS STADIOS HAS BEEN STORES TO THOSE -- CINOTES THE GRISTMAL SCALE. CONSTRUCTION FOUNDATION REPORT

PLATE 150

